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To : Mrs Mounira Latrech

Contract officer

UNIDO headquarters

Final Report

For contract 98/134

Between UNIDO and Zhejiang Rongsheng Electric Co.Ltd.

From: Liang Rikui

Project Leader

Zhejiang Rongsheng Electric Co.Ltd.



中国浙江荣盛电器有限公司

CHINA ZHEJIANG RONGSHENG ELEC EQUIPMENT CO.,LTD.

公司地址: 浙江省吴山经济技术开发区

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TO:

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DATE: 21/12/1998

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PAGESL:

RE:

Mrs. M. Latrech
UNIDO, Vienna
Fax: 00 431 260 26 6815
Subject: Second Progress Report
Ref. Contract no. 97/134, Project no MP/CPR/97/195

Dear Mrs. Latrech

I am glad to submit to you RSLG second progress report regarding achievement of our various activities to execute contract no 97/134.

We would like to acknowledge the deep cooperation between UNIDO and our company for implementation of the CFC phase project.

1.2 Zhejiang Rongsheng Electronic Co. Ltd.

Zhejiang Rongsheng Electronic Co. Ltd(Rongsheng) is a collective ownership plastic cement, refrigerator and freezer manufacturing company. The company was established in 1988. The plants are located in Deqing County and produce five different products: Horizontal Freezer and Freezing Showcase, Vertical Refrigerating Showcase, Twin Temperature Freezing Showcase, and Plastic Cement.

The production of freezers in Rongsheng started in 1994 with 440 employees. Currently, there are 800 employees, of which, 75 are in the management department and 90 are technicians.

The daily production rate of the factory is about 800 units in two shifts. In 1996 the actual production was 146,186 freezers.

The Company produces 13 models in eight basic size ranges between 98 and 510 litres including Upright Cooler and Chest Cooler/Freezer.

The factory is operating with CFC-12 and CFC-11.

Table 7. Volume of refrigerator production at RONGSHENG

Year	Units
1994	60,058
1995	132,165
1996	146,186
1997 (expected)	230,000

Table 8. Product mix of RONGSHENG

<i>Model</i>	<i>Description</i>	<i>Share in total production, %</i>	<i>Charge, g/unit</i>	<i>Foam weight (cabinet + door) kg/unit</i>
BD-98	freezer, volume 98 l	6.7	150	3.3
BD-122	freezer, volume: 122 l	10.1	155	4.2
BD-158	freezer, volume: 158 l	21.3	155	4.84
BD-172	freezer, volume: 172 l	39.8	175	5.54
BD-268	freezer, volume: 268 l	10.3	205	7.1
BD-308	freezer, volume: 308 l	5.1	209	8.07
BD-408	freezer, volume 408 l	4	265	9.58
BD-510	freezer, volume 510 l	3	315	11.50
Total or average		100	179.66	5.77

Rongsheng is currently running two production lines for foaming and two for assembly of products. They are installed in two separate buildings. One assembly

line is placed in one building and two foaming machines (the cabinet and door foaming lines) and the second assembly line are in another building. The thermoforming machine is located in a separate building.

Rongsheng manufactures 40% of components for the use in their refrigerators. About 10% of the compressors are imported the rest are of domestic origin.

The freezer compartments are equipped with plate tube type evaporators produced locally.

The polyol, isocyanate and the CFCs are from ICI. There is 17% CFC-11 in the currently applied formulation on two lines as foam blowing agent. The technologies and some of the equipment are of Chinese origin, there is no technological agreement with any major international producer regarding refrigerator manufacturing. The foaming of cabinets are carried out in bath position. The arrangements for doors and cabinets are made in carousel. Preheating of cabinets and doors before foaming are with hot air. The preheating ovens are heated with steam. Curing time is eight minutes.

The major manufacturing equipments are as follows:

- 1 set High pressure cabinet foaming machine with one foaming head. Manufactured by Cannon A-100 system, Italy 1994
- 1 set Cabinet foaming carousel with up to 20 moulds. Manufactured by Jiangsu Kunshan Moulds Factory, China
- 1 set Low pressure door foaming machine with one foaming head. Manufactured by Cannon A-40 system, Italy 1989
- 1 set Door foaming carousel with 12 moulds (double) moulds. Manufactured by Jiangsu Kunshan Moulds Factory, China
- 2 sets Preheating oven heated with steam
- 2 sets CFC-12 refrigerant charging boards type 150 Manufactured by Shanghai Aeroplane Manufacturing Co. China
- 2 sets Evacuation carousel equipped with 40 vacuum pumps. Shanghai Vacuum Pumps Factory. 2x2 - 4 Manufactured in China 1993
- 3 sets Leak detectors used on the production and testing lines Manufactured in China 1993

1 set Testing conveyor for testing 120 units simultaneously. The refrigerator travel at 60 Sec./unit speed

1 set Fully automatic thermoforming lines, type: four position. Manufactured by Hungary in 1988. The lines produce inner liners from ABS sheet.

The quality control is extended to every piece (electrical safety, cooling performance), and random thorough tests are applied for a part of the production. Rongsheng has a test room equipped with basic instruments to measure the performance of refrigerators. The appliances designed for refrigerator 5° C and for freezer -18° C. According to the Chinese standard the performance is tested at ambient temperature 16-32°C, 60% humidity.

In 1996 Rongsheng used approximately 27.5 mt of CFC-12 and 150.3 mt of CFC-11

II. PROJECT OBJECTIVE

The objective of this project is to eliminate the use of CFC-11 and CFC-12 in the production of domestic refrigerators/freezers and in refrigeration servicing at Rongsheng through conversion to the use of HFC-134a as refrigerant for the cooling system and cyclopentane as blowing agent for the polyurethane insulation foam

The project will be finalised by end 1999 and thus will contribute to the freeze target of the country by phasing out 177.5 ODP tonnes in line with NEPA's ODS phase out programme.

III. PROJECT DESCRIPTION

Rongsheng has already recognized the need to comply with the Montreal Protocol and has agreed to participate in China's ODS phase out programme. It is prepared to phase out ODS as soon as the new technologies have been acquired, the necessary machinery installed and the technical staff have been trained. Rongsheng is committed to phase out CFCs by converting its foaming equipment to cyclopentane use and using HFC-134a as refrigerant.

This project document describes the activities needed to carry out the phase out process.

III.1. Justification for Selection of Alternative Technologies

III.1.1. Refrigerant

Among the technological options currently available on commercial basis (see Table 9) and in line with the established policy of NEPA and CNCLI to phase out the use of ODS. In the selection of the substitute refrigerant technology for this project the following factors were also taken into account:

Activities

We are delighted to explain some of our activities during execution of the project.

Achievement of Calculation of Models and Methods of Calculation

Calculation of models for redefinition of the prototypes for conversion into R134a refrigerant circuit system.

We chose ASHREA standard to calculate refrigeration load necessary to determine suitable components specially compressor that is the heart of refrigeration system. Other components such as Capillary tube, Evaporator, and condenser are relatively adjusted to achieve best results. In order to determine the correct amount of R134a refrigerant charge, and other data such as pressure at different point of refrigeration circuits, we have to know the performance characteristics of each component, such Suction and Discharge temperature of compressor, inlet and outlet temperature of condenser or saturated liquid and vapor temperature, therefore we should perform theoretical cycle calculations for both pure refrigerants and blends.

The theoretical performances can be compared to one of the following CFC/HCFC fluids: R12, R502 and R22. The calculations are best used as a means of finding trends in fluid performance. The cycle has not been designed to model experimental equipment in detail. Several factors, such as those from heat exchangers and compressor volumetric inefficiencies are not included in the theoretical cycle.

Definition of the Theoretical Cycle:

The calculations are based on a point cycle. The points are as follows

- (1) Evaporator Inlet - Liquid/vapour flash
- (2) Evaporator Outlet - Saturated Vapour
- (3) Compressor Inlet - Superheated Vapour
- (4) Compressor Outlet - Compressed Vapour
- (5) Condenser Inlet - Saturated Vapour
- (6) Condenser Outlet - Saturated Liquid
- (7) Expansion Device Inlet - Subcooled Liquid

INPUT FIELDS

Evaporator Temperature: defined as the average of the liquid/vapour flash temperature at the evaporator inlet and that of the saturated vapour at the evaporator outlet. The latter is taken to be the dew point temperature at the calculated evaporator pressure. Unlike pure refrigerants, for the R32/R125/R134a blends the inlet and outlet temperature will be different.

Condenser Temperature: defined as the average of the temperature of the

saturated vapour at the condenser inlet and the temperature of the saturated liquid at the condenser outlet. They are taken to be the dew and bubble point temperatures respectively at the condenser pressure.

