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STUDY

ON

THE ROASTING OF AMJHORE PYRITES

AND

SULPHURIC ACID MANUFACTURE

(PHASE 2)

FOR

PYRITES, PHOSPHATES & CHEMICALS LTD

NEW DELHI

INDIA

SPONSORED BY

UNIDO - VIENNA

1985

Amjhore Study

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Chapter 1

Introduction

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Chapter 1

1.1 Introduction

Contract No. 82/92 entered into between UNIDO, Vienna, and Lurgi for the Project No. DP/IND/81/018 has the objective of finding a viable process/es to utilize the pyrite bearing ores at Amjhore, of Pyrites, Phosphates and Chemicals Ltd., a Govt. of India Enterprise, New Delhi/India.

Under the aforesaid agreement the work to be done by Lurgi is divided into two phases

Phase 1:

The work under phase 1 comprised laboratory scale tests to produce a pyrite concentrate, suitable for roasting to produce sulphuric Acid. The results of the test-work under Phase 1 and budget estimates of a 560 t/d sulphuric Acid Plant and an Ore concentrator for 50 t/h capacity were worked out and submitted to UNIDO and PPCL along with operating costs of the plants. The study was submitted in August 1983 and accepted by UNIDO.

Based on the findings of the report on phase 1 UNIDO and PPCL gave the green signal to Lurgi to start work on phase 2 of the Contract.

Phase 2:

In a joint meeting with UNIDO, PPCL and Lurgi in Lurgi office on 24/25.10.83 the results of the phase 1 work were reviewed and the course of action for Phase 2 was decided (see Minutes of Meeting, dated 25.10.83). It was agreed that PPCL sends a bulk sample of the ore to be tested as follows:

Tailings of optical ore sorter: approx. 65 te Concentrate of optical sorter: approx. 15 te Screen undersize -20 mm : approx. 2 te Tailings and concentrates of optical are sorter are "as if produced".

The test material arrived late in the spring of 1984, upsetting the preplanned test schedule to take place already in February 1984. As the laboratory facilities were sold for other tests of other clients the benificiation tests could take place only in September 84.

The report was submitted in February 1985, no. 4548.

In May 1984 PPCL wanted to amend the course of the test programme originally foreseen. This amendment consisted of dropping of the roasting test to be conducted with a blend of the flotation concentrates and the finely ground concentrates of the optical ore sorter. It was declared by PPCL that they will be satisfied with the judgement of Lurgi on the roastability of the blended Pyrite concentrates on the physical appearance and the chemical composition of the blende so produced. The roastability of the blende is considered an established fact, as long as the size spectrum of the composite material can be kept uniform for feed to the roaster. PPCL wanted the above mentioned tests to be replaced by a direct roasting of the pyrite-ferrous shale-tailings of the optical sorter. The reason behind this thinking was that the recovery in the flotation and the flotation step will not be satisfactory economically, thus adding to cost of procudtion.

Since the Amjhore pyrites do not contain any appreciable non-ferrous metals the pyrites remain the only value bearer. The underground mining of the pyrites is cost intensive, hence the raw material costs have to be kept down.

The shale pyrites contains only 10 per cent sulphur, hence the autogenous roasting was at first sight thought doubtful. The application of the circulating fluid bed principle was therefore thought of in the beginning. However the very low water content below 2% and the insignificant carbonate levels are positive towards heat consumption. It was decided at first to conduct the tests in a stationary fluid bed, as this system is simpler and cheaper. To get a sulphur dioxide gas of sufficient strength it was important to achieve a high degree of conversion of sulphur. This is valid also for the sake of the thermal balance. For the same reason the carbon conversion is also of importance. The silica content of over 50% is also a phenomenon. To suppress the formation of silicates a low roasting temperature was selected. The commercial plant has to be suitably designed to tolerate the silica level and provide long life.

The roasting tests were conducted in July 1984 with a sample of 20 tons of the shale pyrites. The tests were extremely successful. The feed material was crushed to minus 2 mm and fed into the roaster at a rate of approx. 400 kg/h.

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A self-sustained roasting operation was obtained with a stable fluidisation and a steady SO₂-concentration of 8 Vol.%. The roasting efficiency was 97% and the residual sulphur in cinder was below 0.4%. It is expected that in the larger size commercial roaster even better efficiency can be obtained. The residual carbon content was below 0.2%. The bulk density of the feed was approx. 1. The water content in the pyrite was approx. 3%.

Hydraulic tests with the cinder showed binding property which increases with lime addition. It can be safely predicted that the cinder can be used as a cement additive.

The test report 4498 was submitted in August 1984. It can be safely predicted that the shale pyrites can be utilized as a suitable feed for a commercial-scale roasting plant when the composition and size analysis of the pyrite can be maintained uniform and the moisture content can be limited to below 3%. Constituents such as carbonates which can consume energy shall be negligible. The use of the shale pyrites will contribute to better economics of the Amjhore mines and reduce the environmental pollution arising from dumping of this material while mining of the high-grade pyrites.

1.2 Selected Process Route

Based on the test results submitted to PPCL and on subsequent discussions with them on 27th and 28th November 1984 in Frankfurt the process route to be followed for the study was decided. PPCL opined that the flotation step to produce pyrite concentrates from the tailings of the optical sorter will be too expensive due to the desliming step required and the not too high recovery of Sulphur obtainable. Since a direct roasting of shale pyrites has been proved to be technically feasible the process step to enrich it can be spared to reduce investment and operation costs.

PPCL therefore requested to work out the study for a plant with the following structure: -

2 Roaster streams with a common gas scrubbing and purification unit and a common sulphuric acid section.

The two Roaster streams shall each consist of R.1: Stream 1 to reast 217 tpd High Grade Pyrites R.2: Stream 2 to roast 240 tpd Low Grade Pyrites

The size of stream R.2 is derived at on the basis of available quantums while mining, according to PPCL. The resulting sulphuric acid capacity will be of the order of 320 tpd Monohydrate.

The two streams run up to the hot gas precipitators and are joined together before cas scrubbing and purification.

Both streams are fitted with waste heat boilers for maximum steam recovery and power generation as requested by PPCL.

1.3 Objectives of the Study

The objectives of the study can be summerized as follows: -

- To investigate a viable technical route or routes for the direct utilization of the pyrite deposits
- To determine the investment and operation costs of the selected process route.

The proposed capacity of the plant is decided by PPCL based on the site conditions and the marketability of the products. The capacity of 320 tpd Acid must be considered as small. The specific costs are generally higher at lower capacities than for large-scale plants. Hence, in evaluating the data of this study this fact must be borne in mind. The two major factors determining the selling price of the acid are the cost of pyrite and the interest rate of the money invested to build the plant. The remaining costs contribute in comparison less to the price of the acid.

An additional revenue can be expected from the sale of the cinder ash from the shale pyrites due to its binding property.



1.4 Significance of Pyrites: -

The pyrites play a significant role in the supply of sulphur which is largely used in the production of fertilizers and chemicals. The production of pyrites in the world, excluding Eastern Bloc countries, stood at 3.8 Million tons in 1984. The main source of the pyrites is as a by-product from flotation plants of zinc, lead and copper metals and in a few places of coal. These are mostly flotation pyrites forming an ingredient of metal bearing ores. As a by-product such flotation pyrites can be cheaper than those pyrites which are directly mined and have no association with other valuable minerals or metals.

The pyrites of the second category must be able to be mined in an economical way to compete with the by-product pyrites.

Compared to sulphur pyrites are widely dispersed on the earths crust and therefore found in almost all countries. In the more developed countries with an established infrastructure pyrites, when available as a national resource, form the backbone of sulphuric acid production. Some major producers & consumers of pyrites are Spain, Portugal, Sweden, Finland, Italy, Norway, Turkey, China, Germany, South Africa, Romania, Bulgaria, Japan, Philippines, USSR, etc.

In contrast the use of pyrites in India for sulphuric acid is nil, even though the pyrite resources are immense, the own sulphur production is negligible and almost all sulphur is imported against foreign exchange. The by-product pyrites are dumped at present! The main reasons seem to be

- no history of pyrite utilization in India
- the deposits are far way from consuming areas
- the lean nature of the pyrites with low sulphur contents.

The Indian pyrites as mined are extremely lean (20-25%s), contain no other metal values and are burdened with silica and earth minerals. In the absence of any pretreatment the ore can widely vary in its composition and disturb operation of a plant. A simple pretreatment will help to homogenize the feed material. Large-scale tests conducted by Lurgi with Indian pyrites have demonstrated the technical feasibility of roasting the pyrites.

It can be safely predicted that with properly designed plants the roasting of Indian pyrites can be made a commercial proposition.



Since the international sulphur prices have increased due to imbalance in the supply and demand of sulphur and this pattern is predicted to continue for a long time the use of domestic pyrites in future in India can be considered a logical step. With increasing consumption of pyrites the mining and pre-preparation costs can be brought down to relieve the cost of sulphuric acid.

The establishment of a fertilizer industry at the mines will reduce the transport problem of acid. An infrastructure for transport of acid by rail can lead to the development of acid terminals at major centres. These steps can help pyrites to compete successfully with imported sulphur.

1.5 General (Plant size and economics)

1.5.1 Plant size and Economics

The roasting and sulphuric acid plant with a capacity of 320 tpd Acid is too small in size to be fully economical from a purely commercial point of view. The perspectives in Amjhore are different. The plant size may have been fixed to match the present mine output and the marketability of the acid or its derivative -

Fertilizer, presently.

The addition of a second roaster stream to Ronsume the pyriteferrous shale with 10 % Sulphur content, which is a by-product companion of the pyrites mined and a waste until now, involves high investment costs, which can be justified only if an outlet for the calcine as a cement additive is considered to obtain additional revenue and as a waste utilization measure of the mine operations in the overall picture.

Otherwise it would be more economic to roast a mixture of pyrites and shale in a single roaster. This would save costs also in the ore preparation section.

Thus, the plant especially is to be seen as a demonstration unit, with the character of being a forerunner for larger units in the future.

This constraint must be properly evaluated in the economic and financial analysis that may be required for the investment decision, to dertermine the commerciability of the plant.

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1.5.2 Impact of the Plant to People:

In the opinion of the authors of this study a part or whole of the investment money required to put up the plant must be available as soft loan to PPCL because pyrites, as a substitute for imported sulphur, have a strategic importance for the Indian economy and relieved funds can be utilized for other essential imports. Sulphuric acid as the mother of chemistry can facilitate the sport of other industries in the region and allieviate poverty.

In a larger perspective the pyrites plant offers the benefit of employment to thousands of people in the region and in addition produces fertilizers which is a stragetic commodity for India to increase food output. Using a domestic raw material it helps to strengthen the economic base of India by decreasing the dependence on imported raw materials. As India has an adverse balance of payment the reduction in import of sulphur, which is a tight commodity now, can release funds for other purposes and thus help the people of India to benefit from their own resources.

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1.6 Economic Comparison between Flotation Route and Direct Roasting Route

When the study was elaborated, two different ways of producing sulfuric acid from the ores won in the amjohre mine were thoroughly discussed. The investigations and considerations of both stages permit a rough assessment of the economy of sulfuric acid production in the two routes:

- Photometric preseparation, flotation of the shale portion, roasting of a blend of photometric and flotation concentrates (Route 1)
- Photometric preseparation, separate roasting of post-comminuted concentrate resulting from photometric preseparation (high-grade pyrite) and shale (low-grade pyrite) (Route 2)

This economic appraisal is implemented by a comparison of the capital and operating costs incurred for every route. Both cases are based on an acid production of 320 t/d requiring a run-of-mine ore rate of 570 t/d for Route 1 and of 520 t/d for Route 2.

The comparison is related only to the actually deviating processes of the two routes, i.e. costs for photometric preseparation, infrastructure etc. have not been taken into account.

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The following costs will be incurred:

| Route 1 | Route 2 | | |
|---------------------|---|--|--|
| | | | |
| Rs 3C million | Rs 10 million | | |
| Rs 175 million | Rs 186.6 mill. | | |
| (one stream) | (two streams) | | |
| Rs 205 Mill. | Rs 196.6 Mill. | | |
| | | | |
| | | | |
| Rs 74.8/tMH | Rs 9.75/tMH | | |
| no significant char | nge. | | |
| | Rs 3C million Rs 175 million (one stream) Rs 205 Mill. ======== | | |

As regards pyrite preparation, major differences occur in the operating costs due to the expense required for grinding (energy and grinding media) and for flotation reagents.

The disadvantage to be considered of Route 1 is the loss of part of the sulfur in the slimes and tailings of beneficiation. These tailings might also cause some difficulties in an environmental respect.

Chapter 2

Design Conditions, Production and Consumption Figures and Staff Requirements

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Chapter 2

2.1 Design Conditions

2.1.1 Raw Materials

Raw Material delivered to plant from mines

ROM, crushed to minus 110 mm

Prescreening before ore sorter

minus 10 mm.

This material is taken out as agricultural grade pyrites.

Working hours of ore sorter: section: 12 hrs/day

Optical ore sorter separates

1. HGP = High grade pyrites.

2. LGP = Low grade pyrites.

Since the Amjhore pyrites have the property for selfignition long storage of crushed pyrites is avoided. The roaster bins, with a capacity of 150 cu.m. is filled each day with freshly crushed pyrites.

Reference drawings ore preparation: L1A 00 2250 00001/2

This ore sorter section is designed to treat the necessary amount for one week operation of the roaster $(240 \text{ t} + 217 \text{ t}) \times 7 = 3199 \text{ t}$ plus agricultural grade pyrite within six days of operation.

The crushing section operates on the same cycle as the roasting plant, i. e. on seven days per week. Buffer stock between these sections are the stockpiles for high and low grade coarse pyrites.

2.1.2 Pyrites Feed

Roaster Stream no. 1: 217 tpd HGP Roaster Stream no. 2: 240 tpd LGP

PPCL supplied by telex on 02.07.34 the following analysis for HGP:

Chemical Analysis HGP

Sulphur (tot) 38.1 33.5 Iron (tot) Carbon (tot) 1.4 Silica 22.5 : Aluminium 0.8 - 1.2Magnesium 0.15 Arsenic : less than 0.1 0.005 Manganese 0.025 Lead 0.03 Cobalt 0.015 Nickel Chromium 0.03 0.007 Vanadium Copper 0.01 0.01 Zinc Antimony 0.02 Molybdenum 0.005 0.0002 % Silver

Moisture content: 5 %

We were asked to base design of Roaster no. 1 on above analysis.

| Chemical | Analysis | LGP |
|----------|----------|-----|
|----------|----------|-----|

| tot. | Sulphur | = | 11.6 | 8 |
|------|---------------------|---|---------|----------|
| tot. | Iron | = | 11.8 | 8 |
| tot. | Carbon | = | 2.7 | ક |
| | Copper | = | 0.05 | 8 |
| | Zinc | = | 0.05 | 8 |
| | Lead | = | 0.05 | ક્ર |
| | Arsenic | = | 0.007 | 8 |
| | Mercury | = | less th | an 1 g/t |
| | Florine | = | 0.08 | 8 |
| | Chlorine | = | 0.03 | 8 |
| | Silica | = | 52.2 | 8 |
| | Alumina | = | 10.8 | 8 |
| | Ca0 | = | 0.55 | 8 |
| | MgO | = | 1.1 | 8 |
| | TiO ₂ | = | 0.56 | 8 |
| | Potassium | = | 2.8 | 8 |
| | Phosphorus | = | 0.14 | ક |
| | (co ₂ -c | = | 0.11 | %) |
| | | | | |

Moisture content: 3 %

The pyrites are poor in non-ferrous metal contents. The high content of Silica is note-worthy. The moisture level is low. Dusting will be a nuisance in the ore preparation plant.



While designing the handling system by the company involved for pyrites appropriate measures shall be incorporated to avoid dusting of material during transfer and movement of pyrites.

- rubber skirts at transfer points
- wide slow belts
- minimum fall heights while transferring
- dust suction system
- fall pipes to remove spillage

Appropriate protection shall be provided against rain without hindrance to ventilation, especially the LGP do not tolerate higher moisture.

Typical size analyses of the LGP pyrites

| greater | than | | | 2 | mm | = | 0.0 | 용 |
|---------|------|------|------------|-------|----|---|------|---|
| | 2 | ? | - | 1.5 | mm | = | 9.6 | 용 |
| | 1 | 5 | - | 1.0 | mm | = | 24.9 | 용 |
| | 1 | .0 | - | 0.5 | mm | = | 29.2 | 용 |
| | 0 | .5 | . - | 0.315 | mm | = | 11.9 | 8 |
| | 0 | .315 | - | 0.2 | mm | ± | 9.8 | 용 |
| | 0 | .2 | - | 0.125 | mm | = | 4.9 | ક |
| | 0 | .125 | - | 0.09 | mm | = | 2.6 | ક |
| | 0 | .09 | - | 0.063 | mm | = | 2.2 | 용 |
| | less | thar | 1 | 0.063 | mm | = | 4.9 | ક |

Bulk density : average 1.5 kg/dm 3 Angle of repose : 40 $^\circ$

2.1.3 Location of the Plant: Amjhore, State Bihar

India

Height above sea level: 165 m

Earthquake danger : nil

Soil bearing strength : 2 kg/cm²

Climate Conditions at Site.

Barometric pressue : 980 mbar

Air temperature : min 4 °C

max 48 °C

Average : 25 °C

Air Humidity average : 75 %

2.1.4 Cooling Water

Fresh water : min 15 °C

max 30 °C

Average : 25 °C

The cooling water for industrial purpose shall be filtered and free of impurities. The pH value is assumed to be 7.

Supply pressure at B/L: 4 bar.

Fresh cooling water is required as make-up for the cooling water recirculation system.

Wet bulb temperature : 27 °C

Cooling water temperature

after cooling tower : 30 °C

Cooling water temperature

1 1 1

inlet c.t. : 40 °C



2.1.5 Process Water

Temperature : average 25 °C

Pressure : 3 - 4 bar

Quality : drinking water quality

Process water is required as make-up water in the gas cleaning plant and in the acid plant.

2.1.6 Electricity

High voltage : 3.3 kV, 50 cycles

Low voltage : 415 V, 50 cycles

Control voltage : 220 V, 50 cycles

Signal voltage : 24 V, DC

Tropicalised design.

2.1.7 Compressed Air

Normal pressure : 7 - 8 bars

for continuous supply for boiler rapping instrument air shall available free of oil and moisture for electro-pneumatic actuators. Pressure: 5 - 6 bars

2.1.8 Fuel Oil

Light oil, free of water and impurities required for preheating the roasters and the converter

L.c.v. of oil : 9 500 kcal/kg Viscosity : less than 350 Cs

2.1.9 Operating Time

The plant operating time per year : 330 days

2.1.10 Roasting Process

Normal roasting process for dead roasting of the pyrites, with complete oxidation.

2.1.11 Steam

High pressure steam, 40 bars, superheated to 350 °C will be generated in the waste heat boilers of both roaster streams. The steam is used to run a turbo-generator for power generation.

2.1.12 Power Generation

A condensation turbine is attached to the Plant to expand the produced superheated steam in the plant and produce electric power, 3.3 kV.

The produced power is integrated into the captive circuit of the Plant.

An auxilliary condensor is provided for the full steam output in case the turbine is out of operation.

2.1.13 Boiler Feed Water

BFW is required as make-up for losses in the watersteam circuit.

Fully demineralised BFW must be prepared in a feed water treatment plant.

The BFW must have the following analysis: -

General condition : clear and colourless Hardness : less than 0.02 mval/kg : less than 0.02 mval/kg 0xygen : less than 25 mg/kg : not detectable : less than 0.05 mg/kg CO₂-bound free Fe-total Cu-total : less than 0.01 mg/kg

: over 9.0

pH-value at 25 °C KMnO₄-consumption : less than 10,0 mg/kg : less than 1,0 mg/kg

Conductivity : less than 0.02 micro S/cm

Temperature : 25 °C average

: 2.5 bar Pressure

Continuous steady supply required at boiler.



2.1.14 Cinder

The cinder produced in the plant are of two qualities. Cinder from Roaster no. 1 is cooled and wetted for further handling by storage and transport. It can be partly sold to cement plants for adjusting the iron module.

Cinder from Roaster no. 2 is indirectly cooled in a rotary cellular cooler and stored in a silo for further sale as an additive to make a hydraulic binding agent. For this reason this cinder is not wetted to avoid any build-up.

2.1.15 Wash Acid: -

The wash acid discharged from the gas scrubbing plant is turbid, but has a H₂SO₄ strength of approx. 15-20%. Usually for fertilizer²production this acid can be used for mixing with rock phosphate. Thus a dumping can be avoided and the by-product valorized.

2.1.16 Turbo-Generator Set

Type: condensation turbine, terminal output 3.5 MW.

Inlet steam conditions:

Pressure : :0 bars Temperature: 350 °C

Low pressure steam pass out: 5 bar Exhaust steam pressure : 0.14 bar Cooling water temperature : 30 °C

Steam flow rates:

Inlet to turbine : normal 16 t/h
max. 18 t/h
Pass-out : 0 - 1.8 t/h

Exit steam : max. 18 t/h

Output at generator terminals: max. 3.5 MW.



Specific steam consumption:

| Output | kW 3 | 500 | 3 300 |
|-------------------|--------|------|-------|
| Live steam in. | t/h | 18.0 | 18.0 |
| Pass-out | t/h | 0.0 | 1.8 |
| Specific steam to | kg/kWh | 5.14 | 5.45 |
| energy racio | _ | | |

Generator design data.

| Generator apparent power: | 4 375 kVA |
|---------------------------|-------------|
| Cos. Phi (power factor): | 0.8 |
| Terminal voltage : | 3.3 kV + 59 |
| Frequency : | 50 cycles |
| Protection : | IPR 44. |

Condensor

| Steam input | : | normal | 16 | t/h |
|-------------|---|--------|----|-----|
| | | max. | 18 | t/h |

Exhaust steam pressure : 0.14 bar Cooling water inlet : 30 °C

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2.2 Production Figures

At nominal capacity of the plant the production figures below are expected.

2.2.1 Acid Production

The main product of the plant is sulphuric acid monohydrate

Acid from roaster stream R.1: 240 tpd (MH)
Acid from roaster stream R.2: 80 tpd (MH)

Total: <u>320 tpd</u> (MH)

2.2.2 By-Products from the Plant

a. Superheated Steam: 41 bar, 350 °C

Stream R.1: approx. 12 t/h
Stream R.2: approx. 4 t/h

Total: approx. 16 t/h

- b. Electric power generation: max. 3.5 MW
- c. Cinder:

Stream R.1 : = 6 800 kg/h (dry) Stream R.2 : = 9 000 kg/h (dry)

2.3 Consumption Figures

At nominal capacity of plant

2.3.1 Pyrites

H.G.P for Stream 1: approx. 217 tpd (dry)

L.G.P for Stream 2: approx. 240 tpd (dry)

2.3.2 Cooling Water

a. Make-up water : approx. 60 m³/h
for cooling Tower

b. Fresh water : approx. $10 \text{ m}^3/\text{h}$

Water in circulation in the cooling tower is approx. 1 800 m³/h; of which approx. 3% assumed lost.

Cold water temperature : 30 °C Hot water temperature : 40 °C

2.3.3 Process Water

Process water is required in the gas cleaning plant as make-up and in the acid plant for adjusting acid concentration.

Demand : approx. $3 \text{ m}^3/\text{h}$

2.3.4 Electric Power

Installed motor capacity: approx. 3 460 kW

Power consumption is expected to be as follows:

a. Ore preparation plant : 170 kW (no ore sorter)

b. Roasting Plant, incl. HGP

Roaster stream 1 = 296 kWRoaster stream 2 = 241 kW

BFW-Pump = 36 kW common for both

c. Gas Cleaning Plant = 160 kW

d. Acid Plant = 960 kW

e. Turbo-Alternator set = 30 kW

f. Water Treatment Plant = 267 kW

All figures are estimated approximately.

2.3.5 Compressed Air

Approx. 200 Nm³/h for each boiler at intervals. Pressure: 7 bar steady

2.3.6 <u>Fuel Oil</u>

Light oil is required only for preheating purposes at the roaster and the converter

max. consumption at roaster: 600 kg/h
max. consumption at converter: 600 kg/h

2.3.7 Instrument Air

approx. 20 m^3/h at 5 - 6 bar for electro-pneumatic valves.



2.4 Operating Staff

The following personnel is recommended, but the actual number, grades, etc can change according to local conditions

1 plant manager

1 mechanical engineer

1 electrical engineer

Shift operation (3 x 8 hours)

4 foremen

4 operators (chemical workers)

4 boiler operators

8 assistant operators

10 helpers and loaders

Plant maintenance

A gang of 2 mechanics, 1 electrical foreman, 1 welder, 1 instrument mechanic and 2 helpers.

1 laboratory Chemist and 1 helper for sample taking

A total of approx. 50 persons is considered adequate.

2.5 PPCL has indicated vide their telex of 10.10.85 that the manpower requirement for running the plant under local conditions will be as follows:

Operation : 37 persons

Maintenance: 43 persons

Total : 80 persons

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2.5 Plant Effluents

2.5.1 Roasting Plant

- Blow-down from boiler: approx. 0.3 m³/h

- Cinder from R.1 : approx. 6.8 t/h

- Cinder from R.2 can be used. ~ 9 t/h

2.5.2 Gas Cleaning Plant

- sludge (acidic) : approx. 240 kg/day

To be mixed with cinder from R.1 before disposal

- Flushing water : 8 m³/day occasionally

2.5.3 Sulphuric Acid Plant

- Tail gas (75 °C) : approx. 34.000 Nm³/h

SO₂ in tail gas : approx. 0.7 g/Nm^3

Acid mist in tail gas: approx. 50 mg/Nm³

- Flushing water : approx. 72 m³/day

at intervals, slightly acidic, after cleaning

2.5.4 Total effluent water: approx. 80 m³/day (occasional)
The acidic water, nating from the plant is due
mainly by from an its in the closed system and
subsequent washing with water, and not from any
continuous source.
This effluent water, whenever it is acidic, can be
diverted to a pit, where lime stone/soda is added for

neutralization. The pump installed in the pit can be used to circulate water in the pit or discharge it to canal for final

disposal along with the mine water.



Chapter 3

General Process and Plant Description



Chapter 3

General Process and Plant Description

3.1 Ore Preparation Plant

3.1.1 Screening and sorting section

The run-of-mine ore with a maximum grain size of 110 mm will be delivered from the mine by trucks with 7 tons capacity, these trucks will dump their load either to a feed hopper of approx. 70 tons (2 hours) capacity or an emergency dump near the hopper. According to the amount of ore in the hopper, ore from the emergency dump is reclaimed by a wheel loader.

The working time for the equipment of the ore preparation plant will be 18 hours per day. As the daily capacity of the plant will be 650 t/d, the nominal capacity of the equipment was chosen to be 36.1 t/h of feed.

From the hopper the ore is discharged at a controlled rate by a reciprocating feeder onto a conveyor belt. This feeds the screen above the sorting equipment. The screen is equipped with two decks to classify the ROM-ore into two fractions for photometric sorting (10-40 mm and 40-110 mm) and the undersize minus 10 mm (as agricultural grade pyrite). The screen undersize is transported by a belt conveyor to a dump outside the screening/sorting building.

The two coarse fractions flow to surge bins above the photometric sorters. Feeding to the sorters takes place by vibrating feeders.

The sorters are separating the material according to their different optical properties in high grade pyrite and shale. Two belt conveyors collect the pyrite respectively the shale from the two sorters.

A larger amount of material 10 - 110 mm will be stored outside on dumps. These dumps represent the main buffer stock between the mine and the two roasting plants. The dumps will have a life capacity of approx. 720 t pyrite resp. 530 t shale. Total capacity is approx. 4-fold this amount.



3.1.2 Crushing section

According to the requirements of the roasting plants the material has to be crushed to below 2 mm. This is done in the crushing and screening section alternatively for the two qualities of feed material. Crushed material is produced in an amount, which is sufficient for the daily production of each roasting plant. By storage of relatively small amounts of crushed material over a short period of time the danger of self-ignition shall be avoided as far as possible.

Beneath the two dumps of high grade pyrite resp. shale a tunnel is arranged. Inside the tunnel a belt conveyor is installed. Onto these belt conveyor either pyrite or shale is fed from the dumps by means of reciprocating feeders with remote controlled drive. A third feeding point between the two dumps may be used for both materials either in emergency cases or for blending purposes. The primary crushing is performed by an impact crusher. Crusher discharge is delivered by a belt conveyor to a double deck screen. The undersize below 2 mm is the final product. The size fraction 2 to 6 mm goes to secondary crushing, which is carried out by a roll crusher. Roll crusher discharge is recirculated to the double deck screen. Oversize plus 6 mm of this screen is recirculated to the primary crusher.

The screen undersize is fed onto a belt conveyor for transport to the day bins of the two roasting lines. By means of a motorized flap the material flow may be directed either to the bin of roasting line 1 or 2. By electric interlocking the flap can be shifted only, when a certain time is passed after stopping a reciprocating feeder. According to the position of the flap only the reciprocating feeder below the appertaining stockpile will be operated. By this interlocking mixing of the two different materials will be avoided.



3.2 Roasting Plants and Gas Cleaning Plant

Two independent roaster streams, starting from the roaster feed bins up to the Lot electro-filters are provided to roast both types of pyrites - standard HGP and shale pyrites LGP - separately.

Stream no. 1, equivalent to an acid production capacity of approx. 240 tpd, can be operated solely as well. Both streams are equipped with waste heat boilers for steam raising. Stream 1 generates approx. 12 t/h and stream 2 approx. 4 t/h of superheated steam. The steam is joined and led to a turbo-generator set for generating 3.5 MW power. The condensate from the turbine is cooled and recycled back to the feed water tank, in a closed loop.

The turbine has in parallel a reducer station to divert steam, when turbine is off. The condensor is designed to take care of cooling under emergency. The boiler feed water preparation plant is designed for a capacity of approx. 4 m³/h as its duty is only to make-up for losses in the closed circuit. The feed water system is common for both streams.

A buffer tank (12 m^3) as stock, the feed water tank integrated with degaser and the feed water pumps to both boilers.

The plant arrangement is made as a grass-roots plant with no restrictions on site.

The roaster stream design features: -

3.2.1 Roaster Stream No. 1

This stream is designed to roast the high grade pyrites.

Incoming pyrites are stored in the day bin, capacity 150 m^3 , with double extraction ends. A speed controlled extraction belt is attached to both bottom ends of the bin.

The extracted pyrites are fed into the roaster at two feed points, via intermediate conveyor belts. At the feed points of the roaster star type valves are fitted to seal the roaster.

The fluid bed roaster is a well proved Lurgi design, with a grate area of approx. 18 m².

Roasting air is introduced into the roaster by a roasting air blower, which has an inlet vane control for metering the air flow into the roaster.

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For preheating the roaster 2 start-up burners with oil-firing are arranged at the bottom section of the roaster. Max. oil flow will be approx. 300 kg/h each.

The oil tanks (2 x 50 m^3) are common for both streams and also the acid plant.

When the roaster auxillary bed is preheated to the ignition temperature of the pyrites, pyrites will be fed into it under fluidisation with the roasting air supplied by the roasting air blower.

The temperature in the fluid bed is controlled via cooling coils inserted into the bed. The cooling coils are cooled with boiler water circulated via the circulating pumps. The cooling coils are designed to extract the surplus heat generated during roasting and keep the preset temperature in the fluid bed well below the fusion point of the pyrites.

The bed temperature shall be equal to or below approx. 800 °C.

The roaster has an underflow with a motorized valve for extraction of the cinder and thus keep the bed volume at permissible levels, as expressed by the bed pressure reading. Secondary air nozzles are arranged at the middle section of the roaster to inject secondary air into the roaster if found necessary.

The fluid bed roaster is bricklined to conserve heat and protect the furnace shell.

The roaster is lagged outside to keep the shell temperature well above the condensation point of SO₃ during operation.

The roasting gases together the fine cinders entrained in the gas are drawn out of the roaster into the waste heat boiler for cocling and steam raising.

The waste heat boiler is of special design to cater to dusty and erosive/corrosive gases. The gas passage through the boiler, the bundle design and the cleaning arrangement of the bundles are specially designed to give trouble-free and uninterrupted service.

The steam pressure is the whole system will be held constant at 42 - 45 bars during operation and in warm condition of the plant so as to keep the metal temperature above the condensation point to prevent corrosion attacks.

For efficient flooding of the boiler tubes a forced circulation boiler design is adopted. The gases cooled to 350 °C pass into a cyclone for dedusting and from there to the hot electrostatic precipitator for final cleaning to below 200 mg/Nm³ dust level in the gas before wet scrubbing.



The cinder settling in the boiler, the cyclone and the HGP are collected by drag conveyors and forwarded to a cooling and wetting drum, where the cinder is conditioned by water jets for final transport and storage. The down-stream equipment after the roaster is made gas-tight to prevent the ingress of air into the system, dilute the gas and also cause corrosion. All these factors must be carefully looked into in detail to ensure prolonged and trouble-free operation of the plant.

The transport equipment must be designed to meet extreme erosion properties of the cinder.

Suction is maintained in the system, to draw off the produced SO₂-bearing roasting gas, by the SO₂-gas blower arranged in the sulphuric acid plant. At roaster outlet the suction pressure shall be plus minus zero.

The roasting gas freed of almost all dust is quenched in the scrubber by water circulated by centrifugal pumps. The hot gas evaporates a part of the water and cools down to the saturation point. The wet gas is then indirectly cooled in a star-type lead cooler to the gas temperature prescribed by the acid plant to maintain the water balance there. This usually lies in the range of 40 °C.

The cooled saturated roasting gas is finally purified and freed of all water and mist in two parallel wet electrostatic filters.

The water separated in the star cooler and the wet filters are collected and flow back into a pump tank. Since the roasting gas contains some SO₃ the water is slowly acidified.

The acid strength of the wash acid is maintained at a constant level by discharging a certain amount of liquid from the system. This wash acid containing some impurities can however be used for normal phosphate rock digestion internally in the plant.

The remnants of particulates contained in the wash acid

The remnants of particulates contained in the wash acid are separated in a settling tank arranged in the circuit. The settled sludge is to be removed from time to time from the settling tank and can be added to the cinder for disposal.

For efficient functioning of the HGP and WGP automatic voltage regulators are used to keep the discharge electrodes at highest possible voltage level before arcing takes place.



3.2.2 Roaster Stream No. 2

The roaster stream no. 2 is designed to roast the very lean pyrite-ferrous shale, having only approx. 10% S. The roaster has a size of 10 m² grate area. Approx. 240 tpd of shale pyrites are roasted to generate only approx. 80 tpd Acid MH. The plant design differs from the stream no. 1 on following points:

A hot cyclone is arranged after the roaster to dedust the gas before cooling in the waste heat boiler. Due to high content of inert solids in the lean shale pyrites the dust concentration in the gas rises to over 900 g/Nm³. The hot cyclone removes the major part of the dust from the gas so as to relieve the boiler and down-stream equipment from the dust load. The roasting gas is dedusted in a separate HGP because of its different behaviour and then the roasting gas joins the stream no. 1 to enter the wet gas cleaning section which is common for both streams.

To adjust the pressure drops in both streams and stabilize the gas flow motorized dampers are provided in both gas ducts.

Because of the binding property of the cinder from stream 2 a rotary cellular cooler with indirect water cooling is provided to receive the hot cinder and cool it to below 80 °C.

This cinder is dry and stored in a silo for further sale as cement additive.

The steam generation is this line is less than 4 t/h.

The cooling water required at the major consumers is recycled in closed loop between the cooling tower and the consumers.

The cooling tower is designed to cool a total of approx. 2000 m 3 /h water by 10 °C and has 4 cells arranged as 2 x 2. The warm water is pumped up from the sump.

The fresh water requirement is reduced to make-up for losses in the system.

The plant design follows the most modern principles and incorporates the latest know-how and technology.



3.3 Sulphuric Acid Plant

The dedusted, demisted and cooled but humid gases from the wet electrostatic precipitators are conveyed to the drying tower, where they come into an intensive contact with sulphuric acid of about 96%.

The tower, which is packed with filling bodies, is irrigated with the sulphuric acid in a countercurrent flow.

The sulphuric acid absorbs the moisture content of the gas and is thus heated-up. The acid is recycled by means of a vertical pump and cooled in acid coolers by means of water.

To prevent acid droplets from being entrained in the gas, the gases leaving the drying tower are passing through a wire-mesh filter.

The dry gas is now conveyed to the SO_2 -gas blower and from here via the heat exchangers T2.140, 141, 110 and 130 to the converter, in which the SO_2 is converted into SO_3 . The converter comprises the vanadium containing catalyst, distributed over 4 trays. This catalyst becomes active at a temperature of about 420 °C and causes the exothermic oxidation of SO_2 to SO_2 .

To initiate the reaction, the SO₂ containing gas has to be preheated to about 440 - 450 °C. For this purpose, the above heat exchangers are provided. On one side, the heat exchangers are traversed by incoming SO₂ gas and on the other by the precatalyzed gas. The gas leaving each tray has to be cooled to such a degree, that in the following tray an optimum conversion efficiency is achieved at a specific temperature.

After the second tray, the gas passes through the heat exchangers T2.120/121 and then to the intermediate absorber, which is designed similar to the drying tower. In this tower, the SO₃, which has been formed after the first and second tray, is extracted from the gas. By this SO₃-absorption, the reaction equilibrium in the last two trays of the converter is shifted towards the SO₃-formation. The circulation acid is pumped by a vertical acid pump from the pump tank via the acid coolers to the irrigation system of the intermediate absorber.

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Before the SO₃ free gas returns to the heat exchangers T2.120/121, it is freed from droplets by means of a filter. In heat exchangers T2.120/121, the gas is heated to reaction temperature and then conveyed to tray no. 3.

The final absorption of the SO₃ gas is achieved in the final absorber. In heat exchangers T2.140/141, the gas is cooled in such a way, that its temperature is approx. 200 °C at the absorber inlet (at normal laod).

The design of the final absorber corresponds in principle with the design of the drying tower. The product acid is taken as 98.5% H₂SO₄ and is delivered by means of the circuit acid pump to the battery limit. The product acid is cooled in an acid cooler by means of water.

The gas leaving the final absorption tower, passes through a candle-type-filter to minimise acid mists from being entrained in the stack gas.

In the drying tower, the moisture is withdrawn from the SO₂ gas by the acid. To avoid a decrease of the dryer acid concentration, cross flow lines are arranged between the drying tower and the intermediate absorber. In these lines, the diluted acid from the drying flows to the absorber and from the absorber 98.5% is pumped to the drying tower.

As mentioned above, the catalyst only becomes sufficiently active at a temperature of 420 - 450 °C. While during plant operation, the system is in a thermal equilibrium, i.e. the reaction heat produced is sufficient to preheat the incoming cold SO₂ gases and to compensate the unavoidable radiation loss, it is during the plant start-up necessary to preheat the catalyst to the adequate temperature by means of an additional heat source. For this purpose, a preheater is provided, consisting of a combustion chamber with heat exchanger. The burner is supplied with oil by an oil pump and with combustion air through the burner air fan. The air to be preheated is circulated through the heat exchanger, and then enters tray 1 and 3 of the converter.



3.4 Effluents from Plant

Effluents of solid nature will be sludge collected at the settling tank of lyers scrubber unit. This sludge will be collected in a wheel barrow and dumped into the main cinder of the R.1 stream for final disposal. Effluents in gaseous form will be in the form of SO₂ and SO₃/Acid mist for the tail gas chimney of the plant. The conversion efficiency of 99.7 % and the separation efficacy of the candle filters at the AT will ensure that the levels are kept below tolerable limits.

Regarding liquid effluents these will be mainly due to any leaks in the gas cleaning and acid plant sections. The spillage shall be collected via the effluent camals.

A pH-meter in the gully can put an alarm if the water gets too acidic. In that case the water is diverted to a neutralization pit, which has a pump and lime/soda is added to the pit to neutralize. As soon as the water is neutral the pump circulation is changed over to discharge the water into the disposal canal, so as to the join the mine water, for any further treatment etc.



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| 4.1.5 IND | Double deck vibration screen, 1 m width, 2.5 m length, screen decks 10 and 40 mm openings |
| 4.1.6 IND | Belt conveyor, 500 mm width, |

| | Feed bin for ore sorter approx. 2 m³ volume | | | | | |
|---------------|--|--|--|--|--|--|
| | Feed bin for ore sorter approx. 2 m³ volume | | | | | |
| 4.1.9 IND | These items are under the scope of PPCL:- Feeder for ore sorter | | | | | |
| | Ore sorter | | | | | |
| | Feeder for ore sorter | | | | | |
| | Ore sorter | | | | | |
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| 4.1.14 | Reciprocating | feeder v | with | variable | arive, |
|--------|---------------|----------|------|----------|--------|
| IND | width 600 mm | | | | |

- 4.1.15 Reciprocating feeder with variable drive, width 600 mm
- 4.1.16 Belt conveyor, 500 mm width, IND center distance 75 m, lift 8 m
- 4.1.17 Single roller belt weigher IND for belt conveyor 500 mm width
- 4.1.18 Impact crusher
 IND Rotor diameter 1000 mm
 Rotor width 1000 mm
- 4.1.19 Belt conveyor, 500 mm width, center distance 38 m, lift 12 m
- 4.1.20 Double deck vibration screen, IND 2 m width, 5 m length
- 4.1.21 Screen decks 6 and 2 mm openings IND
- 4.1.22 Belt conveyor, 500 mm width, IND center distance 35 m, lift 6 m

- 4.1.23 Vibration feeder, 1000 mm width IND
- 4.1.24 Roller crusher
 IND with two rolls, roll diameter 800 mm, roll width 1000 mm

- 4.1.25 Belt conveyor, 500 mm width, IND center distance 42 m, lift 6 m
- 4.1.26 Belt conveyor, 500 mm width, IND center distance 85 m, lift 19 m
- 4.1.27 Dedusting equipment for IND impact crusher
- 4.1.28 Dedusting equipment for IND screen and roller crusher



4.2 Pyrite Storage and Feed System

4.2.0 Conveyor belt for supply of pyrites
IND from 4.1.26. To reversible conveyor
on top of Bin no. 2 of roasting line
no. 2. Center distance: 25 m, width 500 mm.

4.2.1 Roasting Line 1

- 4.2.1.1 Pyrite feed chute
 IND to feed reversible conveyor on top of
 Feed bin no. 1.
- 4.2.1.2 Reversible conveyor on top of Feed bin no. 1.

 Center distance: 3 m, width: 500 mm.
- 4.2.1.3 Double Discharge Feed Bin IND Volume: approx. 150 cu.m.
- 4.2.1.4 Plastic Lining
 GER for lining the inside walls
 of the bin, with the special
 bolts and washers.

4.2.1.5 2 Discharge belt conveyors

IND with speed variable gear motors and remote control actuators

complete with frame and belts

center distance: 3.6 m, width: 1000 mm

GER: multiply rubber belts

GER: the PIV gear with actuator

4.2.1.6 2 Intermediate belt conveyors IND center distance: 8 m, width 650 mm.

4.2.1.7 2 Feeder belts
IND center distance: 2.2 m, width 650 mm.

4.2.1.8 2 Rotary star feeders
GER with gear motors (constant speed).

4.2.1.9 2 Feed chutes between rotary valves IND and feed pockets of FBR GER partly made of stainless steel.

4.2.2 Roasting Line 2

4.2.2.1 Reversible conveyor on top of Feed bin no. 1.

Center distance: 3 m width: 500 mm

- 4.2.2.2 Double Discharge Feed Bin IND Volume: approx. 150 cu.m.
- 4.2.2.3 Plastic lining

 GER for lining the inside walls of
 the bin, with the special
 bolts and washers.
- 4.2.2.4 2 Discharge belt conveyors

 IND with speed variable gear motors
 and remote control actuators
 complete with frame and belts

Center distance: 3.6 m, width: 1000 mm

GER multiple rubber belts

GER the PIV gear with actuator

- 4.2.2.5 2 Intermediate belt conveyors IND center distance: 8 m, width 650 mm
- 4.2.2.6 2 Feeder belts
 IND center distance: 3.3 m, width 650 mm

4.2.2.7 2 Rotary star feeders
GER with gear motors (constant speed)

4.2.2.8 2 Feed chutes between rotary valves IND and feed pockets of FBR GER partly made of stainless steel.

4.3 Roasting Plant with Waste Heat Boilers

4.3.1 Roasting Line No. 1

4.3.1.1 1 Roaster shell

in gas tight welded design,
made of mild steel plates;

the upper part of the roaster is provided with a gas outlet, which will be connected to the gas inlet of the waste heat boiler, by means of a special designed connection duct.

4.3.1.2 The refractory material

IND for inside lining of the roaster shell; consisting of:

- 2 layers of fire clay bricks, 230 mm thick, each
- 1 layer of insulation brick, 150 mm thick,
- the necessary mortar and water glass;

GER with heat resistant supporting bars and ceramic mats.

4.3.1.3 The thermal insulation material

IND for the outside insulation of the roaster.

4.3.1.4 Nozzles

GER for the roaster grate;

of special design, made of highly heat resistant stainless cast steel including the required electrodes to weld-in nozzles.

4.3.1.5 1 Set of cooling coils

GER connected to the circulating system of the waste heat boiler;

the coils are made of seamless tubes of special design,

supporting bars are made of highly heat resistant material.

4.3.1.6 The large fittings

for the roaster;

comprising:

IND inspection and cleaning doors, sight glasses with accessories,

GER - one wearing plate at the lower cinders outlet,

GER - one shut-off gate at the wind-box outlet.

4.3.1.7 Expansion joints

one arranged at the roaster gas outlet duct, one arranged at the boiler gas outlet duct, qualified for horizontal and vertical expansion.

4.3.1.8 Start-up burner equipment

consisting of:

- oil burners, hinged type including frames and burner bricks, each burner designed for a capacity of 300 kg/h of fuel oil;

IND - oil pump and oil tank;

IND - the necessary oil and air pipes
 with flanges, hangers, bolts, nuts and
 gaskets;

IND - oil filter, including the necessary fittings for the burner equipment.

4.3.1.9 Roaster air blower

GER scroll shell made of welded and bolted steel plates, drain cock at the lowest part of the scroll shell;

included is a guide vane regulation, furthermore a common base plate for blower and motor;

the vane control for the blower;

the regulating rings for common adjustment of all vanes are electrically operated;

the blower will be mounted at vibration absorbers;

the blower will be equipped with two silencers (one for the suction and one for the pressure side).

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GER

4.3.1.10 The duct work

IND for roasting air at suction and pressure side at the blower, as well as flanges and hangers/supporting structure.

4.3.1.11 The air pipelines

IND for the burners, secondary and flushing air, including the necessary flanges and hangers, supporting structure.

4.3.1.12 Hermetic shut-off flap valve (special design)

GER O-ring type,

for the roaster air duct, serving as shut-off valve for blower start-up, with indication "open-closed".

4.3.1.13 Gate valves

IND for burner air, for secondary air, for flushing air.

4.3.1.14 Small parts and accessories

IND consisting of:

flexible hoses: for the oil burners, for the secondary air lines, for the flushing air lines,

bolts, nuts and gaskets.

Waste Heat Boiler Plant

1 Waste heat boiler

the specially designed waste heat boiler with horizontal gas-flow working according to the forced circulation principle;

consisting of:-

4.3.1.15 1 Welded high-pressure boiler drum

IND with heads, manhole and stubs, including all necessary internals and the drum support, including surface attemperator.

4.3.1.16 1 Front-evaporator tube bundle

GER with vertical tube coils, inlet and outlet headers.

4.3.1.17 1 Superheater tube bundle

GER with vertical tube bundles, inlet and outlet headers.

4.3.1.18 Rear-evaporator tube bundles

GER with vertical tube coils, inlet and outlet headers.

4.3.1.19 Interconnecting piping

IND within the forced circulation system of the waste heat boiler up to the turbulent layer cooling coils, including their headers and suspensions.

4.3.1.20 Saturated and superheated steam piping

IND between boiler drum, superheater and pressure regulation station, feed water pump turbine, circulating pump turbine and pressure regulating station.

4.3.1.21 l Blow-down tank
IND with connection flanges for all blowdown
pipes, cooling water connections and
blowdown pipe to the drain.

4.3.1.22 1 Sample cooler
IND for boiler water and saturated steam.

4.3.1.23 Start-up pipe-line

IND with silencer.

4.3.1.24 Supporting structure

IND for the individual removable tube bundles.

4.3.1.25 Boiler casing

IND as brick lined, gas tight welded, corstruction including the necessary stiffeners and suspensions.

4.3.1.26 Boiler steel structure

IND made of mild steel.

4.3.1.27 Large fittings

IND the necessary cleaning openings, inspection doors, measuring holes, sampling branches, etc.

4.3.1.28 Small fittings

IND for the boiler drum, the evaporator and superheater, pressure regulating station; superheated steam temperature regulator, including level indicators, safety valves, non-return valves, pressure gauges and thermometers, as well as vent and drain valves.

4.3.1.29 Circulating pumps

GER 2 Centrifugal pumps
with couplings, guards and common base plates
for pumps and motors or steam turbine and small
fittings.

4.3.1.30 1 Steam turbine

GER to drive the stand-by circulating pump, with automatic starting device and small fittings.

4.3.1.31 1 Special boiler rapping and cleaning device

GER to remote the dust deposits from the boiler tubes with automatic sequence switch centre.

4.3.1.32 Thermal insulation IND

Calcine Handling System

4.3.1.33 1 Single-trough chain conveyor

GER of air-cooled design, arranged underneath the waste heat boiler.

4.3.1.34 1 Double-trough chain conveyor

GER of water-cooled design, for cinder from FBR and boiler.

4.3.1.35 1 Single-trough chain conveyor

GER of water-cooled design, for collecting cinder from all centres.

4.3.1.36 The supporting structure

IND made of sectional steel, for the chain conveyors.

4.3.1.37 1 Cooling air and burner air fan

IND for cooling the chain conveyor and to serve the oil burners of the fluid bed roaster.

4.3.1.39 The cooling air and burner air lines

IND required, including valves for individual air adjustment, including flanges and hangers supports.

4.3.1.39 Rotary star discharger

GER arranged at the calcine outlet of the boiler chain conveyor;

comprising:

water-cooled casing and shaft, the star and the gear motor.

4.3.1.40 2 Roller type shut-off devices for Under- and Overflow

GER 1 electrically operated
1 manually operated,
arranged at the lower fluid bed outlet of the roaster.

4.3.1.41 All connecting chutes

within the calcine handling system,

IND partly made of mild stee!,

GER partly made of highly heat resistant steel, in welded construction,

GER x equipped with inspection/cleaning doors, flanges and necessary x expansion joints.

4.3.1.42 The pipe work for cooling water

IND inside the battery limits, including valves and gaskets, as well as hangers/supports.

4.3.1.43 The pipe word for compressed air

IND inside the battery limits, including shut-off valves and hangers/supports.

4.3.1.44 Small parts

4.3.1.45 1 Cooling and wetting drum

IND consisting of:

drum, shell, inlet- and outlet casing,
rims and running rollers, gear rim, base frame,
drive station, water piping with spray-nozzles,

GER gear box, coupling, lubricating device, wear resistant inside lining.

4.3.1.46 1 Vapour washing system

GER for dedusting the vapour;

consisting of:

casing, flanges, sockets, fittings, etc.

4.3.1.47 1 Vapour discharge fan

IND consisting of:

impeller, shaft, bearing, casing sealing,
base frame, V-belt-drive, guards, etc.

4.3.1.48 1 Vapour discharge piping

IND consisting of:

blow-out stack, connecting ducts, butterfly valves, blind disc, supports etc.

4.3.1.49 1 Louvre type damper

motorized, in the gas duct, leading to scrubbing tower.

4.3.2 Roasting Line No. 2

4.3.2.1 1 Roaster shell

in gas tight welded design,
made of mild steel plates;

the upper part of the reaster is provided with a gas outlet, which will be connected to the gas inlet of the waste heat boiler, by means of a special designed connection duct.

4.3.2.2 The refractory material

IND for inside lining of the roaster shell; consisting of:

- 2 layers of fire clay bricks, 230 mm thick, each
- 1 layer of insulation brick, 150 mm thick,
- the necessary mortar and water glass;
- GER with heat resistant supporting bars and ceramic mats.

4.3.2.3 The thermal insulation material

IND for the outside insulation of the roaster.

4.3.2.4 Nozzles

GER for the roaster grate;

of special design, made of highly heat resistant stainless cast steel including the required electrodes in weld-in nozzles.

4.3.2.5 1 Set of cooling coils

GER connected to the circulating system of the waste heat boiler;

the coils are made of seamless tubes of special design;

supporting bars are made of highly heat resistant material.

4.3.2.6 The large fittings

for the roaster;

comprising:

IND inspection and cleaning doors, sight glasses with accessories,

GER one wearing plate at the lower cinders outlet,

GER one shut-off gate at the wind-box outlet.

4.3.2.7 Expansion joints

GER one arranged at the roaster gas outlet duct, one arranged at the boiler gas outlet duct, qualified for horizontal and vertical expansion.

4.3.2.8 Start-up burner equipment

consisting of:

GER - oil burners, hinged type including frames and burner bricks, each burner designed for a capacity of 300 kg/h of fuel oil;

- the necessary oil and air pipes
with flanges, hangers, bolts, nuts and
gaskets;

IND - oil filter, including the necessary fittings for the burner equipment.

4.3.2.9 Poaster air blower

shell made of welded and bolted steel plates, drain cock at the lowest part of the scroll shell; included is a guide vane regulation, furthermore a common base plate for blower and motor; the regulating rings for common adjustment of all vanes are electrically operated; the blower will be mounted a vibration absorbers; the blower will be equipped with two silencers (one for the suction and one for the pressure side).

4.3.2.10 The duct work

IND for roasting air at suction and pressure side at the blower, as well as flanges and hangers/supporting structure.

4.3.2.11 The air pipelines

IND for the burners, secondary and flushing air, including the necessary flanges and hangers, supporting structure.

4.3.2.12 Hermetic shut-off flap valve (special design)

GER

O-ring type,

for the roaster air duct, serving as shut-off valve for blower start-up, with indication "open-closed".

4.3.2.13 Gate valves

IND

for burner air, for secondary air, for flushing air. 4.3.2.14 Small parts and accessories

IND consisting of:

flexible hoses: for the oil burners, for the secondary air lines, for the flushing air lines,

bolts, nuts and gaskets.

4.3.2.15 Hot Cyclone

IND for operating at temperatures of approx. 900 °C

consisting of

consisting of
mild steel shell,

inside refractory lining, and insulating lining,

external lagging of mineral wool;

GER ceramic mats and special anchor bolts of heat

resistant steel.

4.3.2.16 Gas ducts

IND connecting roaster with hot

cyclone and to the waste heat

boiler inlet nozzle with refractory linings and external lagging.

4.3.2.17 Expansion joints

at the gas ducts

GER for hot operation

made of special ceramic materials,

allowing for vertical and horizontal expansion.

4.3.2.18 Rotary discharger

GER of water cooled design under gas tight conditions, with gear motor, for expulsion of 900 °C hot calcines.

Waste Heat Boiler Plant

l Waste heat boiler

the specially designed waste heat boiler with horizontal gas-flow working according to the forced circulation principle,

consisting of:

4.3.2.19 1 Welded high-pressure boiler drum

IND with heads, manhole and stubs, including all necessary internals and the drum support, including surface attemperator.

4.3.2.20 1 Front-evaporator tube bundle

GER with vertical tube coils, inlet and outlet headers.

4.3.2.21 1 Superheater tube bundle

GER with vertical tube bundles, inlet and outlet headers.

4.3.2.22 Rear-evaporator tube bundles

GER with vertical tube coils, inlet and outlet headers.

4.3.2.23 Interconnecting piping

IND within the forced circulation system of the waste heat boiler up to the turbulent layer cooling coils, including their headers and suspensions.

4.3.2.24 Saturated and superheated steam piping

IND between boiler drum, superheater and pressure regulation station, feed water pump turbine, circulating pump turbine and pressure regulating station.

- 4.3.2.25
 IND
 Blow-down tank
 with connection flanges for all blowdown pipes,
 cooling water connections and blowdown pipe to
 the drain.
- 4.3.2.26 1 Sample cooler
 IND for boiler water and saturated steam.
- 4.3.2.27 Start-up pipe-line

IND with silencer.

4.3.2.28 Supporting structure

IND for the individual removable tube bundles.

4.3.2.29 Boiler casing

IND as bricklined, gas tight welded, construction including the necessary stiffeners and suspensions.

4.3.2.30 Boiler steel structure

IND made of mild steel.