Superheating: defined as the temperature difference between the superheated vapour at the compressor inlet and the saturated vapour at the evaporator outlet. It is assumed that the compression process begins under identical conditions to those at the compressor inlet i.e. the compressor inlet conditions are the same as the suction conditions.

Sub-cooling: defined as the temperature difference between the saturated liquid at the condenser outlet and that of the sub-cooled liquid at the expansion device inlet.

Efficiency: An isentropic compression process is used for the theoretical cycle calculations. The isentropic efficiency is the value, relative to a theoretical maximum of 100%, of the efficiency with which the compressor can isentropically compress the superheated vapour from the suction pressure up to a pressure equivalent to the condenser pressure. It scales directly with the required compressor power.

The Constraint: Cooling Duty or Volumetric Flowrate:

In order to compare the calculations of several refrigerants on the same basis there is an option to constrain either the cooling duty or the volumetric flowrate of the superheated vapour prior to compression (i.e. the compressor inlet).

Cooling Duty: the required cooling capacity of the system. In this program, it is defined as the cooling that occurs from directly after the expansion device to the evaporator outlet i.e. the saturated vapour condition.

Volumetric Flowrate: defined for the superheated vapour immediately prior to the compression process (i.e. at the compressor inlet point).

DEFINITION OF CALCULATED FIELDS

Pressure: the pressure for which the average of the calculated evaporator inlet and outlet temperatures give the input evaporator temperature.

Condenser Pressure: the pressure for which the average of the calculated condenser inlet (dew point) and outlet (bubble point) temperatures give the input condenser temperature.

Coefficient of Performance: the ratio of the refrigeration effect to the heat of compression. The refrigeration effect is defined in two ways, as the difference between the evaporator inlet condition (expansion valve outlet) and either the evaporator outlet condition (exclusive of superheating), or the compressor inlet condition (inclusive of superheating). The heat of compression is defined as the enthalpy rise of the vapour as a result of the compression process.

EER - Energy Ratio: the ratio of the gross capacity (see below) in Btu/hr to the compressor power in watts. The EER has been defined in this way for all cycle calculations, including those in SI and METRIC units.

Cooling Duty: same definition as given in input fields.

Gross Capacity: The calculated gross cooling capacity of the system. It is defined as the cooling that occurs from directly after the expansion device to the compressor inlet i.e.. superheated vapour.

Compressor Power: The heat (enthalpy) required from the compressor.

Mass Flow rate: The refrigerant mass flow rate required around the system to meet the input constraint value at the input conditions.

Suction Line Temperature: The temperature of the superheated vapour at the compressor inlet point.

Discharge Temperature: The temperature of the compressed vapour at the compressor outlet, which in this cycle is also taken as the point at the end of the compression process.

Temperature Glide in the Evaporator: The difference between the evaporator inlet and outlet temperatures.

Temperature Glide in the Condenser: The difference between the condenser inlet and outlet temperatures.

Refrigeration Load Calculation for Upright Ref.- Freezer, Chest Freezer and Display cases

Refrigeration load consist of three individual components:

- 1- Transmission load;
Heat transfer through side walls by conduction
- 2 - Product load;
Heat Removed from and produced by the products which are stored.
- 3 - Internal load;
Heat produced by internal sources such as lights, fan or heaters;
- 4 - Infiltration load
Heat gains associated with air entering the refrigerated space and door opening and etc.;

In this section , the above mentioned components will be discussed separately to analyze and extract the most useful and practical equipment's.

- 1) Making Prototypes;
- 2) Testing Prototypes;
- 4) Calculating Heat Leaks;
- 5) Being familiar with Montreal Protocol and UNIDO's Projects;
- 6) Being familiar with aim of the project in Iran;
- 7) Selecting Components for each models;
- 9) Preparing Technical Specifications and Characteristics;
- 10) and other services as mentioned in the subject contracts;

Activities

Following activities were accomplished during execution of the contract

- 1 - Collecting necessary data from each .

- 3 - Measuring Actual Dimension of each model;
- 4 - Reviewing and evaluating data
- 5 - Performing heat leak calculation for models
- 6 - Determining heat loads for models;
- 7 - Determining product load for models;
- 8 - Determining heat gain by infiltration;
- 9 - Preparing data acquisition form;
- 10 - Preparing product specification models;
- 11 - Preparing prototype data summary sheet;
- 12 - Recommending suitable compressors for each prototypes;
- 13 - Reviewing more than 30 compressor technical specifications

in

order to recommend an appropriate compressor as follows

a - Danfuss;

TL5G, TLS6F, TLS7F, FR7.5G, FR8.5G, and FR10G

b - Gold Star;

NR45L, NF45N, NR62L, NR52L, VF75N, V75L

c- Matsushita;

SA3C10AX0, QA66C15RAX5, QA77C18RAX5, D66C15RAX5,
D77C18RAX5, QA,51C11RAX5, QA91C20RAX5, S43C10KAX0

d - Necchi;

ESC5, ESC7K, ESC7, ESC8.5, ESC8.5K, ESC9, ESC9K, ESC11,
ESCHK,

e - Zanussi

GL45AA, GL50AA, GL60AA, GL70AA, GL80AA, GL90AA, GL99AA,
GL80AH,

d- Aspera

BP104822, BP1116Z, BP1118Z

e- Techomseh

Different models of Techomseh compressor specifications were reviewed and we finally chose appropriate compressor models for each models and we decided to install Techomseh Compressor on our prototypes, because we believe that the technical specification of these compressor matches our refrigeration load requirements.

Method of Refrigeration Load Calculation

Refrigeration load consist of four individual components:

- 1- Transmission load;
Heat transfer through walls (sides, back panels, top and bottom) and door panel.
- 2 - Product load;
Heat Removed from and produced by the products which are brought and stored in the refrigerator;
- 3 - Internal load;
Heat produced by internal sources such as lights, fan or heaters;
- 4 - Infiltration load
Heat gains associated with air entering the refrigerated space;

In this section , the above mentioned components will be discussed separately to analyze and extract the most useful and practical equipment□s.

Transmission Load

Heat gain through walls of a refrigerated space depend on cabin Temperature, liner, insulation and cabin conductivity and also the surrounded ambient air. In other word, there are four different resistance opposing heat flow between cabin space and ambient air as given in resistance circuit.

Considering the above mentioned resistances, R_l , R_c and R_a are not compareable in magnitude with R_i (Insulation resistance) and so can

be neglected in our calculations. Therefore, the resultant circuit and related equations is.

$$R = \frac{x}{KA} \text{ Heat Resistance and } Q_{\pi} = \frac{\Delta T}{R} \text{ Heat Transfer}$$

Where:

x = Insulation Thickness, mm

K = Insulation Conductivity, $\frac{Wmm}{m^2 \cdot C}$

A = Outside Area, m^2

ΔT = Temperature difference ($T_a - T_c$), C

If the insulation thickness of side walls, back panels, top, bottom and door are different, heat transfer for each part can be calculated separately and then summed for two door refrigerators, due to different cabin temperature of freezer and refrigerator compartments, heat transfer for each compartment should be calculated separately and then added together.

Product Load

Heat removed from products (meat, fruits, vegetables, water and etc.) to reduce temperature from receiving to storage temperature is known as product load. Following steps can be taken to calculate product loads.

1 - Heat removed from initial temperature (T_i) to storing temperature (T_{rs}) in refrigerator compartment is;

$$Q_{rs} = \dot{M}C (T_i - T_{rs})$$

Where:

\dot{M} = Mass of product, Kg / h

C = Specific heat of product, Kcal / Kg

2 - Heat removed from initial temperature (T_i) to freezing temperature (T_f) is ;

$$Q_{af} = \dot{M} C (T_i - T_f)$$

Where :

\dot{M} = Mass of product, Kg / h

C = Specific heat of product above freezing point, Kcal / Kg

3 - Latent heat of fusion for products is equal to;

$$Q_L = \dot{M} h$$

Where h = Latent heat of product, Kcal / Kg

4 - Heat removed from freezing temperature (T_f) to final storage temperature (T_{fs}) is;

$$Q_{bf} = \dot{M} C_{bf} (T_f - T_{fs})$$

Where: C_{bf} = Specific heat of products below freezing temperature.

For upright freezers or freezer compartment of refrigerators, total product load is

$$Q_{pl} = Q_{af} + Q_L + Q_{bf}$$

For storage products to some lower temperatures above freezing temperature in refrigerator compartment is;

$$Q_{pl} = Q_{rs}$$

Internal Load

Electrical energy dissipated in the refrigerated space such as lights, fan motors, heaters, are included in the internal heat load. Due to the

little amount of consumption of lightings, the effect of lighting can be negligible and only electrical heaters of two door refrigerators or fan motors (if exist) are considered in our load calculation.

Infiltration Load

Infiltration air load is the heat transfer due to exchanging of refrigerated air with ambient caused by opening of the door or leakage through the gasket area. Infiltration load is one of the most important load components and roughly it is about 20 % of total refrigeration load.

Total Refrigeration load

As it was mentioned before, transmission load (Q_{tl}), product load (Q_{pl}) and internal load (Q_{il}) can be calculated separately. For infiltration load (air exchange through doorways or gasket leakage), we take into account 25% of sum of the above mentioned components. (transmission load, product load and internal load). Therefore total refrigeration load can be expressed as:

$$\underline{Q_{TL} = 1.25 (Q_{TL} + Q_{PL} + Q_{IL})}$$

Making Prototypes

Several prototypes have been made so far and we decided to test two of them in our Hot Chamber.

Refrigerant charge

For making prototypes we decided to charge different amount of R134a refrigerant into the refrigeration system. We considered the same amount of refrigerant as the basis of R12 refrigeration system for prototypes number one and we reduced ten percent refrigerant weight from the basis of R12 for the second prototype.

Compressor

The compressor used are in accordance with the results of our calculation and we selected the nearest possible cooling capacity of the compressor to the cooling requirement as calculated.

Capillary tube

We decided to keep the length of capillary tube unchanged, due to our experience and information we received from the compressor manufacturers.

Evaporator

We believe that the evaporator does not need any adjustment due to the higher capacity of the evaporator than what we need.

Condenser

For the same reason that we did not adjust the evaporator we did not adjust the condenser.

Testing Prototypes

Two prototypes were tested under the following condition

Pull down test, Continuous run test and cyclic run test

Ambient temperature	32 C
Relative Humidity	73 %
Test Package	used
"M" Package	used
Number of Temp. Sensors	10

Following refrigeration system points temperature were measured and the results were satisfactory.

"M" packages, Compressor Discharge and suction, condenser outlet, ambient temperature, compressor shell, evaporator surface, energy consumption, starting current.

We enclose the completed test result sheet form for your information

With regards
Liang Rikui
Chief of technical department



"RSLG" Hot Chamber Test Sheet

Date 1998, 12.19		Test Type Cyclic Run		Test Number 4	Ambient Temp. 32°C
Model	Serial number	Overall Dim.	Internal Volume		
BP-168	Prot. 01		168 Lit		
Comp. Model	Comp. Watt	Refrigerant Type	Refrigerant Charge		
AE1350Y	138W	R134A	140 gr.		
Thermostat Type	Thermostat Model	Thermostat Setting			
Defrost	WPF30	Min.			
Test Results			Remarks		
Temp. °C	Therm. Cut in	Therm. Cut out	these temp. inside is little high. may be adjust the setting point in "Min"		
T1	-10.80	-10.70			
T2	-11.70	-11.69			
T3	-11.83	-11.61			
T4	-11.76	-11.61			
T5	-11.44	-11.21			
T6	-11.68	-11.65			
T7					
T8					
T9					
Comp. Suc.			Comments		
Comp. Disch.					
Comp. Shell					
Evap. Outlet					
Evap. inlet					
Cond. Outlet					
Bald Temp					
Comp. Running Time %	26.19%				
Energy Consump. Kw/24 Hrs	0.9214 kWh/24h				
Starting Current Amp.	1.01				
Running Current Amp.	0.85				
Lab. Specialist: Xian Yingdi			Supervisor: Liang Kikui		

"RSLG" Hot Chamber Test Sheet

Date 1998. 12. 19		Test Type <i>cyclic run</i>	Test Number 3	Ambient Temp. 32
Model	Serial number	Overall Dim.	Internal Volume	
<i>BD-168</i>	<i>Prt. 01</i>		<i>168 Lit</i>	
Comp. Model	Comp. Watt	Refrigerant Type	Refrigerant Charge	
<i>AZ1350Y</i>	<i>138W</i>	<i>R134a</i>	<i>140gr.</i>	
Thermostat Type	Thermostat Model	Thermostat Setting		
<i>Defrost</i>	<i>WPF30</i>	<i>Mid.</i>		
Test Results			Remarks	
Temp. °C	Therm. Cut in	Therm. Cut out	<p><i>Temp inside may be a little high. but the position of the thermostat can be adjust. So this result we think it's ok too.</i></p>	
T1	<i>-14.79</i>	<i>-14.91</i>		
T2	<i>-15.71</i>	<i>-15.90</i>		
T3	<i>-15.87</i>	<i>-15.70</i>		
T4	<i>-15.86</i>	<i>-15.76</i>		
T5	<i>-15.60</i>	<i>-15.34</i>		
T6	<i>-15.90</i>	<i>-15.95</i>		
T7				
T8				
T9				
Comp. Suc.			<p style="text-align: center;">Comments</p>	
Comp. Disch.				
Comp. Shell				
Evap. Outlet				
Evap. inlet				
Cond. Outlet				
Bald Temp				
Comp. Running Time %	<i>33%</i>			
Energy Consump. Kw/24 Hrs	<i>1.0481 kw/24h</i>			
Starting Current Amp.	<i>0.968</i>			
Running Current Amp.	<i>0.85</i>			
Lab. Specialist: <i>Xian Yingdi</i>			Supervisor: <i>Liang Rikui</i>	

"RSLG" Hot Chamber Test Sheet

Date <i>1995.12.18</i>		Test Type <i>Cyclic Run</i>		Test Number <i>2</i>	Ambient Temp. <i>32°C</i>			
Model	Serial number	Overall Dim.	Internal Volume					
<i>B7-100</i>	<i>Prt. 01</i>		<i>168 lit</i>					
Comp. Model	Comp. Watt	Refrigerant Type	Refrigerant Charge					
<i>AZ1350Y</i>	<i>138W</i>	<i>R134a</i>	<i>140 gr.</i>					
Thermostat Type	Thermostat Model	Thermostat Setting						
<i>Defrost</i>	<i>WPF30</i>	<i>Max.</i>						
Test Results			Remarks					
Temp. °C	Therm. Cut in	Therm. Cut out	<i>The result is ok.</i>					
T1	<i>-20.73</i>	<i>-22.44</i>						
T2	<i>-21.74</i>	<i>-23.44</i>						
T3	<i>-22.12</i>	<i>-22.74</i>						
T4	<i>-22.02</i>	<i>-22.72</i>						
T5	<i>-21.55</i>	<i>-22.58</i>						
T6	<i>-21.81</i>	<i>-23.46</i>						
T7								
T8								
T9								
Comp. Suc.	<i>15</i>	<i>31</i>	Comments					
Comp. Disch.	<i>32</i>	<i>58</i>						
Comp. Shell								
Evap. Outlet								
Evap. inlet	<i>-20</i>	<i>-27</i>						
Cond. Outlet	<i>+28</i>	<i>41</i>						
Bald Temp	<i>-19</i>	<i>-26</i>						
Comp. Running Time %	<i>57.16%</i>							
Energy Consump. Kw/24 Hrs	<i>1.5020 kwh/24h</i>							
Starting Current Amp.	<i>0.914</i>							
Running Current Amp.	<i>0.85</i>							
Lab. Specialist:						Supervisor: <i>Liang Rikui</i>		

"ASLG" Hot Chamber Test Sheet

Date 1998.12.18		Test Type PULL DOWN	Test Number 1	Ambient Temp. 32°C
Model	Serial number	Overall Dim.	Internal Volume	
BD-168	Prt. 01		168 lit	
Comp. Model	Comp. Watt	Refrigerant Type	Refrigerant Charge	
AE1350Y	138W	R134a	140 gr.	
Thermostat Type	Thermostat Model	Thermostat Setting		
Defrost	WPF30	Max.		
Test Results			Remarks	
Temp. °C	Therm. Cut in	Therm. Cut out	IN our standard, the pull down time from 32°C to -21.9 must be less than 90 minutes. BD-168 spent 68.63 min. So it's ok.	
T1	31.91	-21.92		
T2	31.41	-23.11		
T3	31.63	-22.38		
T4	31.58	-22.37		
T5	31.54	-22.10		
T6	31.43	-23.14		
T7				
T8				
T9				
Comp. Suc.	31		Comments	
Comp. Disch.	60			
Comp. Shell	55			
Evap. Outlet				
Evap. inlet				
Cond. Outlet	41			
Bald Temp	-26			
Comp. Running Time %				
Energy Consump. Kw/24 Hrs				
Starting Current Amp.	0.914			
Running Current Amp.	0.85			
Lab. Specialist:			Supervisor: Liang Bikui	