4.3.2.31 Large fittings

IND the necessary cleaning openings, inspection doors, measuring holes, sampling branches, etc.

4.3.2.32 Small fittings

IND for the boiler drum, the evaporator and superheater, pressure regulating station; superheated steam temperature regulator, including level indicators, safety valves, non-return valves, pressure gauges and thermometers, as well as vent and drain valves.

4.3.2.33 Circulating pumps

GER 2 Centrifugal pumps
with couplings, guards and common base
plates for pumps and motors or steam turbine
and small fittings.

4.3.2.34 1 Steam turbine

GER to drive the stand-by circulating pump, with automatic starting device and small fittings.

4.3.2.35 1 Special boiler rapping and cleaning device

GER to remote the dust deposits from the boiler tubes with automatic sequence switch centre.

4.3.2.36 Thermal insulation

IND

Calcine Handling System

4.3.2.37 1 Single-trough chain conveyor

GER of air-cooled design, arranged underneath the waste heat boiler.

4.3.2.38 Rotary cellular cooler

GER for the indirect cooling of calcines, water cooled walls, with 900 °C, all accessories, with gear acid flanged motor.

4.3.2.39 2 Single-trough chain conveyors

GER for transport of cooled calcines to the bucket elevator.

4.3.2.40 1 Bucket elevator

IND vertical design, to transport the calcine receiving from the chain conveyor to the top of the calcine silo.

4.3.2.41 The supporting structure

IND made of sectional steel, for the chain conveyors and for the bucket elevator.



4.3.2.42 1 Cooling air and burner air fan

IND for cooling the chain conveyor and to serve the oil burners of the fluid bed roaster.

4.3.2.43 The cooling air and burner air lines

required,
made of mild steel,
including valves for individual air adjustment,
including flanges and hangers supports.

4.3.2.44 Rotary star discharger

GER arranged at the calcine outlet of the boiler chain conveyor;

comprising:

water-cooled casing and shaft, the star and the gear motor.

4.3.2.45 Roller type shut-off device for Under- and Overflow

1 electrically operated
1 manually operated,
GER arranged at the lower fluid bed outlet of the roaster.

4.3.2.46 Calcine silo

IND consisting of:

- stiffened mild steel plates in various thicknesses,
- sockets for material inlet and outlet.
- 4.3.2.47 Silo shut-off slide valve

GER electrically operated.

4.3.2.48 Fluidization system

IND for conical parts of calcine silo,

consisting of:

pneumatic rapping slides with ring duct, valves and fittings, rotary piston blower and air duct work.

4.3.2.49 Silo filter

IND with cleaning mechanism and centrifugal fan for clean air.

4.3.2.50 All connecting chutes

IND within the calcine handling system, partly made of mild steel,

GER partly made of highly heat resistant steel, in welded construction,

IND equipped with inspection/cleaning doors, flanges and necessary expansion joints.

4.3.2.51 The pipe work for cooling water

IND inside the battery limits, including valves and gaskets, as well as hangers/supports.

4.3.2.52 The pipe work for compressed air

IND inside the battery limits,
 including shut-off valves and
 hangers/supports.

4.3.2.53 Small parts

- I + G such as bolts, nuts, electrodes, gaskets, etc.
- 4.3.2.54 1 Louvre type damper motorized, in the gas duce to scrubbing tower to adjust the suction pressure.

4.3.3 Common Systems for both Lines

1 Feed water plant

consisting of:

- 4.3.3.1 1 Feed water tank
 IND with internal fittings,
 water level indicator, gauges,
 thermometers and small fittings.
- 4.3.3.2 1 Deaerator for the deaeration of the feed water.
- 4.3.3.3 1 Stream pressure control device for keeping the deaerator pressure constant.
- 4.3.3.4 1 Water flow control for keeping the water level in the feed water tank constant.
- 4.3.3.5

 2 Feed water pumps
 (centrifugal pumps),
 each with coupling, guard and common base
 plate for the pump and motor or steam turbine
 and small fittings.

- 4.3.3.6 1 Steam turbine

 GER for the drive of the stand-by feed water pump, with small fittings.
- 4.3.3.7 1 Reducing station for steam to deaerator
- 4.3.3.8 1 Sample cooler IND for feed water
- 4.3.3.9 Interconnecting piping
 - IND condensate pipe from condensate pumps to deaerator
 - feed water pipe from boiler feed water tank to boiler feed water pumps
 - vent and drain pipes
- 4.3.3.10 1 Dosing equipment for deaerator with dosing pump and PVC-tank.
- 4.3.3.11 Thermal insulation for the parts of the feed water plant.

4.3.3.12 Set interconnectiong piping

IND - feed water pipe from feed water
 pumps to each steam drum

 feed water pipe for injection water from feed water pumps to spray-in cooler.

Hot Steam Piping

4.3.3.13 1 Set superheated steam piping between pressure regulating stations to the turbine inlet controller.

1 Re-cooling plant

consisting of:

- 4.3.3.14 2 Cooling towers
 IND with tower fill,
 water distribution system,
 drift eliminator.
- 4.3.3.15 1 Cold water basin reinforced concrete
- 4.3.3.16 4 Axial fans
 IND with couplings
 direct driven by c-motor

4.3.3.17 2 Centrifugal pumps

IND with couplings and common base plates for pumps and motors.

4.3.3.18 Interconnecting piping

IND - cooling water suction pipe

 cooling water pipe from cooling water pumps to condensers

 return cooling water pipe from condensers to cooling tower

4.3.3.19 1 Water treatment plant

IND only for make up water (BFW)

consisting of the necessary equipment to guarantee the quality of boiler feed water.

4.3.3.20 1 Demin. water tank
IND with connection flanges

4.3.3.21 2 Demin. water pumps
IND with couplings and common base plates for pumps and motors.

4.3.3.22 Interconnecting piping

IND - pipes within the plant for water and chemicals

 demin. water pipe from water treatment plant to demin. water pumps

- demin. water discharge pipe from demin. water pumps to dearator.

4.4 Gas Cleaning Plant

- 4.4.1 Cyclone and Hot Precipitator Lines
- 4.4.1.1 1 High-efficiency Centrifugal Dust Collector (Cyclone)

IND each made of sheet steel with gas inlet connection duct and gas outlet connection duct with flanges for fastening the incoming and outgoing gas ducts, with dust hopper, including flange at the outlet for the connection of the dust expulsion system, included all the required bolts and gaskets, as well as the support brackets.

- 4.4.1.2 the dust expulsion system
- GER consisting of one rotary valve with motorized drive, arranged beneath the hopper of cyclone.
- 4.4.1.3 the material for the thermal insulation of each cyclone
- IND consisting of insulation mats of 100 mm thickness and of a protective aluminium sheet covering.



Electrostatic Hot Gas Precipitator

4.4.1.4 Precipitator Casing with Ancillaries

- IND I casing for the horizontal type electrostatic precipitator of 5 mm steel plate construction, with stiffeners for a max. suction of 30 mbar and a max. temperature of 380 °C; the casing would extend from raw gas inlet up to clean gas outlet and would comprise:
 - one longitudinal hopper with connection flange for dust conveyor,
 - box type roof beams for supporting the precipitator roof and the collecting electrodes and to accommodate the H.T.-insulators for the discharge electrode suspension,
 - precipitator top allowing transit,
 - inspection doors with clamp down device,
 - catwalk on one precipitator longside, with open mesh flooring, including railings;
- IND gas inlet and gas outlet transition of 5 mm steel plate construction with stiffeners;
- IND gas distribution plates at precipitator inlet;
- IND precipitator support structure,
 consisting of the lattice type construction
 with movable supports;
 the precipitator casing is considered as load
 bearing member, the lattice ties transmitting
 the wind forces into the foundations;

IND - 150 mm thick heat insulation for precipitator casing and associated gas inlet and outlet transitions. The heat insulation would consist of mats, attached to galvanized wire netting and covered on the outside by a 1 mm thick aluminium sheeting. Included are seam cover strips and self-tapping screws.
 The heat insulation for the precipitator roof would be 250 mm thick, without metal sheeting;

GER 1 motorized dust conveyor underneath the precipitator hopper, with geared motor;

1 motorized rotary dust valve at dust outlet of the
dust conveyor, with geared motor;

IND - the mechanical interlocking system for the high voltage switches and the doors of the electrostatic precipitator.

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4.4.1.5 The Internal Equipment for the Precipitator

comprising:

GER - discharge electrodes;

GER - frames for the discharge electrodes;

GER - high voltage insulators
 for the suspension system and support;

GER - control and monitoring instruments
for connection to plant voltage,
including branch sockets and heat-resistant
junction lines from the sockets to the heating
bodies;

GER - collecting electrodes
 with guides and upper spacers;

GER - rapping rods;

GER - motorized rappers for the discharge system, including geared motors;

GER - motorized rappers
for the collecting electrodes,
including geared motors.



4.4.1.6 The Electrical Equipment

(corresponding to the relevant GERMAN-regulations)

GER 2 single-phase transformer-rectifier sets as per VDE 0146, provided for being installed in an enclosed high voltage room,

each with the following data:

power supply : 415 V, 50 cps

connection value : 35 kVA *)

signal voltage : 220 V, 50 cps

nominal high voltage : 50 kV ar.

nominal output current : 560 mA *)

ambient temperature : 40 °C

*) the exact date depends upon the make to be supplied.

Each plant comprises:

- a control cabinet in sheet metal design, with built-in thyristor controller, solid-state automatic control of precipitator operation and all switching and monitoring equipment required for operation. The ON-OFF-switches, the signal lamps ON and FAILURE, as well as the measuring equipment for the current and voltage values on the primary and secondary side are arranged in the front door.

The cabinet is suitable for the connection up to remote control and remote monitoring system. All internals are accessible from the front and exchangeable. The cable intake is from below.

Enclosure:

at least IP 20 RAL 7032



- a hermetically sealed rectifier set with the following oil-immersed parts:

high voltage transformer with a rectifier set with silicone diodes; throttle on the low voltage side for current limitation and improvement of the form factor; high frequency throttle or Ohmic resistance for attenuating the high frequency peak voltages on the direct current side, as well as a measuring resistance for connecting the measurement system of the secondary voltage and for the kV-measurement.

The required monitoring equipment is mounted on the vessel cover. There is a shunt for the measurement of the precipitator current in the earthed conductor next to the secondary voltage measurement in the laterally arranged terminal box. The direct current connection is effected via a high voltage bushing, which can be arranged vertically or horizontally.

Enclosure:

- Terminal box : IP 65 IP 43 - High voltage bushing: IP 00

Colour RAL 7033

The electrical installation material

comprising:

GER - high voltage switches with manual actuation for change-over and earthing;

for the high voltage cells
in the form of wire grates
and access doors;

GER - cabling of the units on the low voltage side with interlocking of the cell doors, including warning lights;

GER - the copper earth wires
in the area of the electrostatic precipitator
plant, as well as in the area of the switching and
unit cells,
for connection to the works earth;

GER - earthing equipment,
 i.e. earth rods and earth wires;

GER - attenuating systems;

GER - 100 m single core high voltage cable,
for connecting the high voltage switches
with the electrostatic precipitator,
including terminal boxes and fastening
material. (We will invoice the supply of
additional cables for the respective current
price);

GER - bushing insulators;

GER - 1 switchboard control panel totally enclosed, enclosure IP 44, completely mounted and wired to the terminal board, ready for connection. The board comprises all required switching, monitoring and operating devices for the auxiliary equipment of the electrostatic precipitator plant listed below: **GER** supply via low voltage high breaking capacity fuse, GER outlets for transformer rectifier sets, **GER** motorized rappers for the discharge system, GER motorized rappers for the collecting electrodes, GER motorized rappers for the gas distribution plates, GER electrical heating system for the insulators, dust expulsion device (included rotary dust **GER** walves of the cyclone).

4.4.1.7 Gas Shut-off Devices

IND consisting of a cast iron damper, arranged at the gas inlet and outlet HGP designed for manual operation.



4.4.2 Hot Precipitator Line 2

Electrostatic Hot Gas Precipitator

4.4.2.1 Precipitator Casing with Ancillaries

IND 1 casing for the horizontal type electrostatic precipitator of 5 mm steel plate construction, with stiffeners for a max. suction of 30 mbar and a max. temperature of 380 °C; the casing would extend from raw gas inlet up to clean gas outlet and would comprise:

- one longitudinal hopper with connection flange for dust conveyor,
- box type roof beams for supporting the precipitator roof and the collecting electrodes and to accommodate the H.T.-insulators for the discharge electrode suspensions,
- precipitator top allowing transit,
- inspection doors with clamp down device,
- catwalk on one precipitator longside, with open mesh flooring, including railings;

IND - gas inlet and gas outlet transition of 5 mm steel plate construction with stiffeners;

IND - gas distribution plates at precipitator inlet;

GER - motorized rapper for gas distribution plates, including geared motor;

- precipitator support structure,
consisting of the lattice type construction
with movable supports;
the precipitator casing is considered as load
bearing member, the lattice ties transmitting
the wind forces into the foundations;

- 150 mm thick heat insulation for precipitator IND casing and associated gas inlet and outlet transitions. The heat insulation would consist of mats, attached to galvanized wire netting and covered on the outside by a 1 mm thick aluminium sheeting. Included are seam cover strips and self-tapping screws. The heat insulation for the precipitator roof

would be 250 mm thick, without metal sheeting;

1 motorized dust conveyor underneath the precipitator hopper, with geared motor;

1 motorized rotary dust valve at dust outlet of the GER dust conveyor, with geared motor;

IND - the mechanical interlocking system for the high voltage switches and the doors of the electrostatic precipitator.

GER

4.4.2.2 The Internal Equipment for the Precipitator

comprising:

GER - discharge electrodes;

GER - frames for the discharge electrodes;

GER - high voltage insulators
 for the suspension system and support;

GER - electric heating system
 for the high voltage insulators;

GER - control and monitoring instruments
for connection to plant voltage,
including branch sockets and heat-resistant
junction lines from the sockets to the
heating bodies;

GER - collecting electrodes
 with guides and upper spacers;

GER - rapping rods;

GER - motorized rappers for the discharge system, including geared motors;

GER - motorized rappers
for the collecting electrodes,
including geared motors;

GER - the rapping cycle control
for the third field
for controlling the motorized plate
rapping mechanisms.



4.4.2.3 The Electrical Equipment

(corresponding to the relevant GERMAN-regulations.)

GER 3 single-phase transformer-rectifier sets as per VDE 0146, provided for being installed in an enclosed high voltage room,

each with the following data:

power supply 415 V, 50 cps

: 35 kVA *) connection value

signal voltage : 220 V, 50 cps

nominal high voltage : 50 kV ar.

560 mA nominal cutput current :

ambient temperature : 40 °C

*) the exact data depends upon the make to be supplied.

Each plant comprises:

- a control cabinet in sheet metal design, with built-in thyristor controller, solid-state automatic control of precipitator operation and all switching and monitoring equipment required for operation. The ON-OFF-switches, the signal lamps CN and FAILURE, as well as the measuring equipment for the current and voltage values on the primary and secondary side are arranged in the front door.

The cabinet is suitable for the connecting up to remote control and remote monitoring system. All internals are accessible from the front and exchangeable. The cable intake is from below.

Enclosure : at least IP 20

Colour RAL 7032



- a hermetically sealed rectifier set with the following oil-immersed parts:

High voltage transformer with a rectifier set with silicone diodes; throttle on the low voltage side for current limitation and improvement of the form factor; high frequency throttle or Ohmic resistance for attenuating the high frequency peak voltages on the direct current side, as well as a measuring resistance for connecting the measurement system of the secondary voltage and for the kV-measurement.

The required monitoring equipment is mounted on the vessel cover. There is a shunt for the measurement of the precipitator current in the earthed conductor next to the secondary voltage measurement in the laterally arranged terminal box. The direct current connection is effected via a high voltage bushing, which can be arranged vertically or horizontally.

Enclosure:

- Vessel : IP 65 - Terminal box : IP 43 - High voltage bushing: IP 00

Colour : RAL 7033

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The electrical installation material

comprising:

- GER high voltage switches with manual actuation for change-over and earthing;
- GER connection ducts
 on the high voltage side
 with terminal and support insulators;
- IND protective covering
 for the high voltage cells
 in the form of wire grates
 and access doors;
- IND cabling of the units on the low voltage side with interlocking of the cell doors, including warning lights;
- GER the copper earth wires
 in the area of the electrostatic precipitator
 plant, as well as in the area of the switching and
 unit cells,
 for connection to the works earth;
- GER earthing equipment,
 i.e. earth rods and earth wires;
- GER attenuating systems;
- GER 150 m single core high voltage cable,
 for connecting the high voltage switches
 with the electrostatic precipitator,
 including terminal boxes and fastening material.
 (We will invoice the supply of additional cables
 for the respective current price);
- GER bushing insulators.

- 1 switchboard control panel totally enclosed, enclosure IP 44, completely mounted and wired to the terminal board, ready for connection. The board comprises all required switching, monitoring and operating devices for the auxiliary equipment of the electrostatic precipitator plant listed below:

supply via low voltage high breaking capacity fuse,

outlets for transformer rectifier sets,
motorized rappers for the discharge system,
motorized rappers for the collecting electrodes,
motorized rappers for the gas distribution
plates,
electrical heating system for the insulators,

4.4.2.4 Gas Shut-off Device

consisting of a cast iron damper, arranged at the gas outlet, designed for manual operation.

dust expulsion devices.

4.4.3 Common Gas Cleaning Plant

4.4.3.1 1 Washing Tower

consisting of:

IND mild steel casing;

IND rubber lining;

IND acid resistant bricks and mortar for bricklining;

GER requisite acid nozzles with nozzle tubes;

IND support structure made of sectional steel;

IND service platform and stairway, floors and handrails, made of sectional steel.

4.4.3.2 1 Settling Tank

consisting of:

IND mild steel casing / or plastic

with conical bottom,

including flanges, bolts and gaskets;

IND support structure

made of sectional steel,

including ladder.

4.4.3.3 2 Pump Tanks

IND

consisting of:

plastic with flanges bolts and gaskets;

(for washing Tower and Starcooler circuits).

4.4.3.4 2 Centrifugal Pumps

ER

(1 operating, 1 stand-by pump for washing Tower circuit),

designed for direct motor coupling with base plates, anchoring elements, flexible couplings and motors.

4.4.3.5 1 <u>SO₂-stripper</u>

IND

made of plastic;

IND - the rings for packing
 including the grid made of plastic;

IND 1 damper for manual operation made of plastic;

IND - the required flanges, bolts and gaskets.

4.4.3.6 1 Humidifier Tower

designed as a pump tank,
with gas outlet connection duct;

GER - spraying system
consisting of nozzle pipes and nozzle,
both made of plastic for installation
inside the Humidifier top.

4.4.3.7 4 Centrifugal Pumps

GER

(2 operating and 2 stand-by pump for humidifier tower and gas cooler circuit or for wet precipitator flushing),

designed for direct motor coupling with base plates, anchoring elements, flexible couplings and motors.

4.4.3.8 1 Indirect Gas Cooler

dcuble section model with vertical gas passage, consisting of:

GER

2 cooling bundles, arranged one above the other;

each bundle composed of:

- shell welded to upper and lower tube plates, which are homogeneously lead lined steel on the gas side; shell inside provided with a multiple paint coating for protection against corrosion;
- lead tubes with inside (gas side) provided with longitudinal fins, arranged in star pattern; the tubes soldered into the tube plates;
- cooling water baffles, made of plastic;
- water supply and drain nozzles;
- IND cooler midsection between steel tube bundles, homogeneously lead lined on the inside;
- IND all necessary flanges, bolts and gaskets;
- IND supporting structure of steel beam design;
- GER spraying system,
 consisting of nozzle pipes and nozzles
 both made of plastic for installation
 inside the cooler top.

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4.4.3.9 3 Electrostatic Wet Gas Precipitators

tubular wet gas precipitators, partly in plastic construction, two units are arranged in the first and one in the second stage:

each precipitator consisting of:

IND

- the casing

made of fibre glass reinforced plastic
(FRGRP);

IND

the casing top with:

- the gas inlet connection, respectively the gas outlet connection;
- the connections for the insulator housings;
- the connections for the flushing device;
- the gas distribution plates, made of plastic, including supports (only for the second stage unit);
- the inspection and clean-out manholes, as well as the inspection glasses with the required seals.

IND

the casing centre with:

- the top plastic tube sheet for accommodation of the collecting tubes;
- the support grate for the tube sheet, made of homogeneously lead coated steel;
- the plastic grate for central alignment and guiding of the bottom ends of the collecting tubes.

IND

the casing bottom with:

- the gas outlet connection, respectively the gas inlet connection;
- the gas distribution plates,
 made of plastic,
 including supports (only for the first
 stage units);
- the connections for the insulator housings;
- the inspection and clean-out manholes, as well as the inspection glasses with the required seals.

GER

- the collecting tubes

made of plastic with welded collar and O-ring seal.



4.4.3.10 - the high tension section GER

IND - the upper frame
 for supporting and spacing the discharge
 electrodes,
 made of homogeneously lead coated
 steel;

IND - the lower frame for guiding and spacing the discharge electrodes, made of homogeneously lead coated steel;

GER - the insulators
for supporting the discharge system,
as well as the current intake.

4.4.3.11 The Insulator Housing

each consisting of:

IND - the lower part
 made of homogeneously lead coated steel
 to accomodate the insulators;

IND - the 100 mm thick heat insulation with a 1 mm thick aluminium plate protective cover.

4.4.3.12 The Electrical Equipment GER

(corresponding to the relevant GERMAN regulations.

GER

3 single-phase transformer-rectifier sets as per VDE 0146, provided for being installed in an enclosed high voltage room,

each designed for the following data:

power supply : 415 V, 50 cps

connection value : 27 kVA *)

signal voltage : 220 V, 50 cps

nominal high voltage : 40 kV ar.

nominal output current : 560 mA *)

ambient temperature : 40 °C

*) the exact data depends upon the make to be supplied.

each plant comprises:

- a control cabinet in sheet metal design, with built-in thyristor controller, solid-state automatic control of precipitator operation and all switching and monitoring equipment required for operation. The ON-OFF-switches, the signal lamsp ON and FAILURE, as well as the measuring equipment for the current and voltage values on the primary and secondary side are arranged in the door front.

The cabinet is suitable for the connection up to remote control and remote monitoring system. All internals are accessible from the front and exchangeable. The cable intake is from below.

Enclosure: at least IP 20

Colour : RAL 7032:

- a hermetically sealed rectifier set with the following oil-immersed parts:

High voltage transformer with a rectifier set with silicone diodes; throttle on the low voltage side for current limitation and improvement of the form factor; high frequency throttle or Ohmic resistance for attenuating the high frequency peak voltages on the direct current side, as well as a measuring resistance for connecting the measurement system of the secondary voltage and for the kV-measurement.

The required monitoring equipment is mounted on the vessel cover. There is a shunt for the measurement of the precipitator current in the earthed conductor next to the secondary voltage measurement in the laterally arranged terminal box. The direct current connection is effected via a high voltage bushing, which can be arranged vertically or horizontally.

Enclosure:

- Vessel : IP 65 - Terminal box : IP 43 - High voltage bushing: IP 00

Colour : RAL 7033.



The Electrical Installation Material

comprising:

GER - high voltage switches with manual actuation for change-over and earthing;

GER - connection ducts on the high voltage side with terminal and support insulators;

IND - protective covering
 for the high voltage cells
 in the form of wire grates
 and access doors;

IND - cabling of the units on the low voltage side with interlocking of the cell doors, including warning lights;

GER - the copper earth wires
in the area of the electrostatic precipitator
plant, as well as in the area of the switching
and unit cells,
for connection to the works earth;

GER - earthing equipment,
 i.e. earth rods and earth wires;

GER - attenuating systems;

GER - 150 m single core high voltage cable, for connecting the high voltage switches with the electrostatic precipitators, including terminal boxes and fastening material. (We will invoice the supply of additional cables for the respective current price);

GER - bushing insulators;

- 1 switchboard control panel totally enclosed, enclosure IP 44, completely mounted and wired to the terminal board, ready for connection. The board comprises all required switching, monitoring and operating devices for the auxiliary equipment of the gas cleaning plant listed below:

supply via low voltage high breaking capacity fuse,

outlets for transformer rectifier sets, compressors,

pumps.

4.4.3.13 The Equipment for flushing the Insulators with heatead Air

comprising:

- GER the required compressors with electrical drives;
- GER the required air filters with filter inserts;
- GER the required compensators;
- IND the air ducts
 between compressors and insulators,
 made of steel with the required fastening
 material and the heat insulation.



4.4.3.14 The Equipment for the Filter flushing with Wash Liquor

GER - the required nozzles and nozzle tubes
 made of plastic;

IND - the plastic piping
 for distribution of the flushing líquid;

IND - the required shut-off valves
 for manual control.

4.4.3.15 The Gas Shut-Off Devices IND

consisting of five throttles and slip plates on the gas inlet side and the gas outlet side of each precipitator for manual operation, made of plastic.

4.4.3.16 Support Structures, Platforms and Stairways

IND the precipitator support structure welded of structural steel;

IND the precipitator platforms with protective railing and stairways, including supports.

4.4.3.17 Ducts and Pipelines

consisting of:

IND - gas connection ducts
from the outlet of the cyclone to the
inlet of the washing tower,
made of steel,
including supports, expansion joints,
flanges, bolts and gaskets;

IND - thermal insulation for the hot gas duct, 100 mm thick, bound with galvanized wire mesh and protected on the outside with aluminium cladding, 1 mm thick;

IND - gas connection ducts
 from the outlet of the washing tower to
 the inlet of the drying tower, as well as
 to the start-up stack,
 made of plastic with steel reinforcements,
 including supports, flanges, bolts and
 gaskets;

IND compensators;

IND safety valve;

IND operating platform and ladder for safety valve, made of sectional steel;

IND - pressurized acid lines,
 made of rubber lined steel / or plastic,
 including flanges, bolts, gaskets and supports;

IND - valves and sight glasses for acid lines;

IND - water lines,
 made of seamless mild steel piping,
 vith valves, flanges, bolts, gaskets and supports.

4.4.3.18 Start-up Devices

IND 1 radial compressor
steel rubber-lined, (or PVC/FRP)
designed for direct motor coupling,
with base plate, anchoring elements,
flexible coupling and motor;

IND 1 start-up stack made of PVC/FRP.

4.5 Sulphuric Acid Plant

4.5.1 Drying-, Absorption- and Production Section

4.5.1.1 1 Air Filter

for filtering the required dilution air; consisting of:

a mild steel casing with filter mats.

4.5.1.2 1 Drying Tower

The drying tower is working according to the counterflow-irrigation system;

consisting of:

IND The cylindrical shell of mild steel in welded construction, with dished bottom, gas-inlet, gas-outlet and acid in- and outlets. The gas outlet with cover and bend will be made of stainless steel. Bottom and shell will receive a multi-layer acid resistant lining; before bricklining with acid bricks a plastic foil will be provided in the lower area.

GER Before the gases are leaving the drying tower. they pass a wire mesh <u>filter</u>.

For uniform distribution of acid over the entire cross section of the tower, an irrigation system, made of special designed cast iron pipes, is arranged.

The acid is fed to the irrigation system by means of cast iron pipes.

IND A filling, consisting of INTALOX-saddles, which will be supported by a special grate, all made of acid resistant stone ware, will be provided for the irrigation tower.

Above the INTALOX-saddles, a filter will be provided.

The drying tower will be also equipped with sight glasses.

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4.5.1.3 1 Intermediate Absorption Tower

IND+GER

consisting of:

IND

The cylindrical shell of mild steel in welded construction, with dished bottom, gas-inlet, gas-outlet and acid in- and outlets.

Bottom and shell will receive a multi-layer acid resistant lining.

GER

Before the gases are leaving the intermediate absorption tower, they pass a wire-mesh-filter, arranged in the upper part.

For distribution of acid over the entire cross section of the absorption tower, irrigation pipes, made of special designed cast iron, are arranged.

The acid is fed to the irrigation system by means of cast iron pipes.

The cover, as well as the gas outlet socket with elbow, are made of stainless steel.

A filling, consisting of INTALOX-saddles, made of acid resistant stone ware, will be provided for the intermediate absorption tower.

The absorption tower will be also equipped with sight glasses and 1 mechanical level indicator for measuring the acid level in the lower part.

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4.5.1.4 1 Final Absorption Tower

consisting of:

IND

The cylindrical shell of mild steel in welded construction, with dished bottom, gas-inlet, gas-outlet and acid in- and outlets.