"RSLG" Hot Chamber Test Sheet

Date <i>98. 12. 23</i>		Test Type <i>pull down</i>		Test Number <i>1</i>	Ambient Temp. <i>32°C</i>
Model	Serial number	Overall Dim.	Internal Volume		
<i>BD-182</i>	<i>Prt. 02</i>	<i>990x555x920</i>	<i>182 lit.</i>		
Comp. Model	Comp. Watt	Refrigerant Type	Refrigerant Charge		
<i>AE1360Y</i>	<i>157W</i>	<i>R134a</i>	<i>150 gr.</i>		
Thermostat Type	Thermostat Model	Thermostat Setting			
<i>Pressure Type.</i>	<i>WPF30</i>	<i>Max.</i>			
Test Results			Remarks		
Temp. °C	Therm. Cut in	Therm. Cut out			
T1					
T2					
T3					
T4					
T5					
T6					
T7					
T8					
T9					
Comp. Suc.			Comments		
Comp. Disch.					
Comp. Shell					
Evap. Outlet					
Evap. inlet					
Cond. Outlet					
Brld Temp					
Comp. Running Time %					
Energy Consump. Kw/24 Hrs					
Starting Current Amp.					
Running Current Amp.					
Lab. Specialist:			Supervisor:		

"RSLG" Hot Chamber Test Sheet

Date <i>99. 1. 9</i>		Test Type <i>pull down</i>		Test Number <i>1</i>		Ambient Temp. <i>32°c</i>	
Model		Serial number		Overall Dim.		Internal Volume	
<i>BCD-205</i>		<i>Prt-10</i>		<i>1065x555x920</i>		<i>205 Lit.</i>	
Comp. Model		Comp. Watt		Refrigerant Type		Refrigerant Charge	
<i>AE1350Y</i>		<i>138W</i>		<i>R134a</i>			
Thermostat Type		Thermostat Model		Thermostat Setting			
<i>Pressure Type.</i>		<i>WPF30</i>		<i>Max.</i>			
Test Results				Remarks			
Temp. °C		Therm. Cut in	Therm. Cut out				
T1							
T2							
T3							
T4							
T5							
T6							
T7							
T8							
T9							
Comp. Suc.							
Comp. Disch.							
Comp. Shell							
Evap. Outlet				Comments			
Evap. inlet							
Cond. Outlet							
Bald Temp							
Comp. Running Time %							
Energy Consump. Kw/24 Hrs							
Starting Current Amp.							
Running Current Amp.							
Lab. Specialist:				Supervisor:			

"RSLG" Hot Chamber Test Sheet

Date <i>99.1.7.</i>		Test Type <i>pull down.</i>		Test Number <i>1</i>	Ambient Temp. <i>32°C</i>
Model	Serial number	Overall Dim.	Internal Volume		
<i>BCD-188.</i>	<i>Prt. 09</i>	<i>990x555x920</i>	<i>188 Lit.</i>		
Comp. Model	Comp. Watt	Refrigerant Type	Refrigerant Charge		
<i>AE1350Y</i>	<i>138W</i>	<i>R134a</i>			
Thermostat Type	Thermostat Model	Thermostat Setting			
<i>Pressure Type.</i>	<i>WPF30</i>	<i>Max.</i>			
Test Results			Remarks		
Temp. °C	Therm. Cut in	Therm. Cut out			
T1					
T2					
T3					
T4					
T5					
T6					
T7					
T8					
T9					
Comp. Suc.			Comments		
Comp. Disch.					
Comp. Shell					
Evap. Outlet					
Evap. inlet					
Cond. Outlet					
Bald Temp					
Comp. Running Time %					
Energy Consump. Kw/24 Hrs					
Starting Current Amp.					
Running Current Amp.					
Lab. Specialist:			Supervisor:		

"RSLG" Hot Chamber Test Sheet

Date <i>99. 1. 7</i>		Test Type <i>pull down.</i>		Test Number <i>1</i>		Ambient Temp. <i>32°C</i>	
Model		Serial number		Overall Dim.		Internal Volume	
<i>BCD-168</i>		<i>Prt. 08</i>		<i>900x555x920</i>		<i>168 Lit</i>	
Comp. Model		Comp. Watt		Refrigerant Type		Refrigerant Charge	
<i>AE1340Y</i>		<i>108W</i>		<i>R134a.</i>		<i>115 gr.</i>	
Thermostat Type		Thermostat Model		Thermostat Setting			
<i>Pressure. Type.</i>		<i>WPF30</i>		<i>Max.</i>			
Test Results				Remarks			
Temp. °C		Therm. Cut in	Therm. Cut out				
T1							
T2							
T3							
T4							
T5							
T6							
T7							
T8							
T9							
Comp. Suc.				Comments			
Comp. Disch.							
Comp. Shell							
Evap. Outlet							
Evap. inlet							
Cond. Outlet							
Bald Temp							
Comp. Running Time %							
Energy Consump. Kw/24 Hrs							
Starting Current Amp.							
Running Current Amp.							
Lab. Specialist:				Supervisor:			

"RSLG" Hot Chamber Test Sheet

Date <i>99. 7. 5</i>		Test Type <i>Pull down.</i>		Test Number <i>1</i>		Ambient Temp. <i>32°C</i>	
Model		Serial number		Overall Dim.		Internal Volume	
<i>BD-400</i>		<i>Prt. 07.</i>		<i>385x700x920</i>		<i>400 Lit.</i>	
Comp. Model		Comp. Watt		Refrigerant Type		Refrigerant Charge	
<i>AE1390Y</i>		<i>224 W</i>		<i>R134a.</i>		<i>285 gr.</i>	
Thermostat Type		Thermostat Model		Thermostat Setting			
<i>Pressure Type.</i>		<i>WPF30.</i>		<i>Max.</i>			
Test Results				Remarks			
Temp. °C		Therm. Cut in	Therm. Cut out				
T1							
T2							
T3							
T4							
T5							
T6							
T7							
T8							
T9							
Comp. Suc.							
Comp. Disch.							
Comp. Shell							
Evap. Outlet				Comments			
Evap. inlet							
Cond. Outlet							
Bald Temp							
Comp. Running Time %							
Energy Consump. Kw/24 Hrs							
Starting Current Amp.							
Running Current Amp.							
Lab. Specialist:				Supervisor:			

"RSLG" Hot Chamber Test Sheet

Date <i>99. 7. 3.</i>		Test Type <i>pull down</i>		Test Number <i>1</i>	Ambient Temp. <i>32°C</i>
Model	Serial number	Overall Dim.	Internal Volume		
<i>BD-30B</i>	<i>Prt. 06</i>	<i>1125x700x920</i>	<i>30B Lit.</i>		
Comp. Model	Comp. Watt	Refrigerant Type	Refrigerant Charge		
<i>AE1390Y</i>	<i>224 W</i>	<i>R134a.</i>	<i>190 gr.</i>		
Thermostat Type	Thermostat Model	Thermostat Setting			
<i>Pressure Type.</i>	<i>WPF30.</i>	<i>Max.</i>			
Test Results			Remarks		
Temp. °C	Therm. Cut in	Therm. Cut out			
T1					
T2					
T3					
T4					
T5					
T6					
T7					
T8					
T9					
Comp. Suc.			Comments		
Comp. Disch.					
Comp. Shell					
Evap. Outlet					
Evap. inlet					
Cond. Outlet					
Bald Temp					
Comp. Running Time %					
Energy Consump. Kw/24 Hrs					
Starting Current Amp.					
Running Current Amp.					
Lab. Specialist:			Supervisor:		

"RSLG" Hot Chamber Test Sheet

Date <i>98. 12. 25</i>		Test Type <i>pull down</i>		Test Number <i>1</i>	Ambient Temp. <i>32°C</i>
Model	Serial number	Overall Dim.		Internal Volume	
<i>BD-2/0</i>	<i>Prt. 05</i>	<i>1065x555x920</i>		<i>2/0 Lit</i>	
Comp. Model	Comp. Watt	Refrigerant Type		Refrigerant Charge	
<i>AE1370Y</i>	<i>172 W</i>	<i>R134a</i>		<i>160 gr.</i>	
Thermostat Type	Thermostat Model	Thermostat Setting			
<i>Pressure Type.</i>	<i>WPF30.</i>	<i>Max.</i>			
Test Results				Remarks	
Temp. °C	Therm. Cut in	Therm. Cut out			
T1					
T2					
T3					
T4					
T5					
T6					
T7					
T8					
T9					
Comp. Suc.				Comments	
Comp. Disch.					
Comp. Shell					
Evap. Outlet					
Evap. inlet					
Cond. Outlet					
Bald Temp					
Comp. Running Time %					
Energy Consump. Kw/24 Hrs					
Starting Current Amp.					
Running Current Amp.					
Lab. Specialist:				Supervisor:	

"RSLG" Hot Chamber Test Sheet

Date <i>9 B. 12. 25</i>		Test Type <i>pull down</i>		Test Number <i>1</i>	Ambient Temp. <i>32°C</i>		
Model	Serial number	Overall Dim.		Internal Volume			
<i>BD-195</i>	<i>Prt. 04</i>	<i>990x555x920</i>		<i>195 Lit.</i>			
Comp. Model	Comp. Watt	Refrigerant Type		Refrigerant Charge			
<i>AE1360Y</i>	<i>157W</i>	<i>R134a</i>		<i>150 gr.</i>			
Thermostat Type	Thermostat Model	Thermostat Setting					
<i>Pressure Type</i>	<i>WPF30</i>	<i>MAX.</i>					
Test Results				Remarks			
Temp. °C	Therm. Cut in	Therm. Cut out					
T1							
T2							
T3							
T4							
T5							
T6							
T7							
T8							
T9							
Comp. Suc.							
Comp. Disch.							
Comp. Shell							
Evap. Outlet						Comments	
Evap. inlet							
Cond. Outlet							
Bald Temp							
Comp. Running Time %							
Energy Consump. Kw/24 Hrs							
Starting Current Amp.							
Running Current Amp.							
Lab. Specialist:				Supervisor:			

"RSLG" Hot Chamber Test Sheet

Date <i>98. 12. 23</i>		Test Type <i>pull down</i>		Test Number <i>1</i>		Ambient Temp. <i>32°C</i>	
Model		Serial number		Overall Dim.		Internal Volume	
<i>BD-198</i>		<i>Prt. 03</i>		<i>1065 x 555 x 920</i>		<i>198 Lit.</i>	
Comp. Model		Comp. Watt		Refrigerant Type		Refrigerant Charge	
<i>AE1360Y</i>		<i>157W</i>		<i>R134a</i>		<i>160 gr.</i>	
Thermostat Type		Thermostat Model		Thermostat Setting			
<i>Pressure type</i>		<i>WPF30</i>		<i>MAX.</i>			
Test Results				Remarks			
Temp. °C		Therm. Cut in	Therm. Cut out				
T1							
T2							
T3							
T4							
T5							
T6							
T7							
T8							
T9							
Comp. Suc.				Comments			
Comp. Disch.							
Comp. Shell							
Evap. Outlet							
Evap. inlet							
Cond. Outlet							
Bald Temp							
Comp. Running Time %							
Energy Consump. Kw/24 Hrs							
Starting Current Amp.							
Running Current Amp.							
Lab. Specialist:				Supervisor:			

Transmission load calculation
Chest Freezer Model BD168
Dimensions

	Dimension Mt.	Area (sq. Mt.)	Insulation Thickness mm.
Side Walls	2x0.58x0.55	0.638	60
Back Panel	0.895x0.58	0.519	60
Door	0.895x0.55	0.49	40
Bottom Floor	0.895x0.55	0.49	65
Front Panel	0.895x0.58	0.519	60

Insulation Type: Pu Foam

CP5. Foam Thermal Conductivity: 0.0195 W /mt.C

Temperature Difference: $(\Delta T) = 32 - (-18) = 50 \text{ C}$

Ambient Temperature = 32 C

Freezer Air Temperature = - 18 C

Calculation :

$$Q_{TL} = Q_{SW} + Q_{BP} + Q_{BOTTOM} + Q_{Front} + Q_{DOOR}$$

$$Q = U A (T_a - T_f)$$

$$U = \frac{1}{X_1 / K_1 + X_2 / K_2 + \dots}$$

Where :

U = Heat Resistance Coefficient Factor

K₁ = Foam Thermal Conductivity

X₁ = Foam Thickness

Note : Due to the short thickness of cabinet out side panel (0.5 mm) and aluminum inner liner (0.5 mm) heat resistance of these materials have been considered negligible.

Therefore:

$$1- \quad Q_{\text{Side Walls}} = [U A (T_a - T_f)]$$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.060 / 0.0195) = 0.32 \text{ W/ Sq. Mt. C}$$

$$A = 0.638 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Side Walls}} = 0.32 \times 0.638 \times 50 = 10.2 \text{ Watts}$$

$$Q_{\text{Side Walls}} = 10.2 \text{ Watts}$$

$$2 - \quad Q_{\text{Back panel}} = [U A (T_a - T_f)]$$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.060 / 0.0195) = 0.32 \text{ W/ Sq. Mt. C}$$

$$A = 0.519 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Back panel}} = 0.32 \times 0.519 \times 50 = 8.3 \text{ Watts}$$

$$Q_{\text{Back panel}} = 8.3 \text{ Watts}$$

$$Q_{\text{Front Panel}} = [U A (T_a - T_f)]$$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.060 / 0.0195) = 0.32 \text{ W/ Sq. Mt C}$$

$$A = 0.519 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Front Panel}} = 0.32 \times 0.519 \times 50 = \text{Watts}$$

$$Q_{\text{Top}} = 8.3 \text{ Watts}$$

$$4 - \quad Q_{\text{Bottom}} = [U A (T_a - T_f)]$$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.065 / 0.0195) = 0.30 \text{ W/Sq. Mt. C}$$

$$A = 0.49 \text{ Sq. Mt.}$$

$$T_a = 42\text{C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Bottom}} = 0.3 \times 0.49 \times 60 = 8.9 \text{ Watts}$$

$$Q_{\text{Bottom}} = 8.9 \text{ Watts}$$

$$5 - \quad Q_{\text{Door}} = [U A (T_a - T_f)]$$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.040 / 0.0195) = 0.49 \text{ W/ Sq. Mt. C}$$

$$A = 0.49 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Door}} = 0.49 \times 0.49 \times 50 = 12 \text{ Watts}$$

$$Q_{\text{Door}} = 12 \text{ Watts}$$

Total Heat Leaks;

$$Q_{\text{TL}} = 10.2 + 8.3 + 8.3 + 8.9 + 12 = 47.7$$

$$Q_{\text{Total Heat Leaks}} = 47.7 \text{ Watts}$$

b) Product Loads;

$$Q_{\text{product}} = 65 \% Q_{\text{Heat Leaks}}$$

$$Q_{\text{Product Loads}} = 47.7 \times 70\% = 33.4$$

$$Q_{\text{Misc}} = 30 \% (Q_{\text{Heat Leaks}} + Q_{\text{Product Loads}})$$

$$Q_{\text{Misc}} = 30 \% = 24.3$$

$$Q_{\text{Misc}} = Q_{\text{Electricity}} + Q_{\text{Infiltration}} + Q_{\text{Door Opening}} + Q_{\text{Etc.}}$$

Total Cooling Capacity required is calculated as follows;

$$Q_{\text{Grand Total}} = Q_{\text{Heat Leaks}} + Q_{\text{Product Loads}} + Q_{\text{Misc.}}$$

$$Q_{\text{Grand Total}} = 47.7 + 33.4 + 24.3 = 105.4 \text{ Watts}$$

$$Q_{\text{Grand Total}} = 105.4 \text{ Watts}$$

Type of Compressor suitable for this model is recommended Aspera Model BP 1111Z, or Compressor HUAYI Model AE1340Y, or Zanussi Model OF789CY.

Transmission load calculation
Chest Freezer Model BD182AF
Dimensions

	Dimension Mt.	Area (sq. Mt.)	Insulation Thickness mm.
Side Walls	2x0.58x0.55	0.638	60
Back Panel	0.985x0.58	0.57	60
Door	0.985x0.55	0.54	40
Bottom Floor	0.985x0.55	0.54	65
Front Panel	0.985x0.58	0.57	60

Insulation Type: Pu Foam

$$\text{CP5. Foam Thermal Conductivity: } 0.0195 \text{ W /mt.C}$$

$$\text{Temperature Difference: } (\Delta T) = 32 - (-18) = 50 \text{ C}$$

$$\text{Ambient Temperature} = 32 \text{ C}$$

$$\text{Freezer Air Temperature} = -18 \text{ C}$$

Calculation :

$$Q_{TL} = Q_{SW} + Q_{BP} + Q_{BOTTOM} + Q_{Front} + Q_{DOOR}$$

$$Q = U A (T_a - T_f)$$

$$U = \frac{1}{X_1 / K_1 + X_2 / K_2 + \dots}$$

Where :

U = Heat Resistance Coefficient Factor

K₁ = Foam Thermal Conductivity

X₁ = Foam Thickness

Note : Due to the short thickness of cabinet out side panel (0.5 mm) and aluminum inner liner (0.5 mm) heat resistance of these materials have been considered negligible.