Bottom and shell will receive a multi-layer acid resistant lining.

Before the gases are leaving the final absorption tower, they pass a wire mesh <u>filter</u>, arranged in the pper part.

GER

For uniform distribution of acid over the entire cross section of the tower, an irrigation system, made of specially designed cast iron pipes, is arranged.

The acid is fed to the irrigation system by means of cast iron pipes.

The cover of the gas outlet with dome and elbow will be made of stainless steel.

A filling, consisting of INTALOX-saddles, made of acid resistant stone ware, will be provided for the final absorption tower.

The absorption tower will be also equipped with sight glasses and one mechanical level indicator for measuring the acid level in the lower part.

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4.5.1.5 3 Pump Tanks

IND one tank for the drying tower circuit, one tank for the intermediate absorption circuit, one tank for the final absorption circuit,

each consisting of:

a vertical cylindrical shell with vaulted bottom, made of mild steel;

the acid resistant lining material, as well as a mechanical level indicator;

branches are provided for acid filling, acid pumps, circulating acid and level indicator.

4.5.1.6 - Water Injectors

GER for the addition of dilution water, made of teflon-coated steel, will be provided for the intermediate absorption tower and final absorption tower, one for each tower.

4.5.1.7 - The Acid Coolers

IND for the drying tower circuit.

4.5.1.8 - The Acid Coolers

IND for the intermediate absorption— and final absorption circuits and production acid.

4.5.1.9 - The Gas Ducts

GER

in welded steel construction within the drying and IND absorption section for air, SO₂- and SO₃-gases, incl. the necessary expansion joints with lift limitations, as well as blind flanges/shut-off plates;

Material

mild steel, for gas ducts: partly:

partly: boiler plate, heat resistant partly:

steel,

plastic (for partly:

dilution air

only)

IND/GER Expansion joints: partly: boiler plate,

partly:

stainless steel;

flanges

for stainless steel expansion joints:

mild steel.

4.5.1.10 - Butterfly Damper

IND one for gas tight design, manually operated;

IND one for atmospheric dilution air, made of plastic material, motor-operated;

> two for SO₂/SO₃-gases, made in welded steel construction; manually operated by hand-wheel or sprocket wheel with chain.

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4.5.1.11 - The Acid Pipe Lines

mainly of acid resistant cast iron,

ger partly made of enamelled cast iron,
partly made of mild steel welded tubes.

4.5.1.12 - The Acid Valves

GER of acid resistant material, designed for the various temperatures and concentrations of acid to serve;

- bcdy, cover and gate, all made of stainless steel cast,
- hand wheel, made of ordinary cast iron.

4.5.1.13 - The sight Glasses

IND for observing the flow of acid, the sight glasses, made of pressed hard glass, fitted in acid resistant cast iron bodies.

4.5.1.14 - The Lines

IND for dilution water, as well as one small level tank, including fittings and valves, made of mild steel.

4.5.1.15 - The Density-Meter Feed- and Discharge Pipes

IND incl. accessories,

as well as the analysis and pressure measuring pipes,

including valves and accessories,

all made of stainless steel.

4.5.1.16 - The Vent Pipes

IND

made of mild steel.

4.5.1.17 - The Water Pipelines

IND for cooling water,

made of mild steel,

including valves, to connect the acid coolers of the various circuits with the feed pipe for the cooling water at battery limits.

4.5.1.18 2 Wire-Mesh-Filters

GER - cne filter,

arranged in the drying tower.

Materials:

hostaflon knitmesh and stainless steel top and bottom structure;

bottom structure,

- one wire-mesh filter, arranged in the intermediate absorber, in one-stage design.

Materials:

hostaflon knitmesh and stainless steel top and

bottom structure.

4.5.1.19 1 Candle Type Filter

GER arranged in the top of the final absorption tower, material: glass fibre in stainless steel cages

4.5.1.20 - Instrument Air Pipes

IND made of stainless steel, as well as the necessary ball valves, also made of stainless steel.

4.5.1.21 - Lifting Equipment

IND 2 hoists, manually operated,
- 1 for serving the shut-off plate,
- 1 to serve the acid pumps.

4.5.1.22 - The Ladders, Platforms and Handrails

IND within the drying and absorption section, for the irrigation towers and pump tanks, made of welded sectional steel construction; flooring for platforms, made of galvanized grate.

4.5.1.23 - The Supports

IND made of steel sections for the gas-, acid- and other ducts and pipe lines within the drying and absorption section.

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4.5.1.24 - The Supports and Platforms

IND with ladder, for dilution water level tank.

4.5.1.25 - The supporting Beams and Gantries IND

for the cable tray system and lifting equipment.

4.5.1.26 - The required small Materials

consisting of bolts, nuts, packings, glass ware, etc.

- 4.5.1.27 The Insulation IND
 - for acoustic purposes
 for the gas ducts on the inlet side,
 as well as on the outlet side,
 of the SO₂-gas compressor;
 - for thermal purposes for the duct from the intermediate absorption tower to the intermediate heat exchanger, as well as for the duct from the heat exchanger II to the final absorption irrigation tower;

consisting of mineral wool plankets and a 1 mm aluminium cover sheeting.

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4.5.1.28 - Emergency Showers

arranged near the acid pumps within the drying and absorption section,

including eye-washers, to be op rated by hand or foot.

4.5.1.29 - Centrifugal Acid Pumps GER

vertical design,

for the following duties:

- 1 vertical pump
 for the drying tower circuit,
- 1 vertical pump
 for the intermediate absorption circuit,
- 1 vertical pump
 for the final absorption circuit,
- 1 vertical pump for the production acid.

The above mentioned pumps will be Chemical Process Pumps for concentrated sulphuric acid.

The material for the pumps will be provided for the actual temperatures and concentrations, including flexible couplings with guards.

The pumps are provided for electrical motor drive.

4.5.1.30 1 SO₂-Gas Blower GER

Medium:

gas with approx. 8 % SO₂

Details of Design

Single-inlet centrifugal compressor with open impeller in overhung position;

consisting of:

Scroll housing horizontally split, made of cast iron;

Transition diffuser on the outlet;

Open steel impeller with forged impeller body and welded-on, radially ending blades;

Shaft;

Shell at the shaft passage through the blower housing, horizontally split, designed as carbon ring sealing with sealing gas connection;

Welded steel bearing pedestal with integral sleeve bearings. Bearing pedestal and sleeve bearings horizontally split; common lubrication.

Bar thermometers to control the bearing temperatures;

The coupling between blower and turbine, (coupling guards included);

The base frame to receive the fan and the turbine of fabricated welded construction using mild steel plates and sections;

- Oil Supply Equipment

water oil cooler, oil filter, electric gear oil pump for starting and stand-by, oil manometers, oil thermometers, pressostat, oil reservoir (arranged in the base frame), oil piping and the required fittings flow detector;



1 Sound Absorging Hood

to reduce the noise level to 85 dB(A), measured at a distance of 2 m from the hood;

the hood is equipped with a forced ventilation system.

4.5.1.31 1 Final Gas Stack IND -----

in self-supporting structure;

Material:

mild steel;

top of stack will be made of

stainless steel.



Converter Group

4.5.1.32 1 Tray Type Converter IND

The converter consists of a stiffened shell made of boiler plate and heat resistant steel; acid resistant lining material is provided for the protection of the shell; all parts of the shell, top cover and gas in- and outlets not bricklined, which come into contact with hot gases above 420 °C will be spraycoated with aluminium after sand blasting, where boiler plate is utilized only.

For reaching every individual tray for inspection purposes, the shell is equipped with two manholes for each tray. Inside the converter four trays will be provided to receive the catalyst material.

The converter comprises:

GER(partly) the shell,
partly made of boiler plate,
partly made of heat resistant steel
with flat bottom, conical top;

rectangular gas inlets and gas outlets with manholes above all travs;

GER(partly) the trays are made of perforated heat resistant materials;

the bricklining materials for lining the complete converter shell and bottom with one layer of bricks; the material used will be an acid resistant brick;

the necessary mortar for bricklining the convertor, viz. potassium silicate and water glass.

4.5.1.33 - Vanadium containing Catalyst IND

of different hardnesses.

4.5.1.34 - RASCHIG-rings 25 x 25 x 3 mm

IND

made of ceramic material as covering layer for the catalyst.

4.5.1.35 - INTALOX-saddles 3/4" IND ------

made of ceramic material as supporting layer for the catalyst.

4.5.1.36 1 Heat Exchanger I

IND

for heating up the preheated gases coming from the heat exchangers IV by means of the gases coming from the first layer of catalyst of the converter; operating in accordance with the cross current principle;

the heat exchanger comprises:
a straight bottom,
a cylindrical lower and upper part,
an intermediate part with tubes and tube plates,
expansion joint with guide plates, as well as gas
inlet and outlet;

the bottom of the heat exchanger will be lined with one layer of acid resistant bricks, for protection against condensate;

the tubes of the heat exchanger are made of mild steel.



4.5.1.37 2 Heat Exchangers II

IND

for heating up the preheated gases coming from the intermediate absorption by means of the gases coming from the second layer of catalyst of the converter; operating in accordance with the cross current principle;

each heat exchanger comprises:
a straight bottom,
a cylindrical lower and upper part,
an intermediate part with tubes and tube plates,
expansion joint with guide plates, as well as gas
inlet and outlet;

the bottom of the heat exchanger will be lined with one layer of acid resistant bricks, for protection against condensate;

the gas-inlet chambers will be spray-coated with aluminium after sand blasting, the tubes of the heat exchanger are made of mild steel.

4.5.1.38 1 Heat Exchangers IV

IND

for heating up the gases coming from the drying tower by means of the gases coming from the fourth layer of catalyst of the converter; operating in accordance with the cross current principle;

the heat exchanger comprises:
a straight bottom,
a cylindrical lower and upper part,
an intermediate part with tubes and tube plates,
expansion joint with guide plates, as well as gas
inlet and outlet;

the bottom of the heat exchanger will be lined with one layer of acid resistant bricks, for protection against condensate;

the tubes of the heat exchanger are made of mild steel.



4.5.1.39 1 Heat Exchanger III

IND

for preheating the gases coming from the SO₂-gas blower by means of the gases coming from the third layer of catalyst; operating in accordance with the cross current principle;

the heat exchanger comprises:
a straight bottom,
a cylindrical lower and upper part,
an intermediate part with tubes and tube plates,
expansion joint with guide plates, as well as gas
inlet and outlet;

the bottom of the heat exchanger will be lined with one layer of acid resistant bricks, for protection against condensate;

the tubes of the heat exchanger are made of mild steel.

4.5.1.40 - Preheater Unit

consisting of:

IND

- refractory lined combustor, complete with oil burner and flue gas distribution ring;
- tube bundle
 with refractory lined casing;
- combustion air fan;
- combustion controls as required for the system.

The preheater unit will be designed for initial preheating of the converter system, including catalyst for start-up purposes, as well as reheating after idle operations.

4.5.1.41 - The Oil Piping

IND for the preheater unit;

for the connection from battery limits to the oil pump and the oil pump to the oil burner, including fittings and other accessories.

4.5.1.42 - All necessary connecting Duct Work

for the different gases within the converter group,

including the required expansion joints, with the necessary lift limitations;

partly made of mild steel,
partly made of boiler plate,
partly made of heat resistant steel;

the ducts and expansion joints, coming into contact with hot SO₃-gases of more than 420 °C, will be spray-coated with aluminium after sandblasting where carbon steel is utilized only.

4.5.1.43 - Shut-off Plates

manually operated,

made of boiler plate or heat resistant steel.

4.5.1.44 - Butterfly Dampers

IND off butterfly dampers to be manually operated with sprocket wheel and chain, off butterfly damper to be pneumatically operated;

all made of boiler plate or heat resistant steel in welded construction.

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GER

4.5.1.45 - Gas-Gate Valves

IND bodies made of meehanite cast iron;

partly equipped with electric actuator, partly equipped with sprocket wheel and chain for manual operation.

4.5.1.46 - Analysis and Pressure Measuring Pipes

IND as well as the instrument pipes;

for the converter group,
including valves;

the pipes are made of stainless steel, as well as the ball valves and the condensate valves.

4.5.1.47 - Service Platforms and structural Steel Supports

IND within the converter sections,

for the converter and the ducts in different design,

including saddles, hangers and springs, as well as rollers.

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4.5.1.48 - All necessary Insulation Material

IND for thermal and acoustic insulation of equipment and duct work within the converter group;

Materials:

mineral wool blankets or blocks bound with chicken mesh of appropriate thickness;

for outside protection aluminium sheets have been included.

4.5.1.49 - Hoist

IND for serving a shut-off plate, manually operated.

4.5.1.50 - All necessary small Parts

IND such as nuts and bolts, gaskets, small steel parts, etc.;

required within the converter group.



Electrical Equipment and Turbo-Generator Plant 4.6

Turbo-Alternator-Set 4.6.1 IND

Rating

- live steam pressure : 40 bar
- live steam temperature : 350 °C
- operating voltage : 3.3 kV, 3-phase
- frequency : 50 Hz

Design

The turbo-alternator-set will consist of a condensation turbine with a generator and will be designed for island operation and for operation in parallel with the 6 kV network.

Technical Data

a) turbine - swallowing capacity: normal 16 000 kg/h max. 18 000 kg/h
- speed : 11 900 rpm
- extraction : 0...1 800 kg/h

at 5 bar

b) generator - output at 18 000 kg/h without extraction live steam of 40 bar 350 °C: 3 500 kW

- output at 18 000 kg/h with extraction 1 800 kg/h
power factor : 0.8
speed : 1 500 rpm
system : 3-phase, 50 Hz
construction : B3/D6
protection : IPR 44 - power factor - speed - system - construction - protection



Additional Data for Generator Control and Protection

a) Turbine-Operation

The turbine will be capable of operation both in parallel with the network or as an isolated generator feeding only the plant.

During parallel operation, the turbine control objective will be to maximise the use of available steam. Governor control action will therefore be to open the steam valve as far as possible without the high pressure steam line pressure falling below 40 bar. In this way maximum electrical power will be generated under any given combination of steam supply and plant operation conditions. It is important to note that during parallel operation the speed of the turbine-alternator-set is rigidly determined by the net frequency.

When operating as an isolated generator, governor action will be based solely on speed in order to ensure a proper 50 Hz supply to the electrical drives. Should there be inadequate steam available to the turbine, it will be necessary to disconnect some electrical load, before a speed drop of the turbine will occur.

If the operation of the alternator will be changed from parallel operation to isolated operation, the change over from pressure controlling to speed control will be done automatically.



b) Turbine-Protection

In the event any of the mechanical and/or electrical protection or the emergency push button are calling for a shut down, the quick shut-off valve or the alternator circuit breaker or both will be tripped automatically. If the quick shut-off valve is tripped only, the alternator circuit breaker will be tripped by the reverse power relay before the alternator will be feeded by the network. The required de-excitation will be done automatically. If for some reasons the turbine will be suddenly unloaded, the turbine speed will intercepted before a dangerous overspeed can occur, which would effect a trip of the quick shut-off valve.

c) Alternator-Operation

When connected in parallel with the network, the alternator will be unable to exercise any significant control over the 3.3 kV voltage thus the automatic voltage regulator (A.V.R.) will be controlled on the basis of the power factor of the alternator.

Should the net supply be lost, the A.V.R. will assume normal voltage control fully automatically. This changeover is effected by the turbine generator control equipment.



d) Alternator-Protection

The following protections and/or protection relays will be provided:

- overcurrent time relay
- differential relay
- reverse power relay
- stator earth fault relay
- high voltage relay
- winding overtemperature temperature transducers embedded in the stator will protect against winding overtemperature
- bearing overtemperature this transducer will guard against bearing failure
- overvoltage subject to the advice of the net regulating on 50 Hz dynamic overvoltage relay will be installed.

Fault conditions in the electrical circuit of the alternator will be detected by a high impendance, unbiased differential relay and earth fault protection.

The C.T.'s for this protection will be located at the (external) star point of the alternator winding and on the 3.3 kV bus side of the alternator circuit breaker;

- undervoltage- underfrequency relay
- A.V.R. relay
- underfrequency relay
- unbalanced-load protection
- overfrequency relay.



e) Busbar and H.V. Circuits-Operation

During normal operation the alternator circuit breaker will be closed giving parallel operation with the network supply. In the event of a serious disturbance in the network, the 3.5 MW turbine alternator set will either speed up or slow down and possible run at reduced voltage; the exact situation depending on the nature and location of the disturbance. Since the nature of the disturbance will be unknown at the control room, mains failure can only be inferred by frequency deviations. It is therefore proposed to supply two relays to detect both high and low frequency. In the event of either relay operation the circuit breaker will be tripped, locked out and the turbine alternator revert to independent running.

It is understood, that the network is subject to earth faults. To prevent these faults unduly affecting the operation of the turbine alternator, the circuit breaker will be fitted with directional overcurrent and earth fault protection so that should the alternator feed a fault in the network, the circuit breaker will trip and lock-out.

To facilitate synchronisation of the turbine alternator to the network supply an half-automatic synchronizer will be supplied.

This design renders to bring the turbine up to speed by hand and if the frequency and the phases are synchron to the network, the alternator circuit breaker will be closed automatically. This operation prevents unnecessary stresses of mechanical and electrical equipment.

For synchronising a synchronoscope dual-voltmeters and dual-frequencymeters will be provided.

Whilst facilities will be provided adjacent to the turbine to run it up to speed, we believe that the paralleling operation should only be carried out in a quiet room to avoid as many causes of operator distraction possible.



f) Plant Metering

We will supply MW, MVar and kWh metering on the bus couples and turbine alternator circuit breakers. The turbine alternator circuit breaker will also carry power factor, current, voltage and frequency metering.

g) Surge Protection

We have made provision for station class surge divertors with blow-out valves in view of lighting activities and the fact, that the alternator is directly connected to the 6 kV-system.

Scope of Supply

- turbine with alternator;
- auxiliary- and main exciter (brushless);
- main condenser; auxiliary condenser;
- vacuum pumps;
- oil pumps;
- control panel for instruments, push buttons, signalling lamps, etc.;
- switch board for contactors, auxiliary relays, fuses etc., for auxiliaries and controls.



4.6.2 Electrical Equipment for Pyrit Storage and Handling, Roasting Plant, Gas Cleaning Plant, Sulphuric Acid Plant

rianc

IND

DESIGN DATA

High voltage : 3.3 kV, 50 cps

Low voltage : 415 V, 50 cps

Control voltage : 220 V, 50 cps

Signal voltage : 24 V, D.C.

Standards : DIN, IEC.

High Voltage Switchgear Plant

Rating:

Operating voltage : 3.3 kV, 50 cps

Breaking capacity : 350 MVA

Control voltage : 220 V, D.C.

Design

Sheet metal-clad type (IP 21), with partions between the cells, single busbar system, single-row layout of the switch cell, switchgear truck with motoroperated circuit breaker, switching cycle counter, front door of the switchgear truck with installed control instruments, emergency off momentary contact switch for circuit breaker, earth isolator, indoor installation;

signalling display built in switch-cells for fault signalization as well as for overcurrent, overtemperature, Buchholz etc.



Outfittings

- 1 incoming feeder panel;
 circuit breaker, 3 current and 3 voltage trans formers, 1 voltmeter, voltmeter switch, wattmeter,
 frequency meter, earth leakage relay, protective
 and auxiliary equipment;
- 4 outgoing feeder panels for high-voltage motors; circuit breaker, current and voltage transformer, 1 ammeter, wattmeter, hourmeter, thermal overload relays in 3 phases, protective and auxiliary equipment;
- 2 outgoing feeder panels for transformer, 630 A,
 3 kV;
 circuit breaker, current transformer, protective
 auxiliary equipment;
- 1 measuring panel;
- 1 turbo-alternator feeding panel, circuit breaker, 3 current transformers, overload and short circuit protection with time lag, Wmeter, kWh meter, ammeter, protective and aux. equipment.

Transformers for the low Tension Power Switchboard

Rating : 1 250 kVA

Voltage : 3.3 / 0.415 kV

Impedance voltage : $u_{k} = 6 %$

three-phase oil-cooled transformer for indoor installation, off-circuit ratio adjuster ± 10 %, neutral brought out, tank cover with thermometer well, tank with oil drain device, cable terminal, expansion tank with liquid-level indicator, transformer with lifting eye, normal coat of paint, thermal switch for alarm and tripping, Buchholz relay for alarm and tripping.



Scope of Supply

2 transformers.

Batteries and Charges for DC-Control Voltage and Emergency Supply

Rating : 415 V, 50 Hz

Input voltage : 220 V.

Design

For the tripping supply of the 3.3 kV circuit breakers, consumers with charger for continuous charging are designed.

Outfitting

The batteries will be lead acid type. The charger unit includes the transformer, rectifier, control devices etc.

Scope of Supply

- 1 battery with ca. 100 cells for 220 V,
- 2 battery chargers:

input voltage : 415 V, 50 Hz
output voltage controlled;

1 DC-voltage switch gear.



4 High-Voltage Motors

Voltage

:

3.3 kV, 50 cps

Enclosure

totally enclosed,

IP 54

(T.E.F.C.)

Type

squirrel cage

motor,

fan-cooled;

suited for direct on-line starting.

Design

The motors will be a 3-phase squirrel cage induction machine for $6.0~\rm kV$, $50~\rm cycles$, and suitable for direct on-line starting.

The enclosure of the motors will be of a totally enclosed fan-cooled type; insulating class "F", temperature rise in accordance with class "B" will be provided.

Scope of Supply

- 2 high-tension motors, 200 kW,
- 1 high-tension motor, 250 kW,
- 1 high-tension motor, 1000 kW.



Low-Voltage Switch Gear

Rating

- operating voltage : 415 V, 3-pbhase

50 Hz

- bus bars system : single bus bar

- control voltage : 220 V, 50 Hz

Design

Generally, the switch gear will consist of two main parts:

a) power section built as MCC with withdrawable units

b) control section with fixed mounted equipment.

The switchgear will be a metal-enclosed type for in-door installation and completely wired.

Protection:

TP 40

The power section will be equipped with:

- 2 incoming feeders
- 1 bus bar coupler
- transformers for control voltage for all contactors, relays, etc. with sufficient capacity
- 3 pol. bus bars and PEN
- feeders
 for motors and/or consumers
 as required.

The control section will comprise all required auxiliary relays for motor controls and/or interlockings. The auxiliary relays will be fixed mounted.



Technical Data

The incoming feeder will be equipped with:

- 1 only 3-pol. hand-operated breaker,
 with over-load and over-current protection,
- 3 ammeters,
- 1 only voltmeter with selector switch,
- 1 only kWh-meter,
- current transformers, as required,
- miniature circuit breakers for control and measuring devices, as required.

The feeders for motors and/or consumers will be equipped with:

- 1 only 3-pol. load-break isolating switch
 and HRC-fuses,
- 1 only 3-pol. main contactor,
- 1 only 3-pol. thermal over-load protestion relay,
- 1 only 1-pole miniature circuit breaker
 for control voltage,
- current transformer, as required.

As mentioned before, the control section will comprise all required auxiliary relays, time relays, etc.

The motors will be controlled locally only or at the instrument control panel in the control room. Motors that are controlled from this panel can be controlled locally too. For that purpose, a delocking switch with start- and stop-button will be installed near the motor. To prevent accidents, motors which are provided with remote control can only be started after a start-up warning has been given. The button for this warning will be installed at the instrument and control panel and the required control system in the control section.



Scope of Supply

1 only low tension switch board,

consisting of power and control section, as described above for roasting gas cleaning and $\rm H_2SO_4$ plant.

1 only low tension switch board consisting of power and control section as des-cribed above per pyrite ore preparation plant.

Low-Voltage Motors

Voltage : 415 V, 50 cps

Enclosure : totally enclosed, IP 54

(T.E.F.C.)

Type : squirrel cage motor,

fan cooled;

suited for direct on-line starting.

Scope of Supply

number of consumers according to consumer list.

Local push Button Stations

The motors can be locally operated through startstop push buttons located inside enclosed box next to each motor.

For motors over 7.5 kW, an ammeter is incorporated in this box.

For interlocking drives, operation of sequences possible from instrument control panel; an interlocking switch is also provided in the local push button station.



Signalisation

Motor and process alarms, number as required, to be mounted in a separate cubicle, withdrawable relay-type design, output voltage 24 V D.C., the signalling lamps and momentary contact push buttons for lamp control and fault signal acknowledgement will be built into the control panel.

Operating voltage

24 V DC

Layout of the signalling plant according to the following diagram:

| | operating state | signal lamp | horn |
|-------------------|--------------------|-------------------|------|
| Motor | | | |
| signal | off | off | off |
| | on | steady light | off |
| | cut off | off | off |
| | failure | rapid flashing | on |
| | acknowledge | slow flashing | off |
| Process signal | no fault | off | off |
| | fault | rapiā flashing | on |
| | acknowledge | slow flashing | off |
| | fault cleared | off | off |

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Lighting Plant, Socket Devices

The lighting distributon will be included in a separate cubicle of the low-tension switchboard.

Fluorescent fixtures and HQL-lamps will be used for lighting.

Lighting will be provided with low-voltage tubular lamps.

The following light intensities will be used:

30-60 Lux - in the plant, on the walkways, stairs, access ways, motors, valves etc.

350 Lux - in the instrument control panel room,

300 Lux - in the switchgear plant room.

Two 220 V socket outlets each are provided in the instrument control panel and in the low tension switching plant room.

415 V socket outlets are arranged in the plant, so that a cable of 30 m length will reach every point of the plant.

Emergency lighters will be provided by means of incandescent lamp 25 W, situated next to emergency way-outs, important stair cases, control rooms and switch gear.

Cables

For power supply, control and lighting PVC insulated, PVC sheathed, cables with copper conductors will be used. The smallest cross section is 2.5 mm² for motors and socket outlets and 1.5 mm² for control cables and lighting.

The maximum voltage drop is 4 % of motor rated current.

Provision has been made for the required cables between high-voltage switchgear plant, transformers and 6 kV-HT-motors, low-voltage switchgear plant, motors, lamps, socket outlets and local control devices.



Installation Material

For the above mentioned items and complete installation material, which is required for the erection of the plant, ready for operation, installation material has been provided such as ascending cable route with fixtures and supports, cable racks, rack brackets, sectional irons, clamps, clips, screwed connections, protecting tubes etc.

Earthing System

The earthing system will be executed with galvanized strip steel 30 \times 3.5 mm.

The scope of supply comprises all materials including fastening material required for earthing of containers and of the low-tension switchgear plant.

Connection of the earthing system to the connecting points above ground in required number.

Earthing rods and their electrical interconnection.



4.7 Measuring and Control Instruments

4.7.1 Roasting Plant

IND

Concentrate Bins Level Alarm

consisting of:

8 paddle type level switches

Temperature Measurement Roaster, Waste Heat Boiler and Gas Ducts

consisting of:

- 24 double thermocouples NiCr-Ni with stop and counter flange
 - 2 measuring point selector switches for 24 measuring points
 - 2 electric indicators
 - 2 electric 12-colour dot recorders
 - 2 cold junction boxes for 24 thermocouples NiCr-Ni.

Local Cooling Water Flow

consisting of:

1 flow meter (rotameter)



Temperature Monitoring System Roasting Air Blower Motors Windings

consisting of:

- 12 resistance thermometers
 (incl. in mech. supply)
- 2 electr. indicators each for 6 points
- 2 signal units with 2 limit contacts
- 2 selector units
- 2 R/I converters

Local Level Measurement Fuel Oil Tank

consisting of:

2 float type level indicators
 (incl. in mech. supply)

Roasting Air Pressure

consisting of:

- 2 shut-off valves
- 2 electric pressure transmitters
- 2 electric two-line recorders
 (second line roasting air flow)
- 2 protection boxes for transm.
- 2 power supply units for transmitters.



Roasting Air Flow

consisting of:

- 2 orifice plates
- 4 shut-off valves
- 2 3-valve manifolds
- 2 electric differential pressure transmitters
 (recorded with roasting air pressure)
- 2 power supply units for transmitters
 with square-root extraction.

Pressure Measurement Roaster Outlet

consisting of:

- 2 shut-off valves
- 2 electric pressure transmitters
- 2 electric indicators
- 2 air purge units with diff. pressure controller
- 2 protection boxes for transmitter
- 2 power supply units for transmitters
- 2 air press. red. station.