Therefore:

1- $Q_{Side\ Walls} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.060 / 0.0195) = 0.32 \text{ W/ Sq. Mt. C}$$

$$A = 0.638 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{Side\ Walls} = 0.32 \times 0.638 \times 50 = 10.2 \text{ Watts}$$

$$Q_{Side\ Walls} = 10.2 \text{ Watts}$$

2 - $Q_{Back\ panel} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.060 / 0.0195) = 0.32 \text{ W/ Sq. Mt. C}$$

$$A = 0.57 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Back panel}} = 0.32 \times 0.57 \times 50 = 9.1 \text{ Watts}$$

$$Q_{\text{Back panel}} = 9.1 \text{ Watts}$$

3 - $Q_{\text{Front Panel}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.060 / 0.0195) = 0.32 \text{ W/ Sq. Mt C}$$

$$A = 0.57 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Front Panel}} = 0.32 \times 0.57 \times 50 = 9.1 \text{ Watts}$$

$$Q_{\text{Top}} = 9.1 \text{ Watts}$$

4 - $Q_{\text{Bottom}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.065 / 0.0195) = 0.30 \text{ W/Sq. Mt C}$$

$$A = 0.54 \text{ Sq. Mt.}$$

$$T_a = 42 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Bottom}} = 0.3 \times 0.54 \times 60 = 9.7 \text{ Watts}$$

$$Q_{\text{Bottom}} = 9.7 \text{ Watts}$$

5 - $Q_{\text{Door}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.040 / 0.0195) = 0.49 \text{ W/ Sq. Mt. } ^\circ\text{C}$$

$$A = 0.54 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ } ^\circ\text{C}$$

$$T_f = -18 \text{ } ^\circ\text{C}$$

$$Q_{\text{Door}} = 0.49 \times 0.54 \times 50 = 13.2 \text{ Watts}$$

$$Q_{\text{Door}} = 13.2 \text{ Watts}$$

Total Heat Leaks;

$$Q_{\text{TL}} = 10.2 + 9.1 + 9.7 + 9.1 + 13.2 = 51.33$$

$$Q_{\text{Total Heat Leaks}} = 51.33 \text{ Watts}$$

b) Product Loads;

We consider 13 Kg ice making capacity for this model per 24 hours.

Therefore;

$$Q_{\text{product}} = Q_1 + Q_2 + Q_3,$$

where;

$Q_1 = mC_1 (T_1 - T_f)$ = energy required to freeze water from initial temperature to freezing point of $0 \text{ } ^\circ\text{C}$

$Q_2 = mC_2 (T_f - T_a)$ = energy required to freeze ice from zero degree temperature to $-18 \text{ } ^\circ\text{C}$

$Q_3 = m \times h$ = heat gain from latent heat of fusion of water

$$Q_1 = 13 \times 1 \times (24 - 0) = 312 \text{ Kcal per 24 hour}$$

$$Q_2 = 13 \times 1 [0 - (-18)] = 234 \text{ Kcal per 24 hours}$$

$$Q_3 = 13 \times 108 = 1404 \text{ Kcal per 24 hours}$$

$$Q_{\text{product}} = 312 + 234 + 1404 = 1950 \text{ Kcal per 24 hour} = 81 \text{ Kcal / hour} = 94 \text{ W}$$

$$Q_{\text{Misc}} = 10 \% (Q_{\text{Heat Leaks}} + Q_{\text{Product Loads}})$$

$$Q_{\text{Misc}} = 10 \% (51 + 94) = 14.5$$

$$Q_{\text{Misc}} = Q_{\text{Electricity}} + Q_{\text{Infiltration}} + Q_{\text{Door Opening}} + Q_{\text{Etc.}}$$

Total Cooling Capacity required is calculated as follows;

$$Q_{\text{Grand Total}} = Q_{\text{Heat Leaks}} + Q_{\text{Product Loads}} + Q_{\text{Misc.}}$$

$$Q_{\text{Grand Total}} = 51.1 + 94 + 14.5 = 159.6 \text{ Watts}$$

$$Q_{\text{Grand Total}} = 160 \text{ Watts}$$

Type of Compressor suitable for this model is recommended

Transmission load calculation
Chest Freezer Model BD198AE

Dimensions

	Dimension Mt.	Area (sq. Mt.)	Insulation Thickness mm.
Side Walls	2x0.58x0.55	0.638	60
Back Panel	1.06x0.58	0.61	60
Door	1.06x0.55	0.58	40
Bottom Floor	1.06x0.55	0.58	65
Front Panel	1.06x0.58	0.61	60

Insulation Type: Pu Foam

CP5. Foam Thermal Conductivity: 0.0195 W /mt.C

Temperature Difference: $(\Delta T) = 32 - (-18) = 50 \text{ C}$

Ambient Temperature = 32 C

Freezer Air Temperature = - 18 C

Calculation :

$$Q_{TL} = Q_{SW} + Q_{BP} + Q_{BOTTOM} + Q_{Front} + Q_{DOOR}$$

$$Q = U A (T_a - T_f)$$

$$U = \frac{1}{X_1 / K_1 + X_2 / K_2 + \dots}$$

Where :

U = Heat Resistance Coefficient Factor

K₁ = Foam Thermal Conductivity

X₁ = Foam Thickness

Note : Due to the short thickness of cabinet out side panel (0.5 mm) and aluminum inner liner (0.5 mm) heat resistance of these materials have been considered negligible.

Therefore:

1- $Q_{\text{Side Walls}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.060 / 0.0195) = 0.32 \text{ W/ Sq. Mt. C}$$

$$A = 0.638 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Side Walls}} = 0.32 \times 0.638 \times 50 = 10.2 \text{ Watts}$$

$$Q_{\text{Side Walls}} = 10.2 \text{ Watts}$$

2 - $Q_{\text{Back panel}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.060 / 0.0195) = 0.32 \text{ W/ Sq. Mt. C}$$

$$A = 0.61 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Back panel}} = 0.32 \times 0.61 \times 50 = 9.8 \text{ Watts}$$

$$Q_{\text{Back panel}} = 9.8 \text{ Watts}$$

3 - $Q_{\text{Front Panel}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.060 / 0.0195) = 0.32 \text{ W/ Sq. Mt C}$$

$$A = 0.61 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = -18 \text{ C}$$

$$Q_{\text{Front Panel}} = 0.32 \times 0.61 \times 50 = 9.8 \text{ Watts}$$

$$Q_{\text{Top}} = 9.8 \text{ Watts}$$

4 - $Q_{\text{Bottom}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.065 / 0.0195) = 0.30 \text{ W/Sq. Mt. C}$$

$$A = 0.58 \text{ Sq. Mt.}$$

$$T_a = 42 \text{ C}$$

$$T_f = -18 \text{ C}$$

$$Q_{\text{Bottom}} = 0.3 \times 0.58 \times 60 = 10.4 \text{ Watts}$$

$$Q_{\text{Bottom}} = 10.4 \text{ Watts}$$

5 - $Q_{\text{Door}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.040 / 0.0195) = 0.49 \text{ W/ Sq. Mt. C}$$

$$A = 0.58 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = -18 \text{ C}$$

$$Q_{\text{Door}} = 0.49 \times 0.58 \times 50 = 14.2 \text{ Watts}$$

$$Q_{\text{Door}} = 14.2 \text{ Watts}$$

Total Heat Leaks;

$$Q_{\text{TL}} = 10.2 + 9.8 + 10.4 + 9.8 + 14.2 = 54.4$$

$$Q_{\text{Total Heat Leaks}} = 54.4 \text{ Watts}$$

b) Product Loads;

We consider 15 Kg ice making capacity for this model per 24 hours.
Therefore;

$$Q_{\text{product}} = Q_1 + Q_2 + Q_3,$$

where;

$Q_1 = mC_1 (T_i - T_f) =$ energy required to freeze water from initial temperature to freezing point of 0°C

$Q_2 = mC_2 (T_f - T_r) =$ energy required to freeze ice from zero degree temperature to -18°C