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Waste Heat Foiler and Cyclone Outlet Pressure

consisting of:

- 4 shut-off valves
- 4 electric pressure transmitters
- 2 electric indicators
- 4 air purge units with diff. pressure controllers
- 4 protection boxes for transmitters
- 4 power supply units for transmitters
- 4 air press. red. station

Remote Control Roaster Air Damper and Inlet Vane

consisting of:

- 4 push buttons "more-0-less"
- 4 electric position indicators
- 4 supply units for position transmitter
- 4 dampers with electric actuator and position
 transmitter
 (incl. in mech. supply)

Remote Control Discharge Conveyor

consisting of:

- 4 electric speed indicators
- 4 electric speed transmitters
- 4 push-buttons "more-0-less"
- 4 control drives with tacho-generator
 (incl. in mech. supply)



Secondary Air Flow

consisting of:

- 2 orifice plates with armoured edges
- 4 shut-off valves
- 2 3-valve manifold
- 2 differential pressure indicator
- 2 protection box

Miscell. Local Temperature Measurements, Cooling Air

consisting of:

2 bimetallic thermometers with protection tubes.

Local Pressure Measurement, Cooling Air

consisting of:

- 1 capsule-type pressure gauge
- 1 shut-off valve

Pressure Measurement Electric Precipitator Outlet

- 2 shut-off valves
- 2 electr. pressure transmitters
- 2 electr. 1-line recorders
- 2 power supply units for transmitters
- 2 protection boxes for transmitters



Remote Control of Butterfly Dampers

consisting of:

- 3 push buttons "more-0-less"
- 3 electric position indicators
- 3 power supply units for position transmitters
- 3 butterfly valves with electr. actuators and with electr. position transmitters (incl. in mech. supply)

Miscell. Local Temperature Measurements

consisting of:

12 bimetallic thermometers with protection tubes

Local Pressure Measurement, Cooling Water

consisting of:

- 2 shut-off valves
- 2 bourdon type pressure gauges

Time Control of Raco-Cylinder for Shutter

consisting of:

- 4 time relays
- 2 hand/auto. switches
- 2 open/closed switches
- 1 motor control cubicle with its auxiliaries
 (incl. in the electr. scope of supply)
- 2 Raco-cylinders with electr. actuator
 (incl. in mech. supply)

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Current Measurement of Roasting Air Blower Motors

consisting of:

- 2 on/off switches
- 2 ammeters
- 2 I/I-converters
 (incl. in the electr. scope of supply)

Current and Voltage Measurement of Precipitators

- 8 on/off switches
- 4 ammeters
- 4 voltmeters
- 4 U/I converters
- 4 I/I converters

Flow Measurement Pyrite Feed to Roasters

- 1 idler weigher
- 1 control cubicle for local installation
 with flow indicator, counter, weighing bridge and
 band speed meter
 (incl. in mech. supply)
- 1 electr. 1-line recorder
- 1 electr. integrator with counter



Oxygen Gas Analysis Outlet of Electrostatic-Precipitators

consisting of:

- 2 gas sampling devices with filter
- 2 gas flowmeters with needle valve
- 2 paramagnetic gas analyzers with power supply unit
- 2 analysis cabinets made out of polyester, glass fibre reinforced, completely mounted, wired and hosed with auxiliaries, ready for connection, for local installation
- 1 electric 2-line recorder

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4.7.2 Waste Heat Boiler

IND

Temperature Control Superheated Steam

consisting of:

- 2 double thermocouples NiCr-Ni with protecting well, weld-in type
- 2 U/I-converters
- 2 electrical PI-controllers
- 2 el./pn. positioners
- 2 electric two-line recorders
 (second-line steam flow)
- 2 3-way mixing slide valves with pneum. actuator (incl. in mech. supply)
- 2 supply pressure regulator stations

Steam Drum Pressure

- 2 shut-off valves
- 2 electric pressure transmitters
- 2 electric indicators
- 2 protection boxes for transmitters
- 2 syphon tubes

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Steam Pressure Control

consisting of:

- 2 shut-off valves
- 2 electric pressure transmitters
- 2 electric single-line recorders
- 2 protection boxes for transmitters
- 2 syphon tubes
- 2 electric controllers
- 2 el./pn. positioners
- 2 control valves with pneum. actuators
- 2 supply pressure regulator stations

Local Pressure indication Steam Drum and Steam Line

consisting of:

- 5 Bourdon type pressure gauges
- 5 syphon tubes
- 5 shut-off valves

Local Pressure Indication Feed Water and Circulating Pumps

- 12 Bourdon type pressure gauges
- 12 shut-off valves



Local Pressure Indication Deaerator

consisting of:

- 1 Bourdon type pressure gauges
- 1 syphon tubes
- 1 shut-off valves

Local Temperature Indication Water and Steam Lines, Feed Water

consisting of:

11 bimetallic thermometers with protection tube

Pressure Control Steam Reducing-Stations

consisting of:

2 direct-acting electro-hydraulic pressure
 controller

Pressure Control Deaerator and Turbo Set

consisting of:

2 direct-acting pressure controller

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Circulating Water Flow

consisting of:

- 4 orifice plates
- 8 shut-off valves
- 4 3-valve manifolds
- 4 electric differential pressure transmitters
- 4 electric indicators with limit contacts
- 2 electr. double-line recorders
- 4 protection boxes for transmitters
- 4 power supply units for transmitters with square-root extraction

pH-Measurement in Condenser Line

- 1 flow chamber for pH
- 1 set of measuring and reference electrodes
- 1 pH-amplifier
- 1 electr. indicator with limit contacts
- 1 electr. single-line recorder

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Flow Control Feed Water

consisting of:

- 2 orifice plates
- 4 shut-off valves
- 2 3-valve manifolds
- 2 electric differential pressure transmitters
- 2 electric PI-controllers (cascade controller)
- 2 electric 2-line recorders
 (second line level steam drum)
- 2 protection boxes for transmitters
- 2 power supply units for transmitters
 with square-root extraction

Steam Flow

- 2 annular chamber type standard orifice plates
- 4 balancing vessels
- 4 shut-off valves
- 2 5-valve manifolds
- 2 electric differential pressure transmitters
 (recorded with temperature superheated steam)
- 2 protection boxes for transmitters
- 2 power supply units for transmitters
 with square-root extraction



Level Control Steam Drum

consisting of:

- 2 balancing devices with condensate vessel
- 4 shut-off valves
- 2 3-valve manifolds
- 2 electric differential pressure transmitters (recorded with feed water flow)
- 2 electric PI-controllers (master controller)
- 2 computing relays (adder-substractor)
- 2 feedwater control valves with pneum. actuator and el./pn. positioner
- 2 supply pressure regulator stations
- 2 protection boxes for transmitters
- 2 power supply units for transmitters

Local Level Indication Steam Drum

consisting of:

4 level gauges

Local Level Alarm Steam Drum

consisting of:

2 float type alarm unit with minimum and maximum contact

Local Level Indication Feed Water Tank

consisting of:

1 level gauge

Local Level Control Feed Water Tank

consisting of:

1 direct acting level controller

Local Level Control Condensers

consisting of:

2 direct acting level controllers

Remote Control Start-Up Steam Valve

consisting of:

- 2 push buttons "less-0-more"
- 2 electric indicators for position indication
- 2 electric actuators with position transmitters
- 2 power unit for position transmitters

Local Level Alarm Feed Water Tank

consisting of:

1 float type alarm unit with min. and max. contact



Local Temperature Control Feed Water to Reducing Station

consisting of:

- 1 hydrolic temperature controller
- 1 control valve with pneum. actuator

Temperature Measurement Condenser Lines

- 2 resistance thermometers with protection tube
- 2 R/I converters
- 2 electr. indicators

4.7.3 Gas Cleaning Plant

IND

Gas Cleaning Section Inlet and Outlet Temperature

consisting of:

- 2 single resistance thermometers Pt 100
- 2 electric indicators
- 2 R/I converters

Temperature Measurement and Alarm Outlet Washing Tower

consisting of:

- 1 double-type resistance thermometer Pt 100
- 1 single-!ine recorder (electric)
- 1 electric indicator with limit contacts
- 1 auxiliary relay
- 1 solenoid valve
- 1 pneum. on-off valve
- 1 supply press. red. station
- 1 R/I converter

Local Temperature Measurement Gas-, Weak Acid- and Water Lines

consisting of:

6 bimetallic thermometers with protection tube

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Local Pressure Measurement Gas Lines

consisting of:

5 U-tube pressure yauges, mounted on beechwood boards, with shut-off valves

Local Pressure Measurement Acid and Water Lines

consisting of:

4 diaphragm pressure gauges with open flange

Pressure Measurement Inlet and Outlet Gas Cleaning Section

consisting of:

- 2 shut-off valves
- 2 electric pressure transmitters
- 2 protection boxes
- 2 electr. indicators
- 2 power supply units for transmitters

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4.7.4 Drying and Absorption Plant

IND

Local Differential Pressure Measurement Filters at Drying Tower, Intermediate and Final Absorbers

consisting of:

- 3 U-tube differential pressure gauges
- 6 shut-off valves

Local Temperature Measurement Cooling Water

consisting of:

5 bimetallic thermometers with protection tubes

Local Temperature Measurement Acid Lines

bimetallic thermometer with protection tube

Local Flow Measurements Dilution Water

consisting of:

- 2 flowmeters (rotameters)
- 6 shut-off valves

Local Level Control Process Water Tank

consisting of:

float type level controller with valve

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Local Level Measurement Acid Pump Tanks

consisting of:

3 Local floats type-level-indicators

Local Temperature Measurement Gas Ducts

consisting of:

4 bimetallic thermometers with protection tubes

Acid Line Temperatures

consisting of:

- 6 resistance thermometers Pt 100
- 1 measuring point selector switch for 12 measuring points
- 1 electric indicator
- 1 power supply unit

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Level Control and Alarm Acid Pump Tanks

consisting of:

- bubbling tubes
 (incl. in mech. equipment)
- 3 air purge units with differential pressure controller
- 3 electr. diff. pressure transmitters
- 3 electr. indicators with limit contacts
- 3 electr. PI-controllers
- 3 el./pn. positioners
- 3 supply pressure regulator stations
- 3 protection boxes for transmitters
- 3 control valves with pneum, actuators
- 3 power supply units for transmitters

${\tt pH-Measurement\ and\ Supervision\ Ccoling\ Water}$

- 1 flow chamber
- 1 reference electrode
- 1 measuring electrode
- 1 resistance thermometer
- 1 electr. pH-transmitter
- 1 electr. indicator with limit contacts
- 1 protection box for transmitter



Acid Concentration Measurement and Control

consisting of:

- 3 acid coolers
- 3 flow chambers
- 3 conductivity electrodes
- 3 measuring transducers with electric indicators for local installation
- 3 electric PI-controllers
- 3 el./pn. positioners
- 3 control valves with pneum. actuator
- 3 electric one-line recorders
- 3 supply pressure regulation stations
- 3 protection boxes for transmitter

Remote Adjustment Air Damper

- push-button "less-0-more"
- 1 electric indicator for position indication
- electric actuator with position transmitter
 (incl. in mech. equipment)
- 1 power unit for position transmitter

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4.7.5 Converter Plant

IND

Temperature Measurement Converter and Gas Line

consisting of:

- 8 single thermocouples NiCr-Ni (type K)
- 6 double thermocouples NiCr-Ni (type K)
- 1 measuring point selector switch for 24 measuring points
- l electric indicator
- 1 electric 6-point dot recorder
- 1 cold junction box for 24 thermocouples (NiCr-Ni)

Pressure Measurement SO₂ Blower Outlet

- 1 shut-off valve
- 1 electr. pressure transmitter
- protection box for transmitter
- 1 electr. indicator
- 1 power supply unit for transmitter



SO₂-Gas Flow

consisting of:

- 1 orifice plate with armoured edge
- 2 shut-off valves
- 1 3-valve manifold
- 1 electric differential pressure transmitter
- 1 electric single-line recorder
- 1 protection box for transmitter
- power supply unit for transmitter
 with square-root extraction

SO₂-Gas Analysis

- 1 gas sampling device with filter
- 1 washing and drying bottle
- 1 gas filter with filling
- 1 gas flowmeter with needle valve
- thermal conductivity gas analyser with power supply unit
- analyses cabinet made of polyester, glass fibre reinforced, completely mounted and wired/hosed ready for connection, for local installation
- 1 electric single-line recor



Remote Adjustment Vane Control SO₂-Blower and Cold Gas Valves

consisting of:

- 3 push-buttons "less-0-more"
- 3 electric indicators for position indication
- 3 electric actuators with position transmitters
 (incl. in mech. supply)
- 3 power units for position transmitters

Temperature Monitoring System SO_2 -Blower Motor Windings and Blower Bearings

consisting of:

- 12 resistance thermometers
 (incl. in mech. supply)
- 2 electric indicators each for 6 points
- 2 signal units with 2 limit contacts
- 2 selector units
- 2 R/I converters

Preheater Temperature Measurement (cold gas inlet and outlet)

- 2 resistance thermometers Pt 100
- 2 electric indicators with limit contacts
- 1 protection box above
- 1 power supply unit

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Local Differential Pressure Measurement Preheater

consisting of:

- 1 capsule-type manometer with limit contacts
- 2 shut-off valves

Local Temperature Measurement Outlet Heat Exchanger III

consisting of:

bimetallic thermometer with protection tube



4.7.6 1 Instrument Panel

IND

for accommodation of the measuring, recording and control instruments, completely mounted and fitted with wired and tubes ready for connection up to the terminal strips, with synoptic diagram including signalling lamps for process failures. It further included signal lamps for the motor drives as well as the required momentary-contact switches to start the motors or motor groups, which are installed in the plant.

The alarm system is included in the scope of the electric power distribution.

The instrument panel is:

open on the top and on the rear, closed on the sides;

length: approx. 8 000 mm
height: approx. 2 500 mm
depth: approx. 800 mm

4.7.7 Measuring Cables, Impulse Lines as well as Installation Material

IND

This item comprises all required cables, tubes, small parts and mounting materials for the above-mentioned measuring and control instruments.

Multi-core cables of the NYY type are mainly used; special cables will be used as far as required.

4.8 Civil Work, including Building and Structural Steel Work

IND

General

The cost estimate for the determination of the investment costs has been based on the relevant German Standards (DIN) and cost situation ruling in the F.R.G., 1985 June.

The quantity survey has been based on the following assumptions:

- the plant site has been suitably graded by others (rough grading);
- the solids as well as subsoil water do not include corrosive properties; subsoil water table can be expected to be below the founding level;
- electric power as well as water consumption for building purposes will be free of charge.



Work included:

The coat estimate includes:

The engineering services:

- the static and dynamic computations,
- the design and workshop detailing for steel structure,
- the civil arrangement drawings,
- reinforcing drawings,
- bending schedules and list of embedded items,
- the architectural details,
- the placing plans for cladding.

The execution of:

- excavation, backfilling, removal of surplus material, blinding, concrete, reinforcement, formwork, surface treatment, plastering, decorating, painting and coating; PVC-tiling as well as acid proof tilings and linings were required; steel structure for buildings including floor coverings, corrosion, protection (gid blasting and painting, 200 µm dry film thickness), corrugated galvanized metal sheeting with all necessary flashings, metal doors, illuminated ceilings in the control rooms, windows or translucent sheeting inside the battery limits.



Battery Limits:

Included in the estimate are the buildings and plant sections themselves.

Not included are any work, storm water and sewage drainage systems, earth work for cables and piping, effluent treatment plant.

The rough grading, soil investigation and subsequent investigation report as well as costs for building permits, insurances, taxes and duties shall be borne by others.

The following buildings and plant sections have been included in the estimate:

Ore Preparation Plant

plant structures, electrical substation, foundations for screens, crushers, conveyors, concrete pads for storage.

Roasting Plant

roofed pyrite storage,
pyrite unloading station,
conveyor bridge system to roasting building,
roasting building with cooling drum support,
hot gas cleaning section,
wet gas cleaning section,
sulphuric acid plant section,
SO2-blower building,
electrical substation (high tension switch room).



Effluent Treatment Unit for neutralizing the liquid effluents from the Plant

- Effluent treatment pit, capacity approx. 200 m³ with concrete walls and anti-acid lining of walls.
- 2. ime/or Soda bin
 capacity approx. 10 cu.m.
 made of steel
 with a totary valve (motorized) at the bottom,
 speed controlled, to adjust the feed rate of
 lime/or soda.
- 3. 1 circulating-cum-discharge pump, in acid-proof design, of suitable plastic material, capacity approx. 6 m³/hr. Pressure-head: 2 bars to circulate or discharge the pit liquid.
- 4. Liquid pipe-lines, made of plastic material, i.d.: 2 inches, will the required valves and fittings.
- 5. 2 pH meters to measure and monitor the pH in the effluents!
 One instrument with remote indication/alarm in the control panel.

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Chapter 5

Budget Estimates of Costs of Equipment

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| 5.1 | Budget Estimates of Cost in Plant | | |
|--------|--|---------------|------------------------|
| | | RS pl | us DM |
| 5.1.1 | Pyrite Ore Preparation Plant and Pyrite Handling : | 7 100 000 | |
| 5.1.2 | Reasting Line 1 incl. HGP : | 10 200 000 | - 3 670 000 . — |
| 5.1.3 | Roasting Line 2 incl. HGP : | 10 100 000 | 3 280 000 |
| 5.1.4 | Common BFW System for both Boilers : | 3 000 000 | - 340 000 |
| 5.1.5 | Wet Gas Cleaning Plant: | 12 500 000 | 2 430 000 |
| 5.1.6 | Sulphuric Acid Plant : | 22 700 000 | 1 480 000 |
| 5.1.7 | Electrical Equipment : | 12 100 000 | |
| 5.1.8 | Turbo-Alternativ Plant: | 14.200.000 | . - |
| 5.1.9 | Water Treatment Plant and Recooling Tower System : | 4 900 000 | · - |
| 5.1.10 | Measuring and Control Instruments : | 4 400 000 | |
| 5.1.11 | Steel support Structure (erected cost) : | 10 300 000 | · <u>-</u> |
| 5.1.12 | Civil Work incl. Concrete : | 3 300 000 | · - |
| 5.1.13 | Erection Cost of Plant Equipment : | 21 000 000 | · <u>-</u> |
| | Total Equipment and Plant Costs : | 135 800 000 | 11 200 000.— |
| | Total Weight of Equipment : | approx. 3 300 | t |
| | Total Weight of Steel Structure : | approx. 735 | t |



The above German prices are based on actual wage tarifs and material costs ruling ont June 1985. The foreign portion is for supply FOB North Sea Port, incl. packing as far as required.

The Indian costs are based on current conditions and for delivery free to site, including packing as far as necessary.

Taxes, custom duties, levies or any surcharges are not included in the above prices.

In case of a contract the services and supplies can be divided between Indian and Foreign, whereby Lurgi is in a position to offer the foreign portion, following an enquiry.

The estimates are as follows:-

Basic Engineering and Know-How Fee (Lurgi Technology) : DM 3 100 000.--

==============

Supply of Essential Parts, to be imported

: DM 8 100 000.--==============

Alı prices are purely indicative and not binding to anyone.

Delegation of Personnel for Supervisory Services

: DM 1 000 000.------- The tabulated equipment prices under 5.1 include the costs for -

- machinery
- vessels
- piping items, pipe supports and service platforms
- the external lagging
- the linings
- the painting
- the detail engineering and the basic engineering

Time Schedule

The completion time for the plant from zero date to commencement of production can be estimated to be approx. 30 months, when competent and experienced companies are engaged in the project execution.



Estimated Capital Investment for Roasting & Acid Plant Amjhore Capacity 320 tpd., 2 roaster Streams.

Exchange rate 1 DM = Rs 4.5

| | | (Figures | in Rs. | Lakhs) |
|---|---|----------|--------|---------|
| | | Indian | German | Total |
| l. Equipment + Materials | | 994.72 | 371.28 | 1366.0 |
| Freight, Insur. & Handling cif & free site (free flag | | 55.00 | 37.00 | 92.0 |
| 3. Sales Tax | | 39.80 | - | 39.80 |
| 4. Custom Duty | | | - | - |
| 5. Civil Works | | 33.00 | - | 33.00 |
| 6. Engineering & Procurement | | 79.20 | 146.48 | 225.68 |
| 7. Tax on Eng. fee | | 36.62 | - | 36.62 |
| 8. Erection, incl. Supervn. | : | 210.0 | 45.0 | 255.0 |
| 9. Tax on Supervn. | | : 29.25 | | 29.25 |
| 10. Sub-Total | : | 1477.59 | 599.76 | 2077.35 |
| 11. Contigency | : | 44.41 | 10.0 | 54,41 |
| 12. Erected Plant Cost | : | 1522.00 | 609.76 | |

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Chapter 6

Operating Cost Estimates

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6.1 Operating Cost Estimates

The costs are estimated at nominal load condition of the Plant.

Actually, similar plants elsewhere in the world give a working time or availability of over 95 %.

In the study considering more idle time due to familiarization of personnel with the plant operation and its maintenance in the initial stage an availability factor of only 90 % (330 days per annum) is assumed.

Plant operating Conditions:-

- 6.1.1 Working days per annum : 330 days
- 6.1.2 Daily acid production : 320 tpd

Annual acid production : 105 600 tpy

6.1.3 Pyrites consumption:

High grade Pyrites : 217 tpd = 71 610 tpy

Low grade Pyrites : 240 tpd = 79 200 tpy

6.1.4 Electrical power consumption
Total consumption for plant
and off-sites assumed at 2400 kW

(180 kW/t Acid) = 19 000 MWh/year

- 6.1.5 Internal power generation = 23 250 MWh/year
- 6.1.6 Estimated surplus power for

 rt from plant = 4 250 MWh/year

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6.1.7 Steam generation

Stream no. 1 : 95 040 t/a

Stream no. 2 : 31 680 t/a

Total 126 720 t/a

All steam is utilized in the T/G-set for power generation.

6.1.8 Fresh water consumption = $70 \text{ m}^3/\text{h}$

Fresh water supply yearly = $554 400 \text{ m}^3/\text{a}$

6.1.9 Chemicals consumptions:

Chemicals will be required as consumables for the demineralisation of boiler feed water. However the consumption will depend on raw water quality, but the costs involved are considered as insignificant on cost of production. The boiler feed water can be value added to cover these costs.

Boiler feed water requirement : 3 168 t/a (approx. 2.5 % of circulated water)

6.1.10 The wash acid bleed can be utilized for the reaction in the SSP plant, provided toxic substances do not abound in the pyrites, such as Mercury, Arsenic, etc.

Since this is not the case the wash acid can be added in clear condition to the production acid.

Wash acid generation (assumed) = 4.8 tpd as MH

= 1 584 tpy as MH

6.1.11 Total Acid Production:

107 184 tpy as MH

======

6.1.12 Cinder Production:

Cinder of HGP:

6.8 t/h = 53 856 t/a

Cinder of LGP:

9.0 t/h = 71 280 t/a

Cinder from HGP can be partly added to cement during klinkering to adjust the iron module. Total use will depend on cement plants capacity to absorb the material and also the type of raw material used there.

The cinder from stream no. 2 has been found to have binding properties and can be used as a binder after proper conditioning. This can add to the revenue of the plant.

6.1.13 Plant manning:

For employing 80 persons at an average cost of Rs 1900/-month

annual expenditure will be: Rs 1 824 000.--

6.1.14 Repair and Maintenance

It is assumed that for repair and maintenance of the Plant approx. 3 % of equipment investment will do, though in the initial years the intensity of these costs can be considered less.

6.1.15 Cost of Pyrites:

The HGP has according to PPCL a cost of Rs 876.-- per tonne (PPCL telex of 10.10.85). It is assumed that the LGP being a waste by-product has nill-value.

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6.1.16 Table of Approx. Operating Costs:

All costs in Indian Rupees

| | | | Unit cost | yearl consu | - | on_ | | yea | arly | cost |
|-----|---------------------------|-----|-------------|----------------|-----|------|--------|-----|------|-------|
| 1. | H.G. Pyrites | : | 876/te | 72 | 000 | te | | 63 | 072 | 000 |
| 2. | L.G. Pyrites | : | nil | 79 | 200 | te | | | | |
| 3. | Cooling water | : | $2/m^3$ | 555 | 000 | m³ | | 1 | 110 | 060 |
| 4. | Boiler Feed water | : | 5.—/m³ | 3 | 168 | m³ | | | 15 | 840 |
| 5. | Chemicals & Lubricants | : | - | Lump | sum | | | | 50 | 000.— |
| 6. | Repair & Maintenance | : | 3% of equi | p. cos | t | | | 4 | 100 | 000.— |
| 7. | Personnel | : | 1900/:nonth | | 80 | | | 1 | 824 | 000 |
| 8. | Compressed air | : | $0.1/m^{3}$ | 3 200 | 000 | m³ | | | 320 | 000.— |
| 9. | Start-up oil | : | 4/kg | | 250 | te | | 1 | 000 | 000 |
| 10. | Cinder disposal | : | 10/te | 125 | 136 | te | | 1 | 251 | 360.— |
| | Total operating | goo | osts : | | | | Rs | 72 | 743 | 200 |
| | Specific operat | | g cost : | | F | ≀s ƙ | 78.67/ | 'te | Acid | (MH) |

6.1.17 Revenue from Production

All figures in Rupees

| | Unit cost | yearly production | revenue | |
|-------------------|------------------|----------------------|---------|-------|
| 1. Sulphuric Acic | : 1 350/t | 107 184 te | 144 698 | 400 |
| 2. Electric power | : 0.75/kWh | 4 250 000 kWh | 3 187 | 500.— |
| Total revenue | | Rs | 147 885 | 900 |
| Income per ton o | f produced acid: | Rs | 1 | 380 |

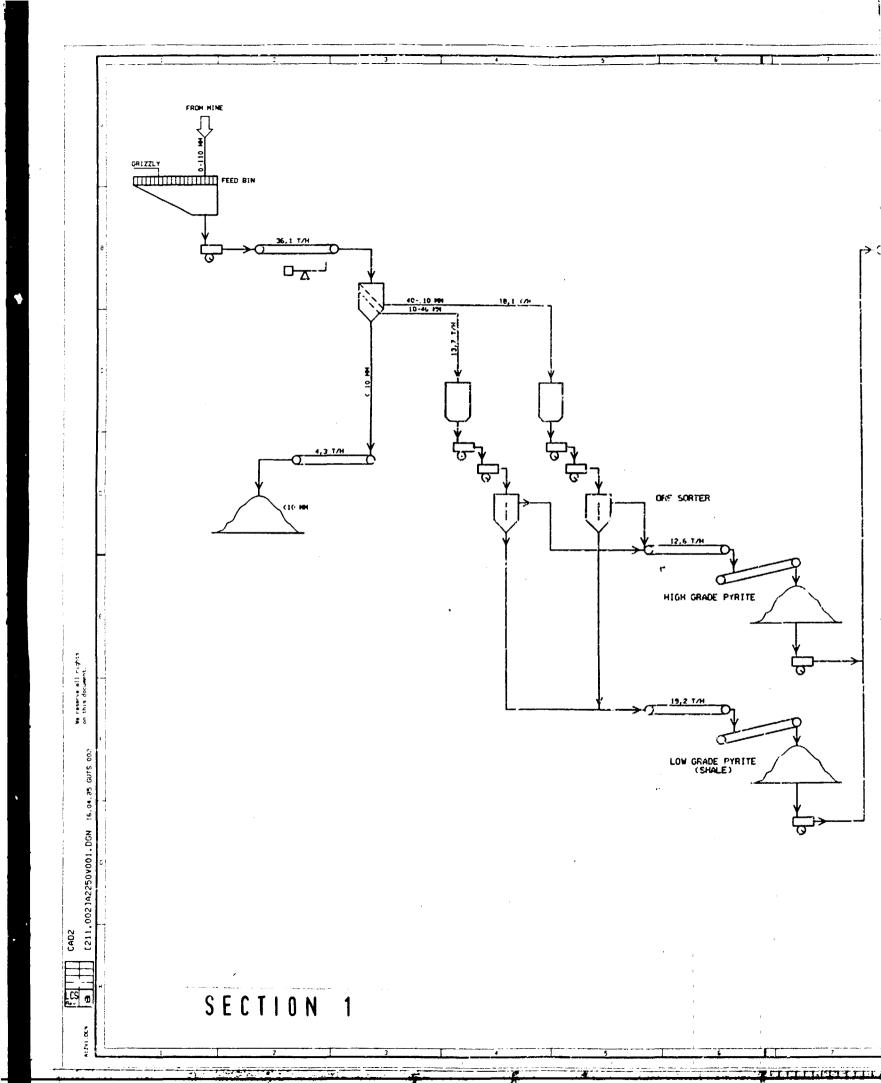
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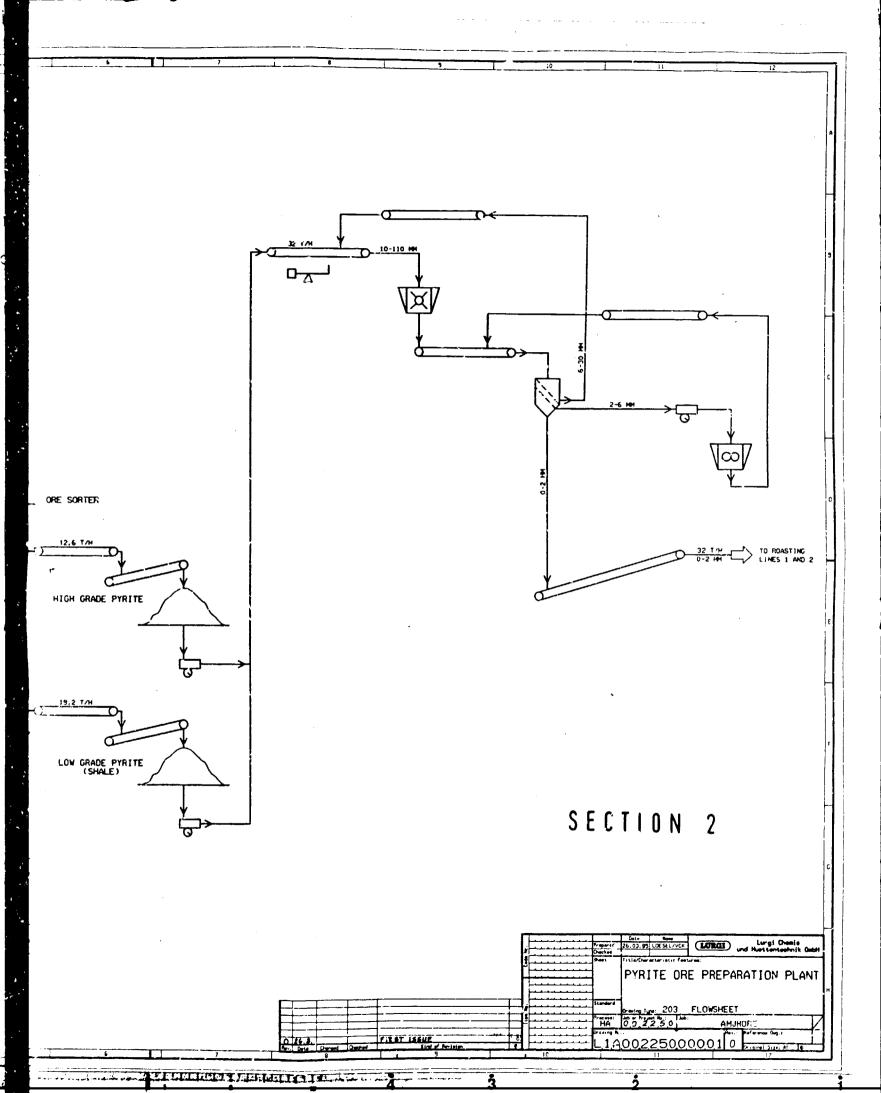
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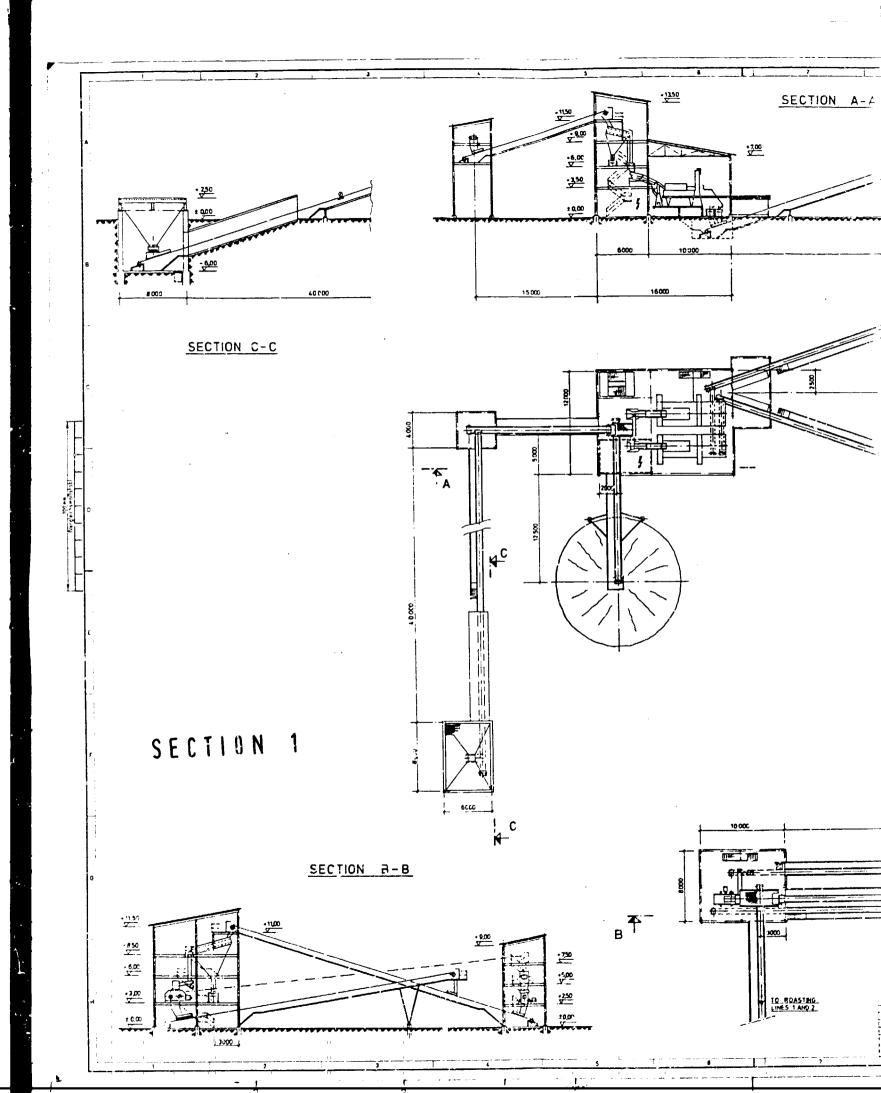
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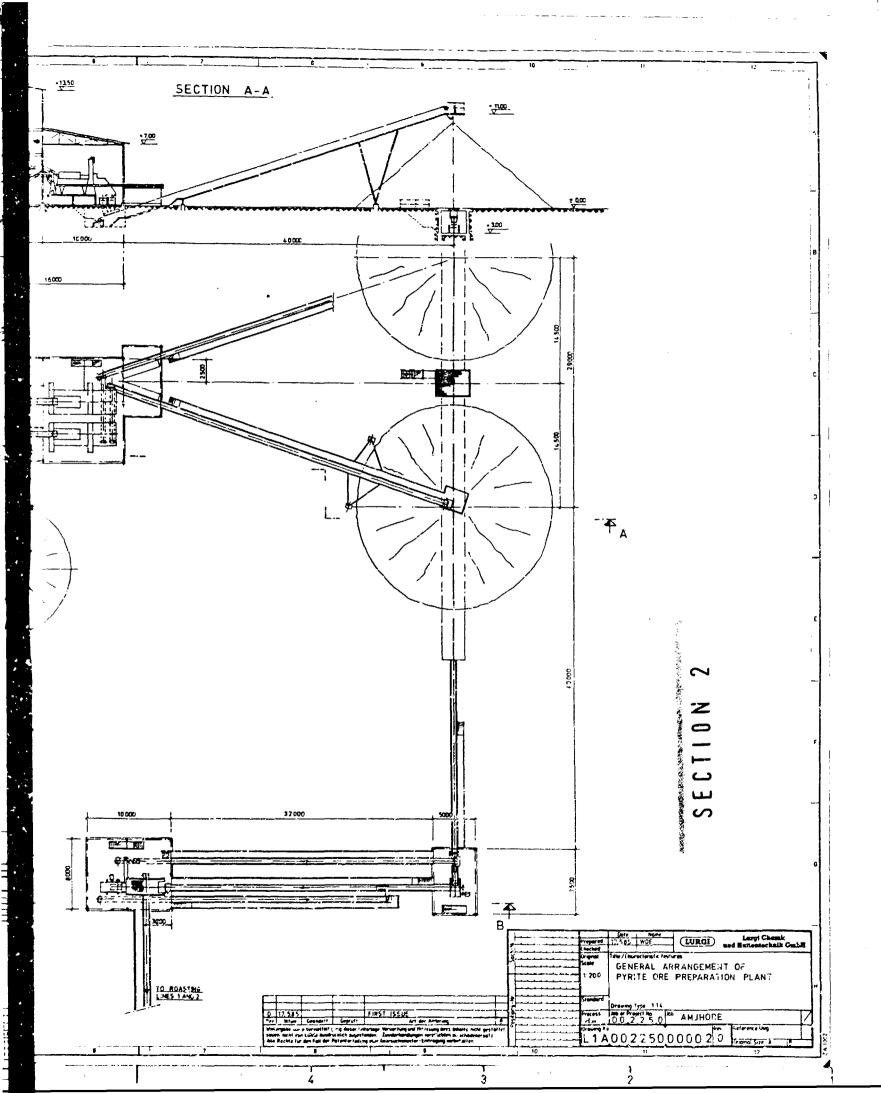
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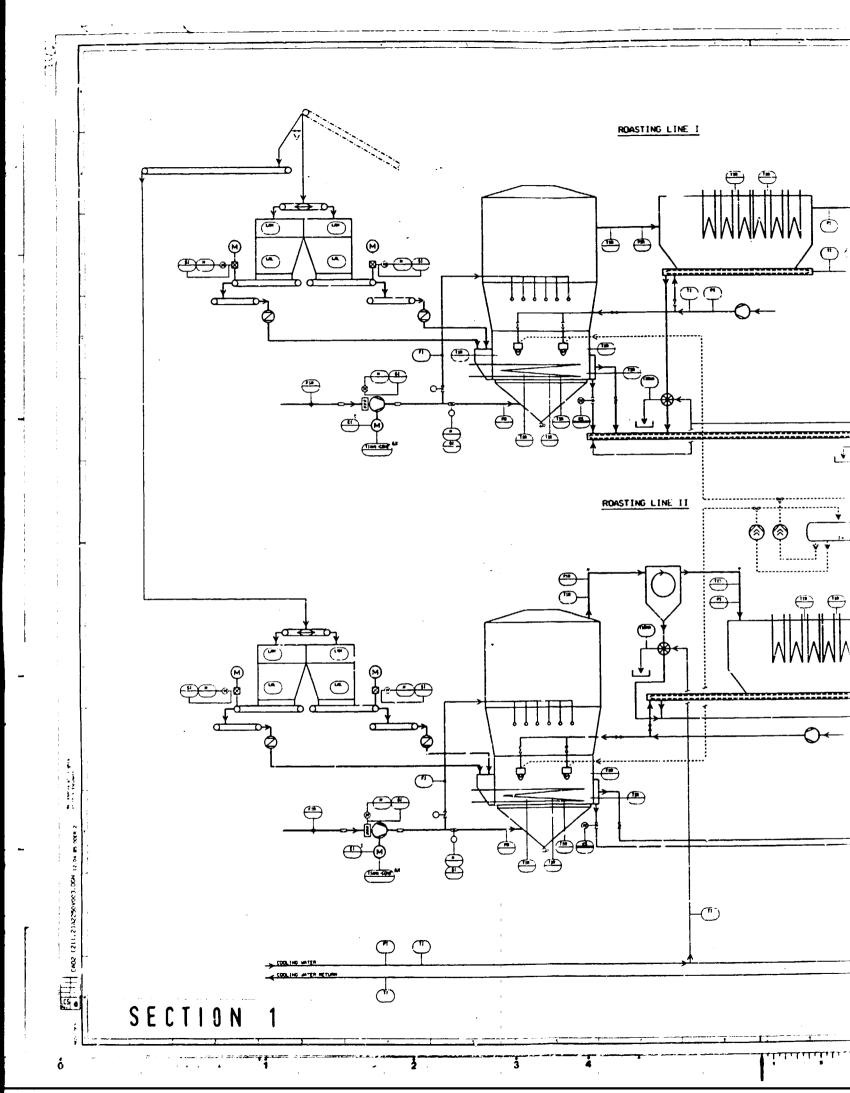
| 7.0 | List of Drawings | |
|-----|-----------------------|--|
| | L1A 00 2250 0000 1 00 | Pyrite Ore Preparation Plant |
| | L1A 00 2250 0000 2 00 | General Arrangement of Pyrite Ore Preparation Plant |
| | LOA 01 2250 0000 1 | Process Flow Sheet Roasting Plant |
| | LIA 01 2250 0000 2 | Waste Heat Utilization Sheets 1 - 2 |
| | LOA 01 2250 0000 3 | General Arrangement Roasting Plant |
| | LOA 01 2250 0000 4 | General Arrangement Poasting Plant |
| | LA 01 2250 0000 5 | General Arrangement Pyrite Plant |
| | T1A 03 2250 0000 1 | Gas Cleaning Plant |
| | L1A 03 2250 0000 2 | General Arrangement Gas Cleaning Plant |
| | IJA 02 2250 0000 1 | Flow-Sheet Drying and Absorption Plant |
| | L1A 02 2250 0000 2 | Flow-Sheet Converter Group |
| | L3A 00 2250 0000 3 | List of Consumers |