$Q_3 = m \times h =$ heat gain from latent heat of fusion of water

$$Q_1 = 15 \times 1 \times (24-0) = 360 \text{ Kcal per 24 hour}$$

$$Q_2 = 15 \times 1 [0 - (-18)] = 270 \text{ Kcal per 24 hours}$$

$$Q_3 = 15 \times 108 = 1620 \text{ Kcal per 24 hours}$$

$$Q_{\text{product}} = 360 + 270 + 1620 = 2250 \text{ Kcal per 24 hour} = 93 \text{ Kcal / hour} = 108.7 \text{ W}$$

$$Q_{\text{Misc}} = 10 \% (Q_{\text{Heat Leaks}} + Q_{\text{Product Loads}})$$

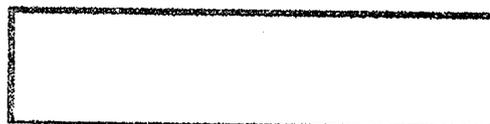
$$Q_{\text{Misc}} = 10 \% (54.4 + 108.7) = 16.3$$

$$Q_{\text{Misc}} = Q_{\text{Electricity}} + Q_{\text{Infiltration}} + Q_{\text{Door Opening}} + Q_{\text{Etc.}}$$

Total Cooling Capacity required is calculated as follows;

$$Q_{\text{Grand Total}} = Q_{\text{Heat Leaks}} + Q_{\text{Product Loads}} + Q_{\text{Misc.}}$$

$$Q_{\text{Grand Total}} = 54.4 + 108.7 + 16.3 = 179.4 \text{ Watts}$$



$$Q_{\text{Grand Total}} = 179 \text{ Watts}$$

Type of Compressor suitable for this model is recommended

Transmission load calculation

Chest Freezer Model BD308

Dimensions

	Dimension Mt.	Area (sq. Mt.)	Insulation Thickness mm.
Side Walls	$(0.8 \times 0.63) + (0.45 \times 0.63)$	0.79	70
Back Panel	$(0.8 \times 1.12) - (0.25 \times 0.24)$	0.89	70
Door	1.12 x 0.63	0.70	65
Bottom Floor	1.12 x 0.63	0.70	75
Front Panel	$(0.8 \times 1.12) - (0.25 \times 0.24)$	0.89	70

Insulation Type: Pu Foam

CP5. Foam Thermal Conductivity: 0.0195 W /mt.C

Temperature Difference: $(\Delta T) = 32 - (-18) = 50 \text{ C}$

Ambient Temperature = 32 C

Freezer Air Temperature = - 18 C

Calculation :

$$Q_{TL} = Q_{SW} + Q_{BP} + Q_{BOTTOM} + Q_{Front} + Q_{DOOR}$$

$$Q = U A (T_a - T_f)$$

$$U = \frac{1}{X_1 / K_1 + X_2 / K_2 + \dots}$$

Where :

U = Heat Resistance Coefficient Factor

K₁ = Foam Thermal Conductivity

X₁ = Foam Thickness

Note : Due to the short thickness of cabinet out side panel (0.5 mm) and aluminum inner liner (0.5 mm) heat resistance of these materials have been considered negligible.

Therefore:

1- $Q_{\text{Side Walls}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.070 / 0.0195) = 0.28 \text{ W/ Sq. Mt. C}$$

$$A = 0.79 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Side Walls}} = 0.28 \times 0.79 \times 50 = 11 \text{ Watts}$$

$$Q_{\text{Side Walls}} = 11 \text{ Watts}$$

2 - $Q_{\text{Back panel}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature
 T_f = Freezer air Temperature

$$U = 1 / (0.070 / 0.0195) = 0.28 \text{ W/ Sq. Mt. C}$$

$$A = 0.89 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Back panel}} = 0.28 \times 0.89 \times 50 = 12.5 \text{ Watts}$$

$$Q_{\text{Back panel}} = 12.5 \text{ Watts}$$

3 - $Q_{\text{Front Panel}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature
 T_f = Freezer air Temperature

$$U = 1 / (0.070 / 0.0195) = 0.28 \text{ W/ Sq. Mt C}$$

$$A = 0.89 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Front Panel}} = 0.28 \times 0.89 \times 50 = 12.5 \text{ Watts}$$

$$Q_{\text{Top}} = 12.5 \text{ Watts}$$

4 - $Q_{\text{Bottom}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature
 T_f = Freezer air Temperature

$$U = 1 / (0.075 / 0.0195) = 0.26 \text{ W/Sq. Mt C}$$

$$A = 0.70 \text{ Sq. Mt.}$$

$$T_a = 42 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Bottom}} = 0.26 \times 0.70 \times 60 = 11 \text{ Watts}$$

$$Q_{\text{Bottom}} = 11 \text{ Watts}$$

$$5 - \quad Q_{\text{Door}} = [U A (T_a - T_f)]$$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.065 / 0.0195) = 0.3 \text{ W/ Sq. Mt. C}$$

$$A = 0.70 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = -18 \text{ C}$$

$$Q_{\text{Door}} = 0.3 \times 0.70 \times 50 = 10.5 \text{ Watts}$$

$$Q_{\text{Door}} = 10.5 \text{ Watts}$$

Total Heat Leaks;

$$Q_{\text{TL}} = 11 + 12.5 + 10.5 + 11 + 12.5 = 57.7$$

$$Q_{\text{Total Heat Leaks}} = 57.5 \text{ Watts}$$

b) Product Loads;

We consider 20 Kg ice making capacity for this model per 24 hours.

Therefore;

$$Q_{\text{product}} = Q_1 + Q_2 + Q_3,$$

where;

$Q_1 = mC_1 (T_1 - T_f)$ = energy required to freeze water from initial temperature to freezing point of 0 °C

$Q_2 = mC_2 (T_f - T_{ff})$ = energy required to freeze ice from zero degree temperature to -18 °C

$Q_3 = m \times h$ = heat gain from latent heat of fusion of water

$$Q_1 = 20 \times 1 \times (24-0) = 480 \text{ Kcal per 24 hour}$$

$$Q_2 = 20 \times 1 [0 - (-18)] = 360 \text{ Kcal per 24 hours}$$

$$Q_3 = 20 \times 108 = 2160 \text{ Kcal per 24 hours}$$

$$Q_{\text{product}} = 480 + 360 + 2160 = 3000 \text{ Kcal per 24 hour} = 125 \text{ Kcal / hour} = 145 \text{ W}$$

$$Q_{\text{Misc}} = 30 \% (Q_{\text{Heat Leaks}} + Q_{\text{Product Loads}}) = 10\%(57.5 + 145) = 20 \text{ w}$$

$$Q_{\text{Misc}} = 20 \text{ Watts}$$

$$Q_{\text{Misc}} = Q_{\text{Electricity}} + Q_{\text{Infiltration}} + Q_{\text{Door Opening}} + Q_{\text{Etc.}}$$

Total Cooling Capacity required is calculated as follows;

$$Q_{\text{Grand Total}} = Q_{\text{Heat Leaks}} + Q_{\text{Product Loads}} + Q_{\text{Misc.}}$$

$$Q_{\text{Grand Total}} = 57.5 + 145 + 20 = 220 \text{ Watts}$$

$$Q_{\text{Grand Total}} = 220 \text{ Watts}$$

Type of Compressor suitable for this model is recommended Compressor HUAYI Model

Transmission load calculation

Chest Freezer Model BD400

Dimensions

	Dimension Mt.	Area (sq. Mt.)	Insulation Thickness mm.
Side Walls	$(0.8 \times 0.63) + (0.45 \times 0.63)$	0.79	70
Back Panel	$(0.8 \times 1.38) - (0.25 \times 0.24)$	1.05	70
Door	1.38×0.63	0.87	65
Bottom Floor	1.38×0.63	0.87	75
Front Panel	$(0.8 \times 1.38) - (0.25 \times 0.24)$	1.05	70

Insulation Type: Pu Foam

CP5. Foam Thermal Conductivity: 0.0195 W /mt.C

Temperature Difference: $(\Delta T) = 32 - (-18) = 50$ C

Ambient Temperature = 32 C

Freezer Air Temperature = - 18 C

Calculation :

$$Q_{TL} = Q_{SW} + Q_{BP} + Q_{BOTTOM} + Q_{Front} + Q_{DOOR}$$

$$Q = U A (T_a - T_f)$$

$$U = \frac{1}{X_1 / K_1 + X_2 / K_2 + \dots}$$

Where :

U = Heat Resistance Coefficient Factor

K_1 = Foam Thermal Conductivity

X_1 = Foam Thickness

Note : Due to the short thickness of cabinet out side panel (0.5 mm) and aluminum inner liner (0.5 mm) heat resistance of these materials have been considered negligible.