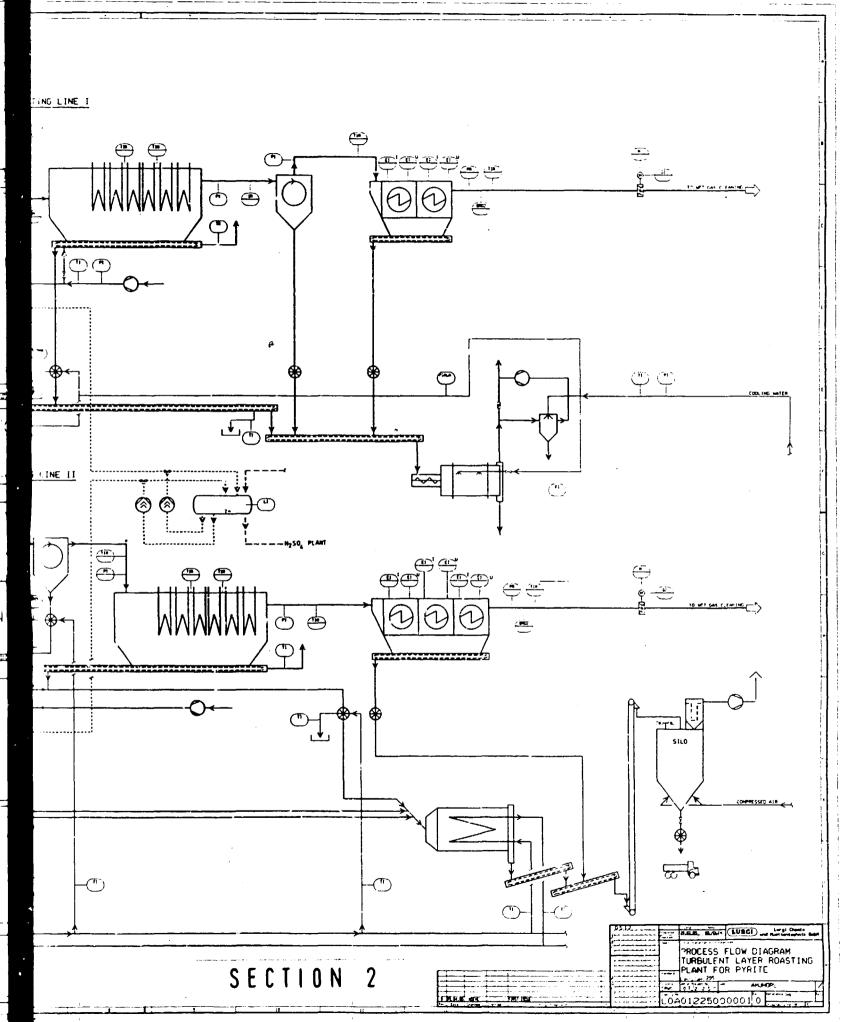


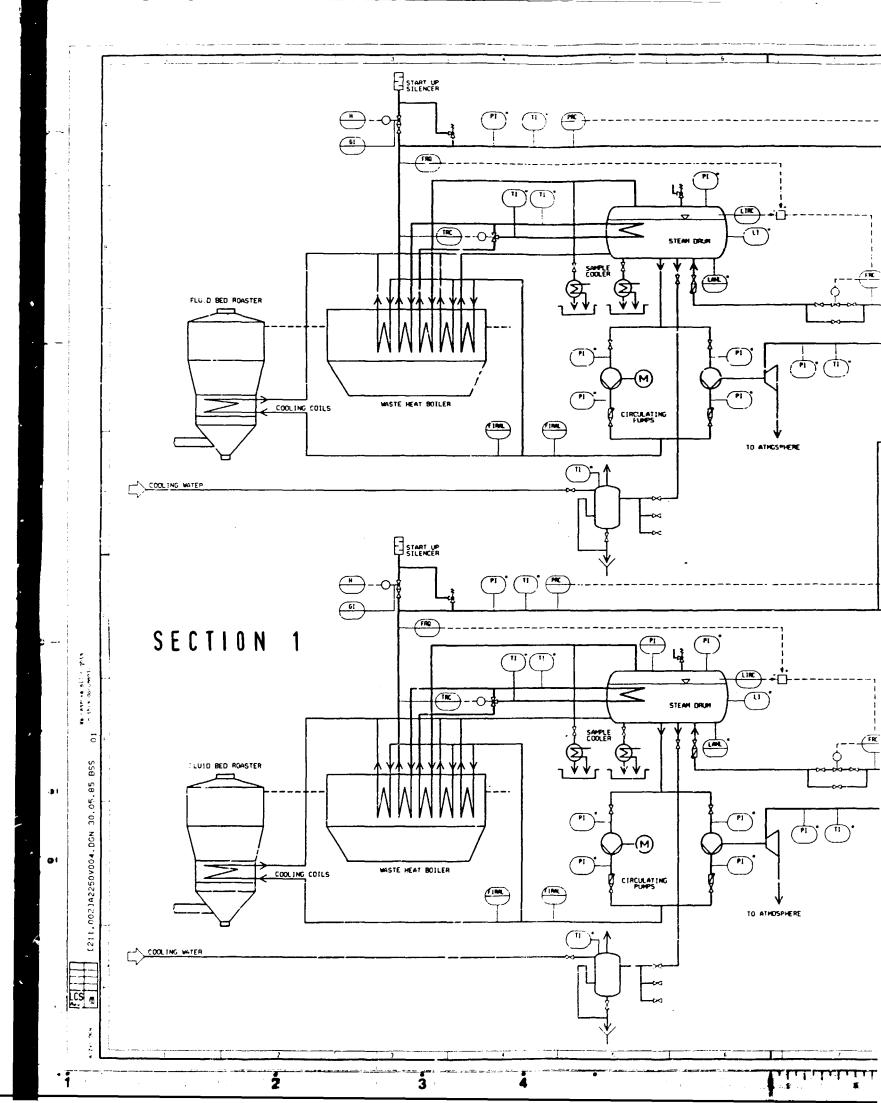


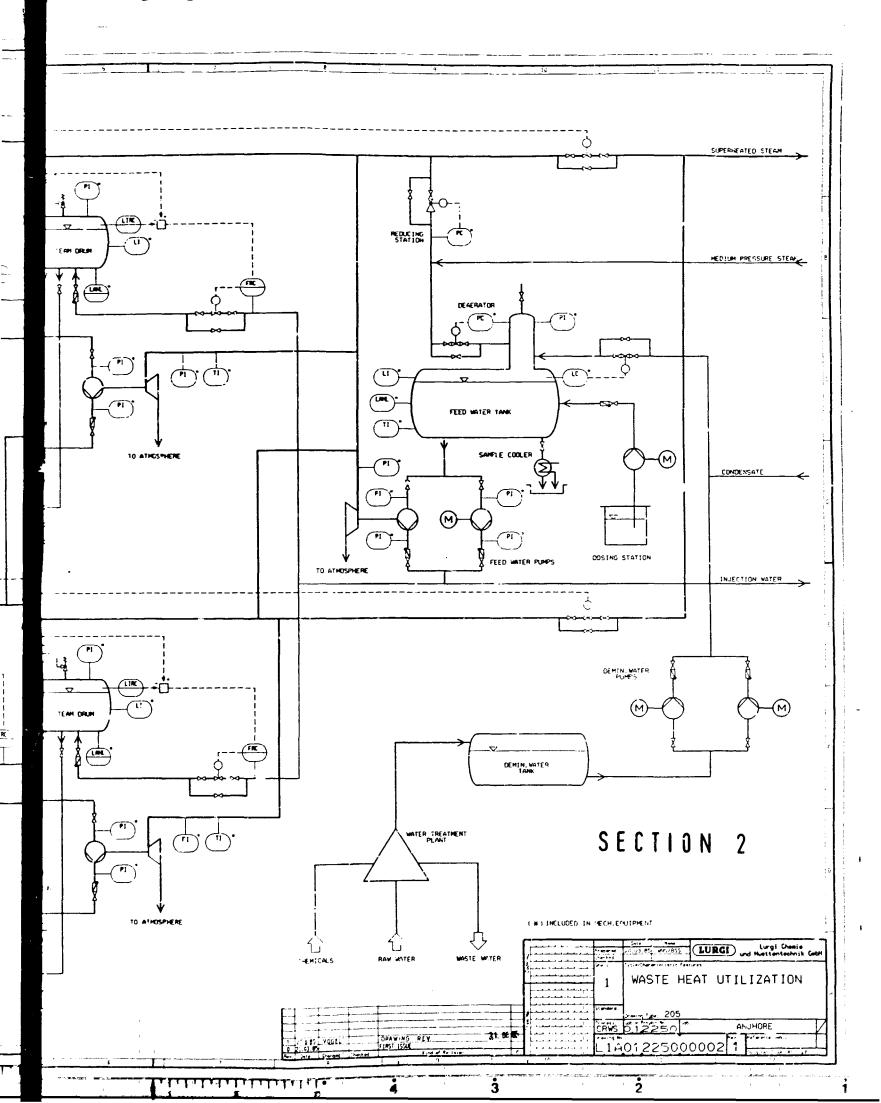


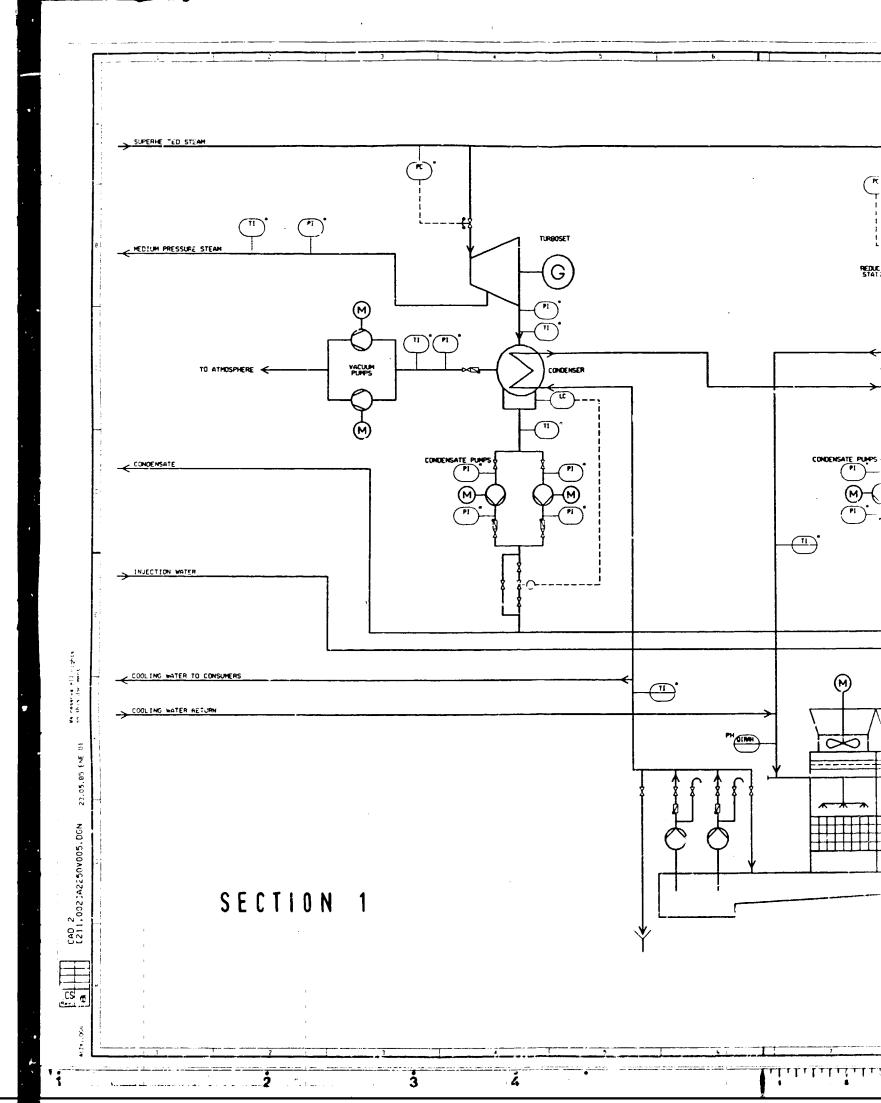


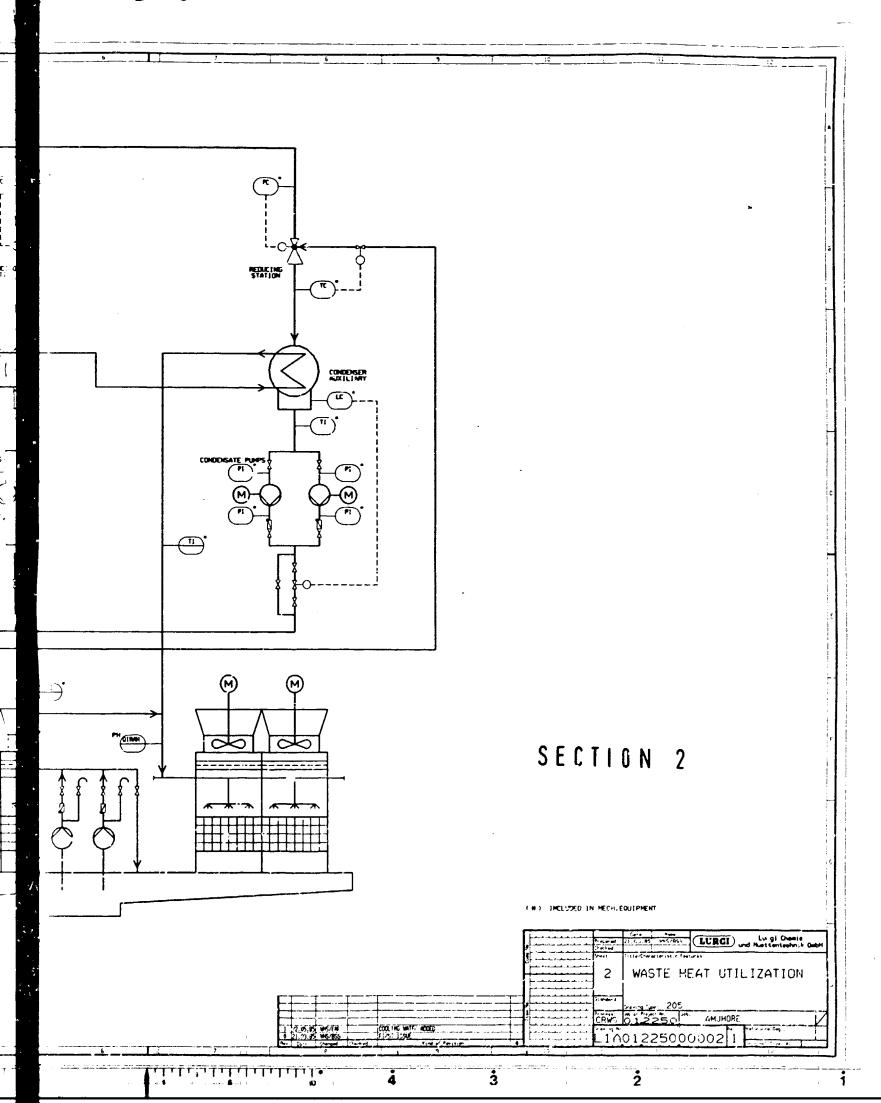


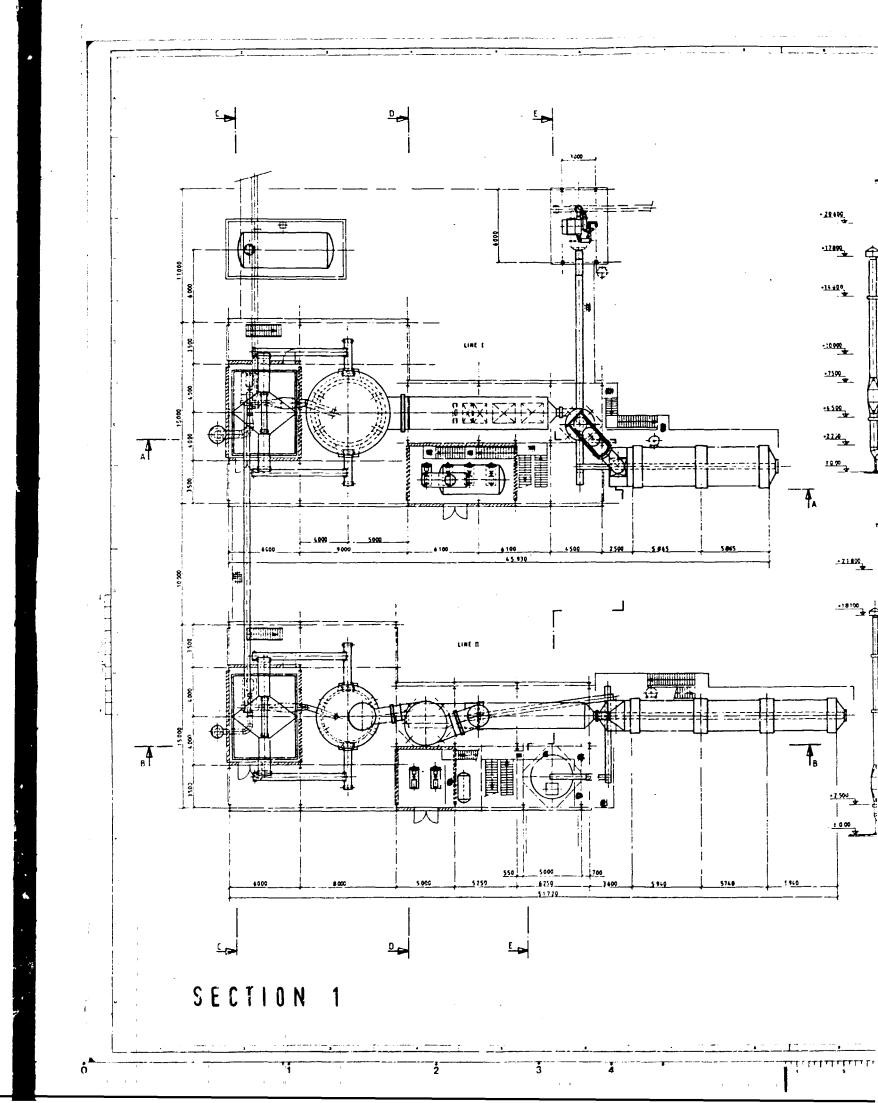


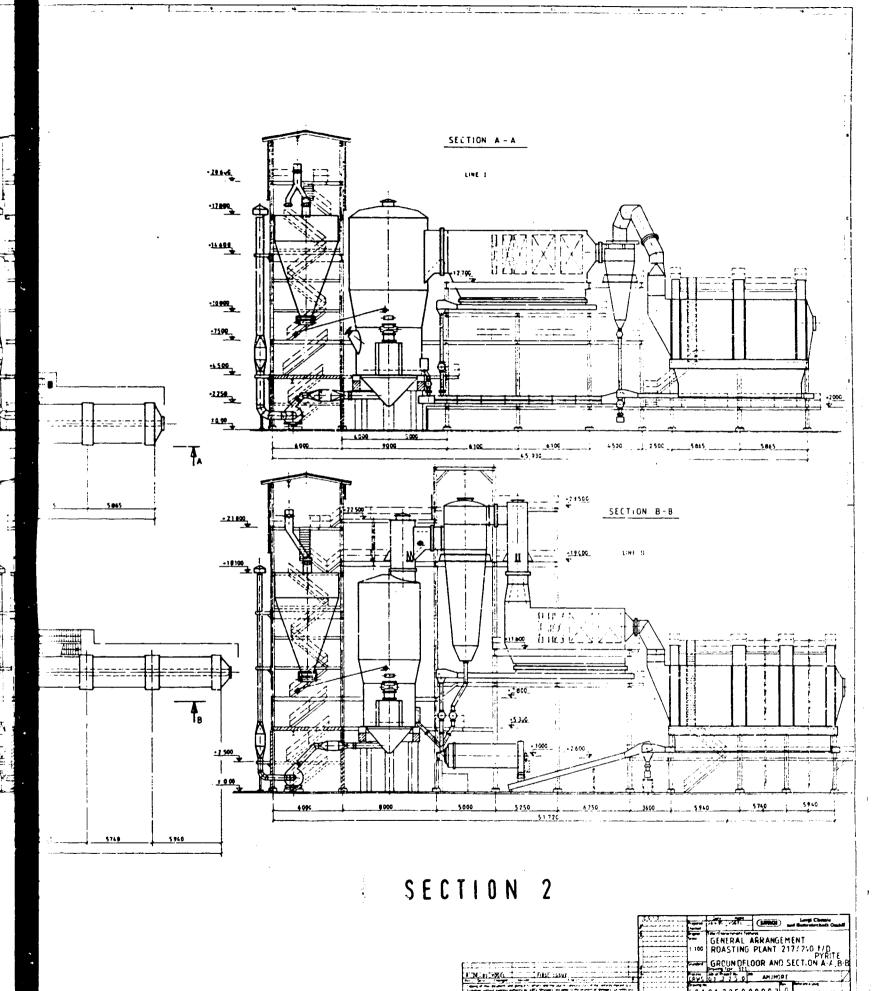




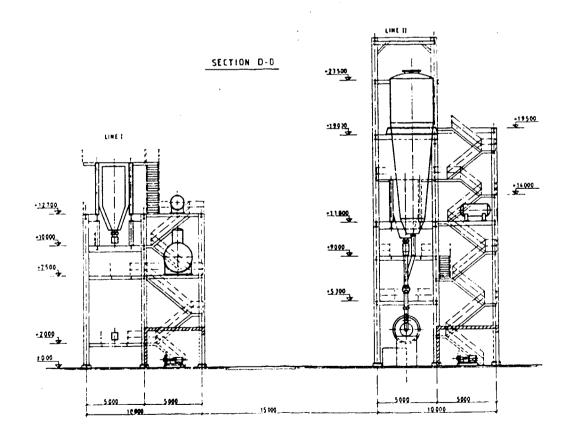








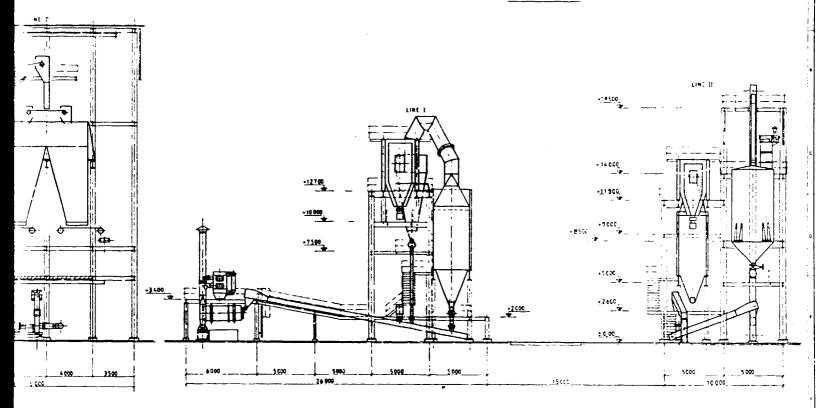
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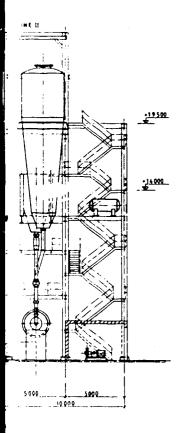


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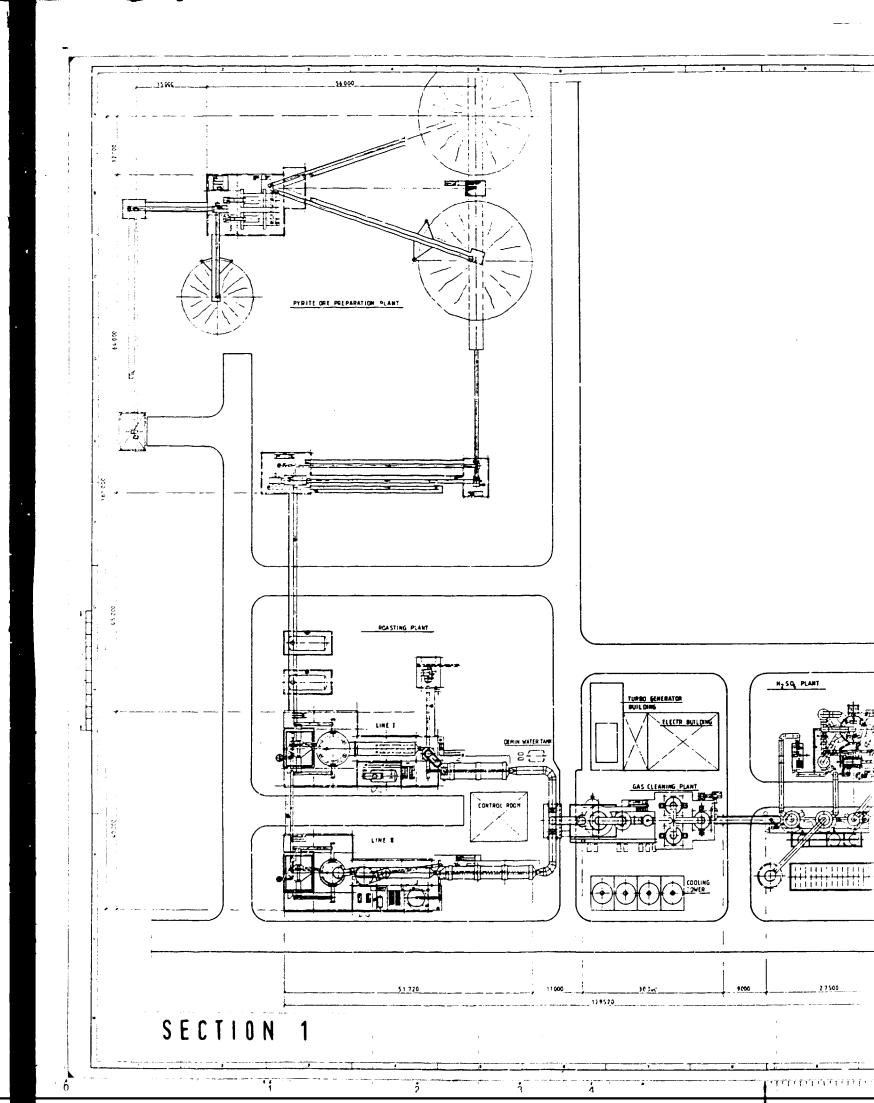


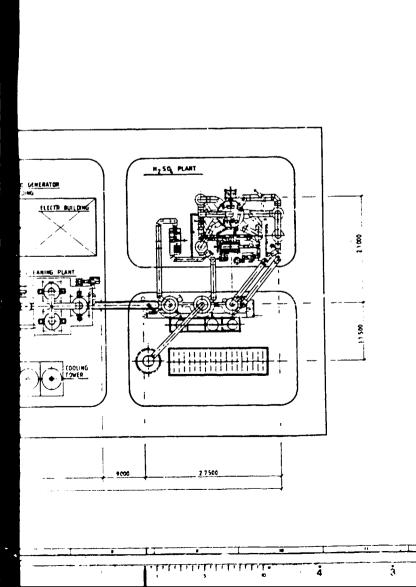
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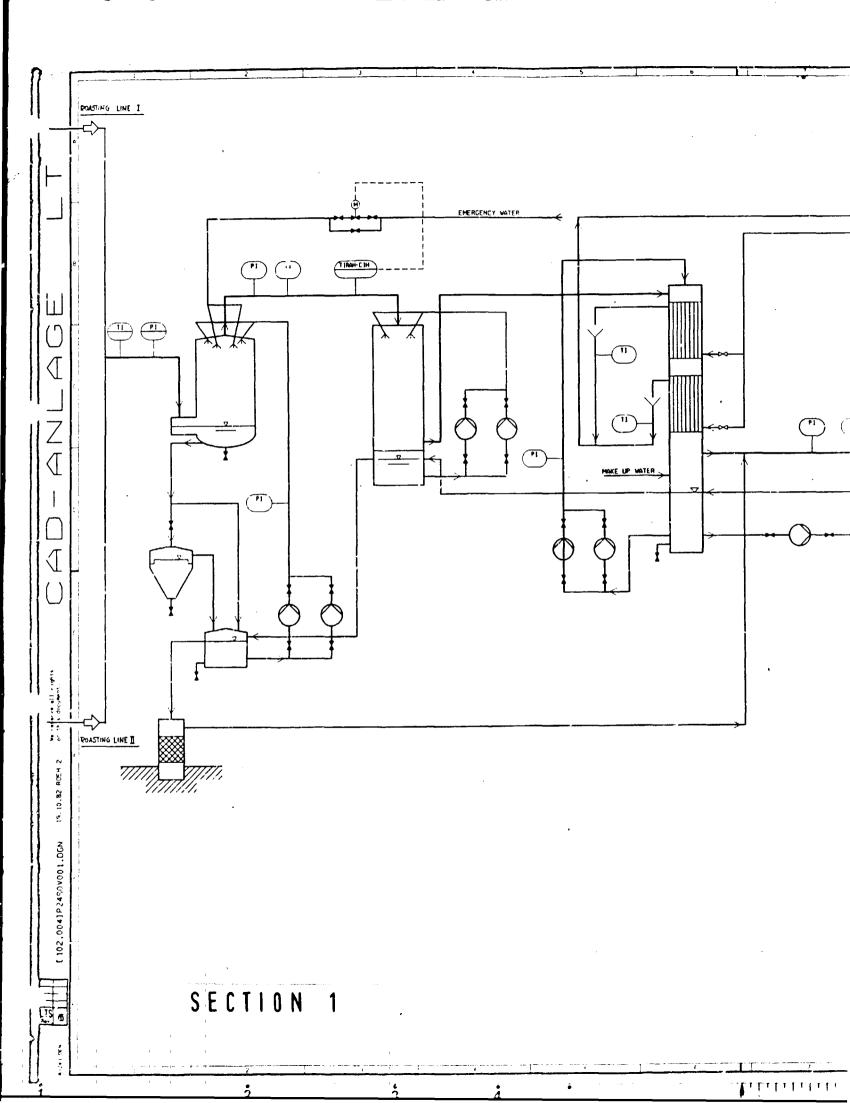


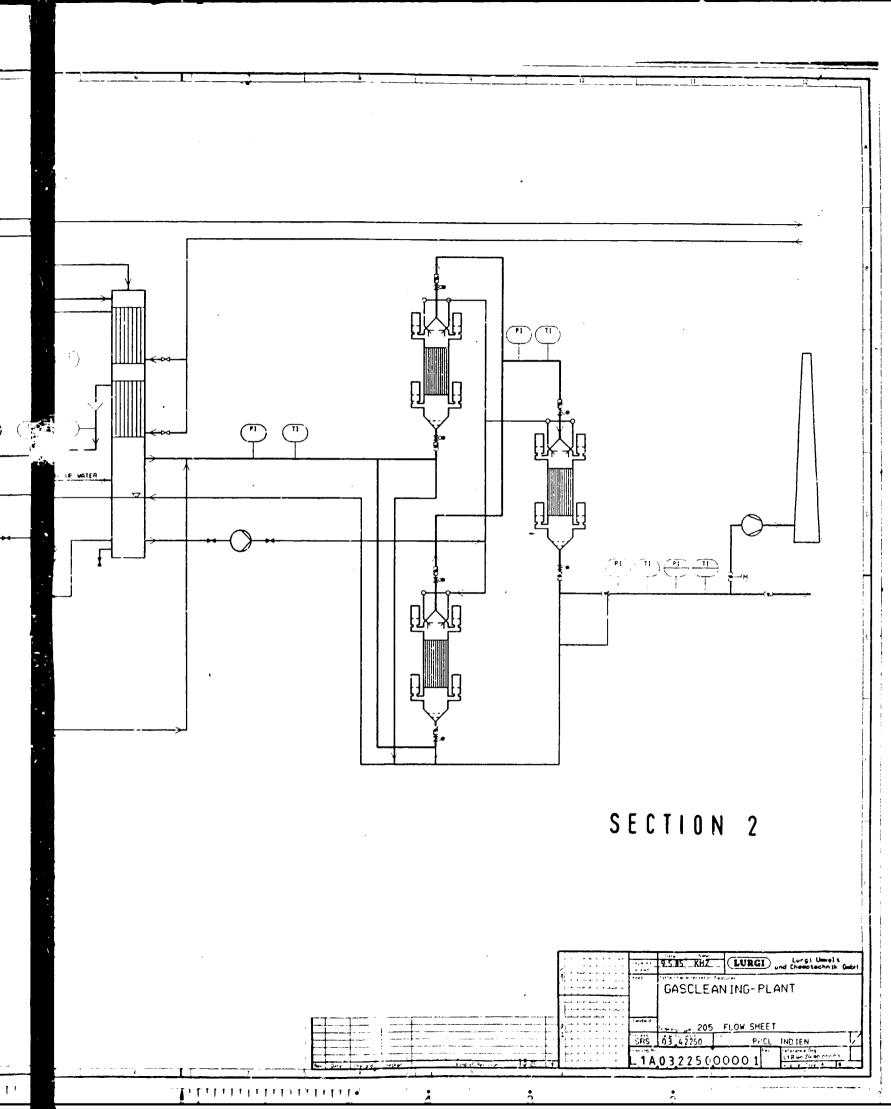


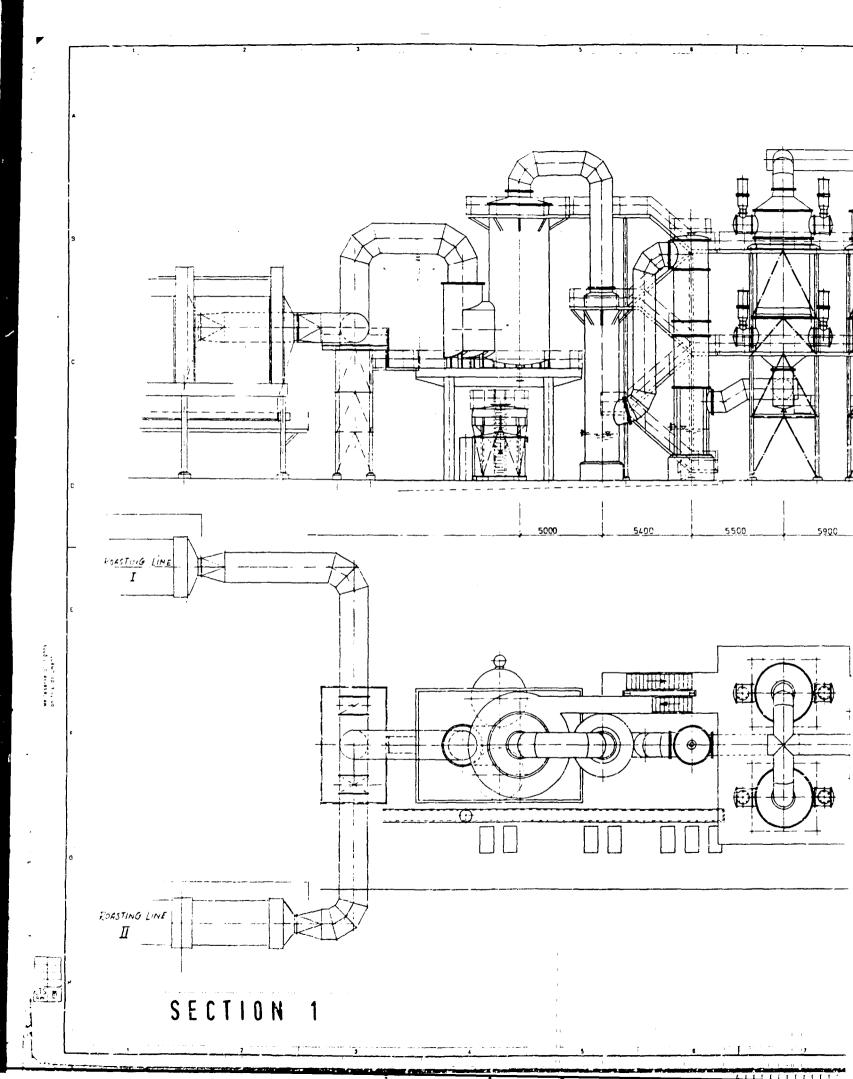
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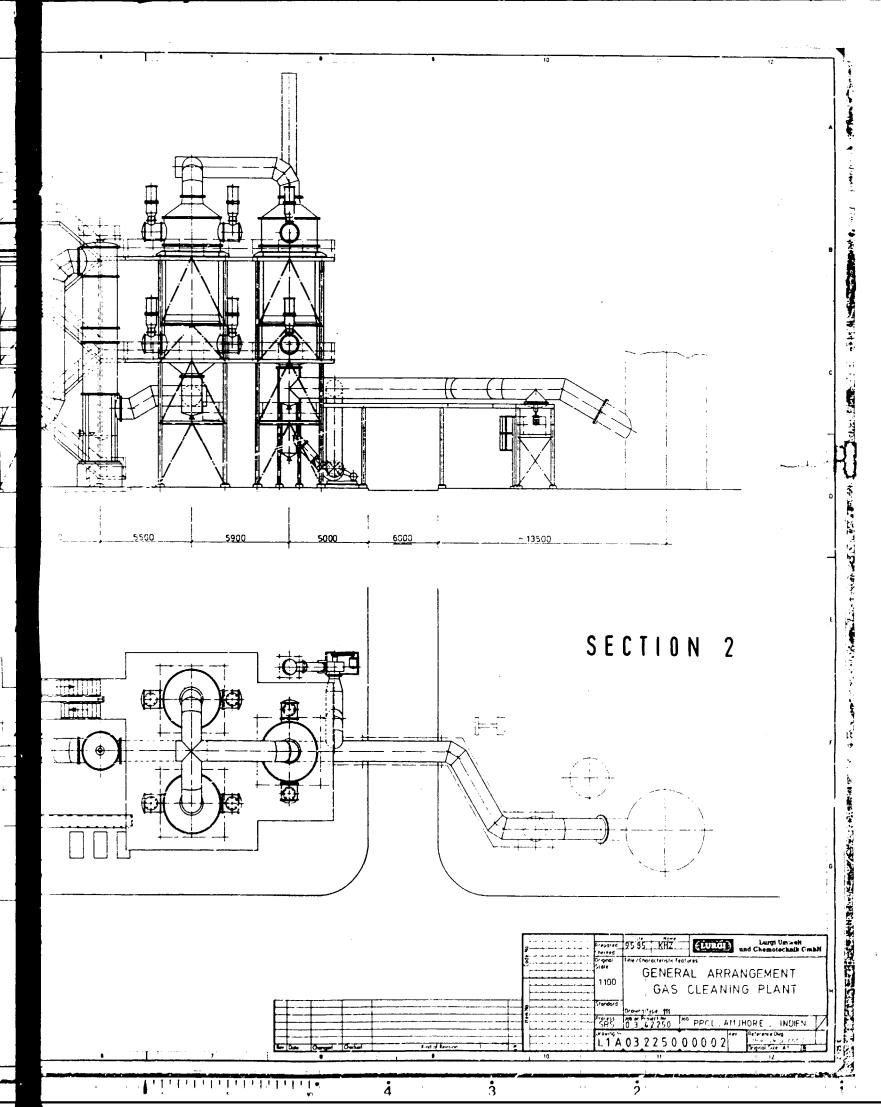
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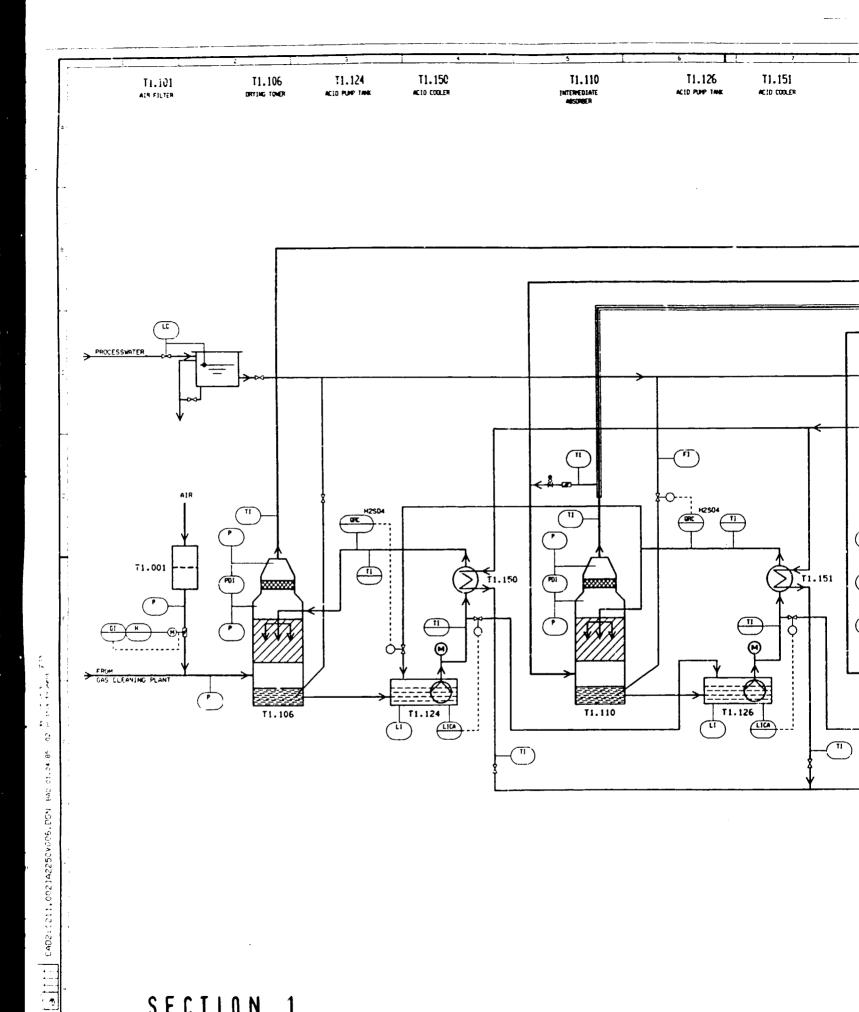
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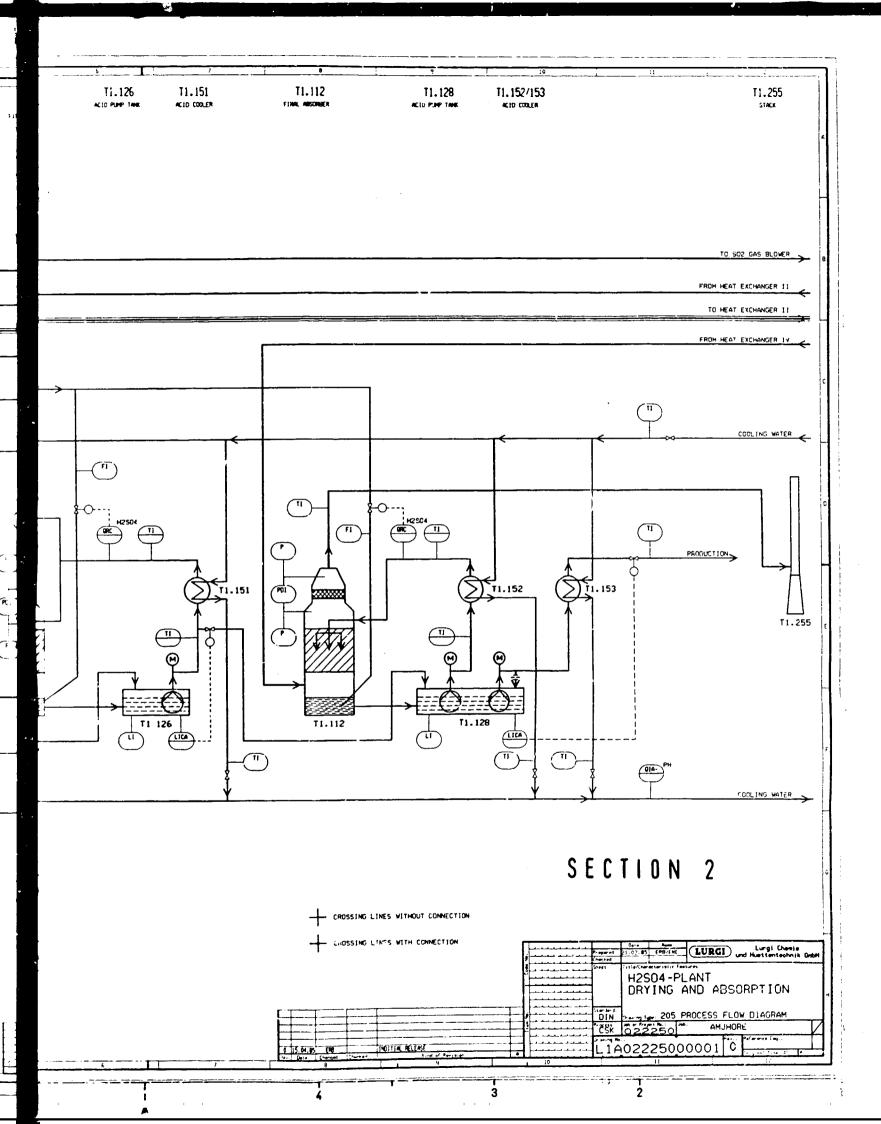


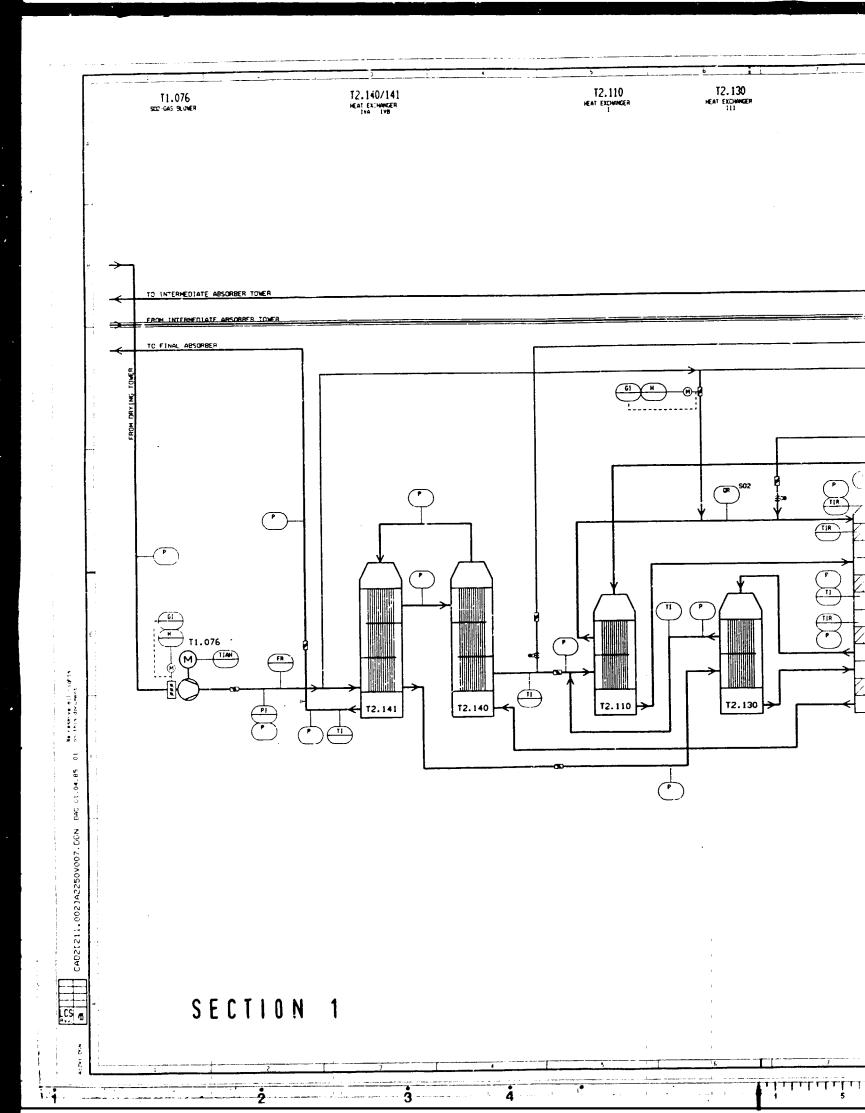


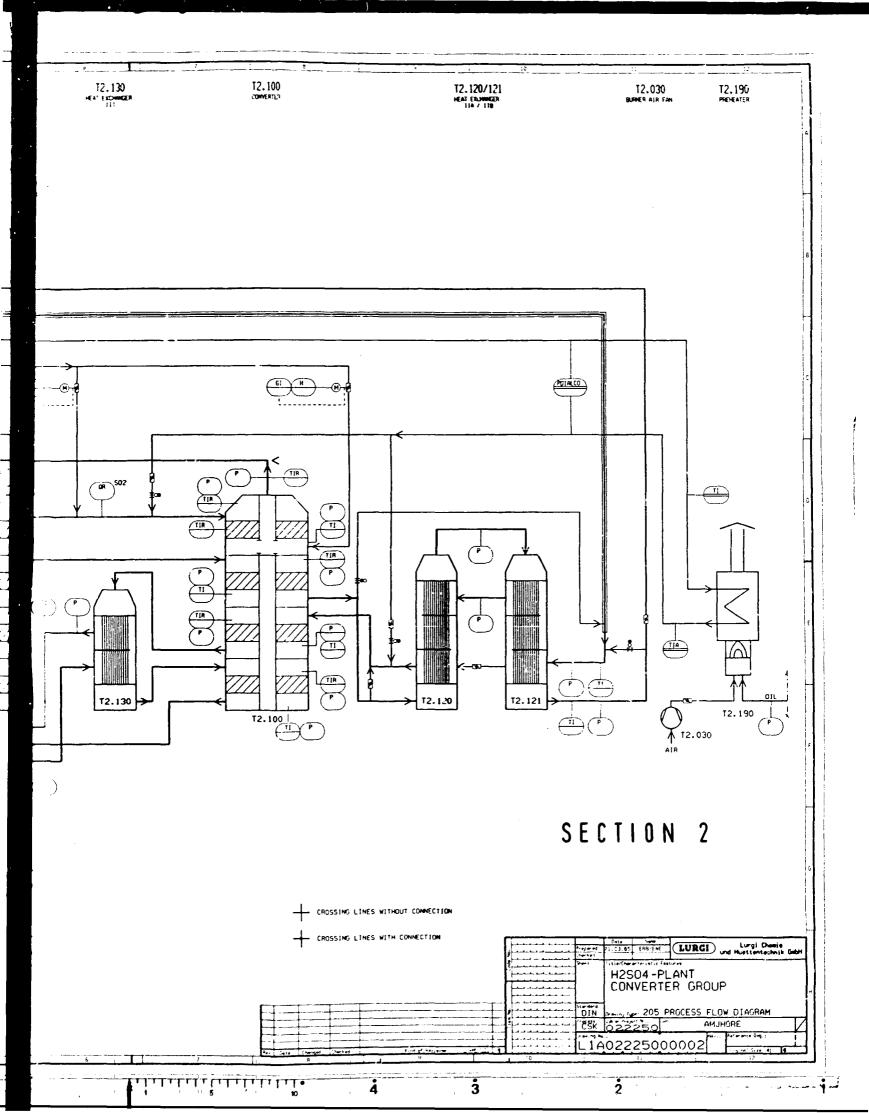




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 $M_{\mathbf{Q}}$: Anlaufmoment - Starting torque

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 M_n : Nennmoment - Rated torque I_a : Anlaufstrom - Starting current I_n : Nennstrom - Rated current

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| die alle I enthalt. 0197.3DE on indexes. | E1 026 | BELT CONVEYOR | / | | 4,3 | | | | 5,5 | 1500 | 415 | <i>83</i> | 3 | 1P574 | | |
| Folgeblatt zur Verbraucherliste F 10 197.3DE, die alle weiteren Angaben und den Anderungszustand enthält. Continuation sheet to list of consumers F 10 197.3DE showing all further information and the revision indexes | B1:027 | VIBRATION FEEDER | | | | | | | 1,5 | 1500 | 415 | | | | | |
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Continuction sheet to list of consumers F10197.3DE showing all further information and the revision indexes. IR2 003 BIN DISCHARGE CONVEYOR 83 1500 4,5 \mathcal{E} 1,250 5,5 IR2 003.1 415 SERVOMOTOR 0.37 IRZ.004 5,5 ح: بد BIN DISCLARGE CONVELOR 1500 83 3 1P374 TRZ 004 1 SERVO MOTOR 415 0,37 IR2.005 BELT CONVEYOR B3 \mathcal{B} 1854 415 1500 IR2 006 BELT CONVEYOR B3 415 B 1500 1054 Z IR2 007 B3 B 1P54 415 1500 BELT CONVEYOR IR2 008 1 BELT CONVEYOR 1500 415 B3 В 1P32 415 5-24,5 I (2 009 2,2 E3 ROTARY VALVE 5 1P34 210 2,2 10:76 ROTARY YALVE

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Ma: Anlaufmoment - Starting torque

J: Massenträgheitsmoment - Polar moment of inertia

 M_n : Nennmoment - Rated torque I_a : Anlaufstrom - Starting current I_n : Nennstrom - Rated current

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* (at shaft) Explosion profect. type % Starting ⊀ torque Insulation class No.req. Enclosure Rated voltage Mounting Rated Rated Reserve Active Мали Item No. Designation J kg m² kW min-1 3 4 5 12 14 15 2 6 7 8 9 10 11 13 1 TR3.010 B3 3 OIL PUMP 3 415 1.254 3000 For writerin Angaben and den Anderungszustand enthält Continuation sheet to list of consumers F10197,3DE showing all further information and the revision indexes. 195 1 IR3 012 ROASTING AIR BLOWER 83 = 1PS4 250 3000 6000 IR3 012.1 VANE CONTROL 0.27 415 TR3 015 ROASTING PIR FLAP 415 1,1 IR4 22 415 SIRCULATION PUMP 13 3000 E? 3 1P22 MAGNETTO VALVES IR4 5 05 220 SIEPNING CYSTEM LYDRAULIC PUMP FOR YUICK TR4 415 02 AUX. TURFINE LIGHTING LEVEL IR4 004 220 STEAM DRUM SECTION Summe Original-Summe 1.01-37-NG 2418 I LU Große Total Total Α3

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Mn: Nennmoment - Rated torque $I_{\mathbf{G}}$: Anlaufstrom - Starting current I_{D} : Nennstrom - Rated current Ausführungsbestimmungen Verbraucher - Consumers Design requirements Für diese Unterlage behal-ten wir uns alle Rechte vor. We reserve all rights on this document. Leistungs-bedarf (Welle) Antauf-moment X Nenn -Nenn -drehzahl Anzahl Nenn-spanng. Explosionsschutzart solierstoff Schutzart klasse Bauform Betrieb Reserve Herst Positions - Nr. Benennung min-1 kW % Mn ٧ kg m² protect, type *Power req. * (at shaft) Starting torque No.req. Insulation class Explosion Enclosure Rated voltage Mounting Rated speed * Rated * power Reserve Manufa Active Item No. Designation % Mn kg m² 14 15 3 4 5 10 11 12 13 1 6 7 8 9 REDLER 2,Z 1500 415 \mathcal{B} 1954 IR7.001 **B**3 Folgeviust zur verbraucherisse F 10 iv vous , die awe weiteren Angaben und den Anderungszustand enthalt Continuation sheet to List of consumers F 10197.30E showing all further information and the revision indexes. TR7.002 3 415 **B**3 3 REDLER 1500 iP54 IR7.003 REDLER 3 415 1500 B3 B 1P54 IR7.005 BLOWER 2z 3000 415 B3 سيجا 3 1500 IR7 007 1,5 4,5 ROTARY VALVE *B3* 122 3 1004 TR7. 012.1 SERVO MOTOR 1.2 415 COOLING AND NETTING IR7 014 1 415 1500 3 :P52 ВЗ DRUM 1500 34 IR7 014 1 2,2 FEED SCREW 415 63 В 1P54 IR7.018 SERVO MOTOR 1 415 SECTION Summe Summe Original-LUF \overline{I} Große ROASTING LINE Total Total A3

J: Massenträgheitsmoment - Polar moment of inertia

Ma: Anlaufmoment - Starting torque

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J: Massenträgheitsmoment - Polar moment of inertia Ma: Antaufmoment - Starting torque Mn: Nennmoment - Rated torque $I_{\mathbf{a}}$: Anlaufstrom - Starting current In: Nennstrom - Rated current Ausführungsbestimmungen Verbraucher - Consumers Design requirements Explosions-schutzart Leistungs-bedarf (Welle) Nenn -drehzahl Anlauf-moment Nenn-leistung indication terloye webat-ten wir uns alle Rechte vor. We reserve all rights on this document. Anzahl Nenn-spanng. Isolierstoff[.] klasse Schutzart Bauform Betrieb Reserve Her Benennung Positions - Nr. kW kW % Mn min-1 ٧ kg m² Explosion profect type * Power req. (at shaft) 5 Starting torque Insulation class No.req. Enclosure Rated voltage Mounting J. Rated Rated Reserve Manu Active Item No. Designation % Mn kg m² kW 3 4 5 6 7 11 12 13 14 15 9 10 8 1 T RZ.00Z REVERS. BELT CONVEYOR 2.2 415 *B3* В 1054 1500 Follower to the such that the support of the suppor BIN DISCHARGE CONVEYOR I RZ 003 5,5 1500 415 B3 B 1P54 415 I RZ 003.1 SERVOMOTOR 0,37 I RZ 004 BIN DISCHARGE CONVEYOR 5,5 415 *B3* 1234 1500 3 SERVOMOTOR II RZ 004.1 0,37 415 3 BELT CONVEYOR 415 \mathcal{B} E RZ 005 1500 *B3* 1952 CONVEYOR 3 II RZ 006 BELT 415 83 1500 \mathcal{B} 1P54 Z BELT I RZ 007 CONVEYOR 1500 415 B3 3 (PSU Rev BELT CONVEYOR 415 *B3* I RZ. 008 1500 3 1P54 3) Datum: I R2.009 ROTARY VALVE 5-21,5 415 *B3* B IPSZ 2,2 R2 010 ROTARY VALVE 5-21,5 415 2,2 83 В 1854 Summe Summe Original-ROPSTING $\overline{\mathscr{U}}$ LINE

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Sach-N M_{a} : Anlaufmoment - Starting torque J: Massenträgheitsmoment - Polar moment of inertia Mn: Nennmoment - Rated torque $I_{\mathbf{a}}$: Anlaufstrom - Starting current I_{D} : Nennstrom - Rated current Ausführungsbestimmungen Verbraucher - Consumers Design requirements Für diese Unterlage behal-ten wir uns alle Rechte vor. We reserve all rights on this document. Anlauf-moment × Nenn-Kieistung Explosicas-schutzart Leistungs-bedarf (Welle) Nenn – drehzahl Anzahl Nenn-spanng. Solierstoff klasse Bauförm Schutzar Betrieb Reserve J Her Positions - Nr. Benennung kW %*M*n ٧ min⁻¹ kg m² A Power req. (at shaft) Explosion profect.type Starting torque No. req. Insulation Enclosure .Rated voltage Mounting Rated speed Rated . Reserve Mani Item No. Designation class % Mn min -1 kq m² 3 4 5 6 9 10 11 12 13 14 15 2 7 8 1 I R3.010 3 OIL PUMP 45 B3 \mathcal{B} IP54 *300*0 Folgeblatt zur Verbraucheriiste F 10 1973 J.C., die alle weiteren Angaben und den Anderungszustand enthalt Continuation sheet to list of consumers F 10173 J.C. ..howing all further information and the revision indexes. I R3.012 160 3000 ROASTING AIR BLOWER 125 415 *B3* 3 1954 IR3 012.1 415 VANE CONTROL 0,37 I R3.015 ROASTING AIR FLAP 415 1,1 415 1,5 83 T. R3.019 ROTARY VALVE 3 IPS4 CIRCULATION PUMP 1 R4. /3 415 3 B3 1P54 3000 MAGNETTC VALVE FOR 5 II R4. 0,5 220 CLEANING SUSTEM Rev HYDRAULIC PUMP R4 0,2 415 QUICK START AUX. TURBINE LEVEL LIGHTING <u> I</u> 24 0.04 220 STEAM DRUM SECTION Summe Original-Summe RIOPSTING Große *77* LINJ E Total Total

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 M_{α} : Anlaufmoment - Starting torque

J: Massenträgheitsmoment - Polar moment of inertia

 $M_{\rm D}$: Nennmoment - Rated torque $I_{\rm G}$: Anlaufstrom - Starting current $I_{\rm D}$: Nennstrom - Rated current

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Mn: Nennmoment - Rated torque $I_{\mathbf{a}}$: Anlaufstrom - Starting current I_{N} : Nennstrom - Rated current Ausführungsbestimmungen Verbraucher - Consumers Design requirements - Anlauf Moment Memonent Für diese Unterlage behalten wir uns alle Rechte vor.
We reserve all rights on this document. Explosions-schutzart × Nenn -K leistung Anzahl Nenn-spanng. drehzahl Isolierstoff klasse Schutzart 3. Nenn – 5. drehzah Bauförm Reserve Betrieb Positions - Nr. Benennung Herst kW ٧ * Power req. % Starting ∡ torque No. req. (at shaft) Insulation class Explosion protect.type Enclosure Rated voltage Mounting ∃.Rated x Rated & power Reserve Manufa Item No. Designation kg m² 2 3 4 5 6 7 9 10 11 12 13 14 15 8 1 1500 ROTARY VALVE 415 2,2 B3 B T. R7. 015 IP54 Foigeblatt zur verztaurherliste F 1019/JUF, die alle weiteren Angaben und den Anderungszustand enthät Continuation sheet to List of Fonsumers F10197.30E showing all further information and the revision indexes. I R7. 018 SERVO MOTOR 1 415 SECTION Summe Summe Original-LUR LINE I ROASTING Große Total Total **A3**

J: Massenträgheitsmoment - Polar moment of inertia

Ma: Anlaufmoment - Starting torque

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Mn: Nerinmoment - Rated torque I_a : Anlaufstrom - Starting current $I_{\rm D}$: Nentistrom - Rated current Ausführungsbestimmungen Verbraucher - Consumers Design requirements Leistungs-bedarf (Welle) Explosions-schutzart Anlauf-moment run diese Unterlage behal-ten winuns alle Rechte von We reserve all rights on this document. Nenn-Leistung Anzahl drehzahl Nenn-spanng. Schutzart solierstoff Nenn -Bauförm klasse Reserve Betrieo Her: Positions - Nr. Benennung kW kW % Mn ٧ min-1 kg m² * Power reg. * (at shaft) Insulation class Explosion protect, type Starting No. reg. Enclosure Rated voltage Mounting Reserve Rated speed Rated power Manu Item No. Designation J %Mn kg m² kW min ⁻¹ 14 2 3 4 5 6 7 8 9 10 11 12 13 15 FEED WATER PUMP 25. 415 В **B**3 39 45 300s IPS4 ļ FEED WATER TANK Folgeniust zur verörauchersisse F10. 2008, die und weiteren Angaben und den Anderungszustand enthält. Continuation sheet to list of consumers F10.197.30E showing all further information and the revision indexes. R5. 1 415 DOSING PUMP 0,3 R5 FEED WATER PUMP 0,6 1,5 3000 415 ВЗ 3 ! 1P54 3,9 R5. FEED WATER PUMP 5,5 300s 415 *B3* \mathcal{B} 19.00 CONTROL BOARD R5 3 415 Z 25 0,3 415 DOSING PUMP COZ BLOWER FOR R5 1,5 415 83 3 30os PZU SPRAYER 3 Datum: R5 SERVICE PUMP 0,7 1,1 3000 415 1P54 83 В PJ 0.7 3000 415 SERVICE PUMP B3 \mathcal{B} ندرج Summe Summe Original-L TREATHENT Große WATER Total Total

Ma: Antaufmoment - Starting torque

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J: Massenträgheitsmoment - Polar moment of inertia

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J: Massenträgheitsmoment - Polar moment of inertia M_{n} : Anlaufmoment - Starting torque Mn: Nennmoment - Rated torque $I_{\mathbf{a}}$: Antaufstrom - Starting current I_{D} : Nennstrom - Rated current Ausführungsbestimmungen Verbraucher - Consumers Design requirements Explosions-schutzart Leistungs-bedarf (Welle) ton diese witerlage wehat-ten wir uns alle Rechte von We reserve alt rights on this document. Antauf-moment X Nenn -Nenn – drehzahl Anzahl Nenn-spanng. Schutzart solierstoff klasse Bauform Reserve Betrieb J Hers Benennung Positions - Nr. kW % Mn min-1 ٧ kg m² Explosion profect, type Starting Frongue Power reg. (at shaft) No.req. Insulation Enclosure -Rated Voltage Mounting Rated Kated Reserve Active class Manufo Item No. Designation j kW %Mn min-1 kg m² kW 12 14 15 3 4 5 6 7 8 9 10 11 13 2 1 0,75 415 ROTARY VALVE ZYCLON Folgonia: zur mitten und den Anderungszustand enthalt. Continuation sheet to list of consumers F10197.3DE showing all further information and the revision indexes. ROTARY VALVE 2 0.75 415 RECTIFIER TRANSFORMER KVA 415 35 HOT GAS PRECIPITATOR PERFORATED PLATE 2 0.015 415 RAPPER PLATE RAPPER 0,015 415 3 0,37 JIRE RAPPER 415 40 INSULATION HEATER 2 415 REDLER 2 3 415 SECTION Summe Summe Original-LUI HOT GAS PRECIPITATOR Große Total Total

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Mn: Nennmoment - Rated torque $I_{\mathbf{Q}}$: Anlaufstrom — Starting current $I_{\mathbf{n}}$: Nennstrom - Rated current Ausführungsbestimmungen Verbraucher - Consumers Design requirements rur diese Unterlage benalten wir uns alle Rechte vor. We reserve all rights on this document. Leishungs-bedarf (Welle) Anlauf-Explosions-schutzart × Nenn-Kleistung . Nenn – . drehzahl Anzahl Nenn-spanng. Isolierstoff Schutzart Bauform klasse Reserve Betrieb Positions - Nr. Benennung Hers kW % Mn ٧ min-1 kg m² Explosion protect.type R Power reg. (at shaft) Starting torque Insulation class No. req. Enclosure Rated voltage Mounting Rated speed Rated Reserve Active Item No. Designation J Manuf % M kg m² kW 3 4 7 9 12 15 8 10 11 13 1 1 36 45 1500 415 83 B SPRAYING TOWER PUMP 1P574 Folgebrain, Zen Victorius distriction, 1819 in the judit with westeren Angaben and den Anderungszustand enthält. Continuation sheet to list of consumers F10197.3DE showing all further information and the revision indexes. PUMP FOR STAND PIPE 5 415 B3 \mathcal{S} 7,5 1500 1P54 5 B3 1954 COOLING PUMP 7,5 1500 415 8 FILTER PUMP 16 18,5 1500 415 83 3 /PJC 3 RING COMPRESSOR 415 12 2,6 RECTIFIER TRANSFORMER KVA 3 415 27 WET GAS PRECIPITATOR SECTION Summe Summe Original-W WET GAS PRECIPITATOR Graße Total Total A 3

J: Massenträgheitsmoment - Polar moment of inertia

Ma: Anlaufmoment - Starting torque

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Ma: Anlaufmoment - Starting torque

J: Massenträgheitsmoment - Polar moment of inertia

 M_n : Nennmoment - Rated torque I_a : Anlaufstrom - Starting current I_n : Nennstrom - Rated current

Ausführungsbestimmungen Verbraucher - Consumers Design requirements Leistungs-: bedarf (Welle) Explosions-schutzart Antauf -Nenn-leistung Für diese Unterlage behal-ten wir uns alle Rechte vor. We reserve all rights on this document. Anzahl drehzahl Nenn-spanng. Isolierstoff Schutzar Bauförm Nenn klasse Betrieb Reserve Hers Positions - Nr. Benennung % Mn kg m k₩ គោin-1 ٧ Explosion protect, type Power req. (at shaft) Starting No. req. Insulation class Enclosure Rated voltage Mounting Rated speed Reserve Rated Manut Designation J Item No. %Mn kW kg m² lmin-1 12 15 3 4 5 9 11 13 14 2 6 7 8 10 SERVOMOTOR GAS FLAP 415 2,2 T1. 045 ı Folgeblatt zur Verbraucherliste F 10.197.3.DE, die alle weiteren Angaben und den Anderungszustand enthält. Continuation sheet to List of consumers F10.197.3.DE showing all further information and the revision indexes. T1 050 ACID PUMP DRYING ı 45 1500 415 11 \mathcal{B} 1PS4 В 55 1500 415 V1 IPS4 T1.053 ACID PUMP INTER. ABSORPT. 30 B 415 V1 /500 بريم/ T1 056 ACID PUMP FINAL AESOKPT. 3 11 h T1 060 ACID PUMP PROJUCTION 1500 1050 B3 3 1 2,2 415 1P:52 T1 062 1500 ACID PUMP T1.076 502 BLOWER 240 83 F 1000 1500 5000 P5: 415 B3 11 084 AUX. CIL PUMP 2,2 1500 В 1854 VANE CONTROL T1 081 415 0,5 415 T1.096 AIR FAN NOISE HOOD SERVOHOTOR GAS FLAP 415 T2 020 2,5 2,5 415 T2 021 SERVOMOTOR GAS FLAP 30 415 83 BURNER AIR FAM S 8 T2. 030 !500 /psz. 3 Datum: T2 (40 415 B3 \mathcal{B} 1254 DIL PUMP FOR BURNER 1500 OIL PUMP FOR BURNER 415 BS 72.041 1,5 1500 3 102 7 045 SONTROL BOFKS 415 Summe Summe Original-LU 42504 PANT Große Total Total **A** 3

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J: Massenträgheitsmoment - Polar moment of inertia Ma: Anlaufmoment - Starting torque Mn: Nennmoment - Rated torque I_0 : Antaufstrom - Starting current I_{N} : Nennstrom - Rated current Ausführung sbestimmungen Verbraucher - Consumers Design requirements Leistungs-bedarf (Welle) Explosions-schutzart Nenn – leistung Nenn – drehzahl rur diese unterlage behal-ten wir uns alle Rechte vor. We reserve all rights on this document. Anlauf-moment Anzahl Nenn-spanng. Schutzari solierstoff Baufèrm klasse Reserve Betrieb Hei Positions - Nr. Benennung kW kW% Mn min-1 ٧ kq m² Explosion protect, type F Power req. Insulation class Starting torque No. req. (at shaft) Enclosure Rated voltage Mounting Rated A Rated A power Reserve Active Man Item No. Designation % Mn kg m² min -3 4 5 7 9 11 12 13 14 15 6 8 10 1 CONDENSATE PUMP 8 15 415 83 1P54 1500 MAIN CONDENSER Folgetian Law Veranaucheriusie in 10.19, July, die July weiteren Angaben und den Anderungszustand enthätt. Continuation sheet to list of consumers F10.197.3DE showing all further information and the revision indexes. CONDENSATE PUMP 415 15 1500 **B**3 B 1P54 AUX. CONDENSER VACUUM PUMPS 7,5 1500 *B3* 3 415 1P54 SERVOMOTOR 0,75 415 0,5 REGULATING 415 VALVE AUX. OIL PURP 15 415 B3 B 1500 IP54 3 SERVOMOTOR 0,37 415 SECTION Summe Summe Original-4 Große TURED PITER NATOR Total Total

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