Therefore:

1- $Q_{\text{Side Walls}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.070 / 0.0195) = 0.28 \text{ W/ Sq. Mt. C}$$

$$A = 0.79 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Side Walls}} = 0.28 \times 0.79 \times 50 = 11 \text{ Watts}$$

$$Q_{\text{Side Walls}} = 11 \text{ Watts}$$

2 - $Q_{\text{Back panel}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.070 / 0.0195) = 0.28 \text{ W/ Sq. Mt. C}$$

$$A = 1.05 \text{ Sq. Mt.}$$

$$T_a = 42 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Back panel}} = 0.28 \times 1.05 \times 60 = 17.64 \text{ Watts}$$

$$Q_{\text{Back panel}} = 17.6 \text{ Watts}$$

3 - $Q_{\text{Front Panel}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.070 / 0.0195) = 0.28 \text{ W/ Sq. Mt C}$$

$$A = 1.05 \text{ Sq. Mt.}$$

$$T_a = 42 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Front Panel}} = 0.28 \times 1.05 \times 60 = 17.6 \text{ Watts}$$

$$Q_{\text{Top}} = 17.6 \text{ Watts}$$

4 - $Q_{\text{Bottom}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.075 / 0.0195) = 0.26 \text{ W/Sq. Mt C}$$

$$A = 0.87 \text{ Sq. Mt.}$$

$$T_a = 42 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Bottom}} = 0.26 \times 0.87 \times 60 = 11.3 \text{ Watts}$$

$$Q_{\text{Bottom}} = 11.3 \text{ Watts}$$

5 - $Q_{\text{Door}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.065 / 0.0195) = 0.3 \text{ W/ Sq. Mt. C}$$

$$A = 0.870 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Door}} = 0.3 \times 0.870 \times 50 = 13 \text{ Watts}$$

$$Q_{\text{Door}} = 13 \text{ Watts}$$

Total Heat Leaks;

$$Q_{\text{TL}} = 11 + 17.6 + 13 + 17.6 + 11.3 = 70.5$$

$$Q_{\text{Total Heat Leaks}} = 70.5 \text{ Watts}$$

b) Product Loads;

We consider 25 Kg ice making capacity for this model per 24 hours.
Therefore;

$$Q_{\text{product}} = Q_1 + Q_2 + Q_3,$$

where;

$Q_1 = mC_1 (T_1 - T_f) =$ energy required to freeze water from initial temperature to freezing point of 0°C

$Q_2 = mC_2 (T_f - T_n) =$ energy required to freeze ice from zero degree temperature to -18°C

$Q_3 = m \times h =$ heat gain from latent heat of fusion of water

$$Q_1 = 25 \times 1 \times (24-0) = 600 \text{ Kcal per 24 hour}$$

$$Q_2 = 25 \times 1 [0 - (-18)] = 450 \text{ Kcal per 24 hours}$$

$$Q_3 = 25 \times 108 = 2700 \text{ Kcal per 24 hours}$$

$$Q_{\text{product}} = 600 + 450 + 2700 = 3750 \text{ Kcal per 24 hour} = 156 \text{ Kcal / hour} = 182 \text{ W}$$

$$Q_{\text{Misc}} = 30 \% (Q_{\text{Heat Leaks}} + Q_{\text{Product Loads}}) = 10\%(70.5 + 182) = 25 \text{ w}$$

$$Q_{\text{Misc}} = 25 \text{ Watts}$$

$$Q_{\text{Misc}} = Q_{\text{Electricity}} + Q_{\text{Infiltration}} + Q_{\text{Door Opening}} + Q_{\text{Etc.}}$$

Total Cooling Capacity required is calculated as follows;

$$Q_{\text{Grand Total}} = Q_{\text{Heat Leaks}} + Q_{\text{Product Loads}} + Q_{\text{Misc.}}$$

$$Q_{\text{Grand Total}} = 70.5 + 182 + 25 = 277 \text{ Watts}$$

$$Q_{\text{Grand Total}} = 277 \text{ Watts}$$

Type of Compressor suitable for this model is recommended Compressor HUAYI Model

Transmission load calculation

Chest Freezer Model BD510

Dimensions

	Dimension Mt.	Area (sq. Mt.)	Insulation Thickness mm.
Side Walls	(0.8x0.63)+(0.45x0.63)	0.79	70
Back Panel	(0.8x1.7)-(0.25x0.24)	1.3	70
Door	1.7x0.63	1.07	65
Bottom Floor	1.7x0.63	1.07	75

Front Panel	(0.8x1.12)-(0.25x0.24)	1.3	70
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Insulation Type: Pu Foam

CP5. Foam Thermal Conductivity: 0.0195 W /mt.C

Temperature Difference: $(\Delta T) = 32 - (-18) = 50 \text{ C}$

Ambient Temperature = 32 C

Freezer Air Temperature = - 18 C

Calculation :

$$Q_{TL} = Q_{SW} + Q_{BP} + Q_{BOTTOM} + Q_{Front} + Q_{DOOR}$$

$$Q = U A (T_a - T_f)$$

$$U = \frac{1}{X_1 / K_1 + X_2 / K_2 + \dots}$$

Where :

U = Heat Resistance Coefficient Factor

K₁ = Foam Thermal Conductivity

X₁ = Foam Thickness

Note : Due to the short thickness of cabinet out side panel (0.5 mm) and aluminum inner liner (0.5 mm) heat resistance of these materials have been considered negligible.

Therefore:

1- $Q_{\text{Side Walls}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.070 / 0.0195) = 0.28 \text{ W/ Sq. Mt. C}$$

$$A = 0.79 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = -18 \text{ C}$$

$$Q_{\text{Side Walls}} = 0.28 \times 0.79 \times 50 = 11 \text{ Watts}$$

$$Q_{\text{Side Walls}} = 11 \text{ Watts}$$

2 - $Q_{\text{Back panel}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.070 / 0.0195) = 0.28 \text{ W/ Sq. Mt. C}$$

$$A = 1.3 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = -18 \text{ C}$$

$$Q_{\text{Back panel}} = 0.28 \times 1.3 \times 50 = 18.2 \text{ Watts}$$

$$Q_{\text{Back panel}} = 18.2 \text{ Watts}$$

3 - $Q_{\text{Front Panel}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.070 / 0.0195) = 0.28 \text{ W/ Sq. Mt C}$$

$$A = 1.3 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = -18 \text{ C}$$

$$Q_{\text{Front Panel}} = 0.28 \times 1.3 \times 50 = 18.2 \text{ Watts}$$

$$Q_{\text{Top}} = 18.2 \text{ Watts}$$

4 - $Q_{\text{Bottom}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature

T_f = Freezer air Temperature

$$U = 1 / (0.075 / 0.0195) = 0.26 \text{ W/Sq. Mt. C}$$

$$A = 1.07 \text{ Sq. Mt.}$$

$$T_a = 42\text{C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Bottom}} = 0.26 \times 1.070 \times 60 = 16.7 \text{ Watts}$$

$$Q_{\text{Bottom}} = 16.7 \text{ Watts}$$

5 - $Q_{\text{Door}} = [U A (T_a - T_f)]$

T_a = Ambient Temperature
 T_f = Freezer air Temperature

$$U = 1 / (0.065 / 0.0195) = 0.3 \text{ W/ Sq. Mt. C}$$

$$A = 1.070 \text{ Sq. Mt.}$$

$$T_a = 32 \text{ C}$$

$$T_f = - 18 \text{ C}$$

$$Q_{\text{Door}} = 0.3 \times 1.07 \times 50 = 16 \text{ Watts}$$

$$Q_{\text{Door}} = 16 \text{ Watts}$$

Total Heat Leaks;

$$Q_{\text{TL}} = 11 + 18.2 + 16.7 + 18.2 + 16 = 80$$

$$Q_{\text{Total Heat Leaks}} = 80 \text{ Watts}$$

b) Product Loads;

We consider 30 Kg ice making capacity for this model per 24 hours.
 Therefore;

$$Q_{\text{product}} = Q_1 + Q_2 + Q_3,$$

where;

$Q_1 = mC_1 (T_i - T_f)$ = energy required to freeze water from initial temperature to freezing point of 0 °C

$Q_2 = mC_2 (T_f - T_n)$ = energy required to freeze ice from zero degree temperature to -18 °C

$Q_3 = m \times h =$ heat gain from latent heat of fusion of water

$$Q_1 = 30 \times 1 \times (24-0) = 720 \text{ Kcal per 24 hour}$$

$$Q_2 = 30 \times 1 [0 - (-18)] = 540 \text{ Kcal per 24 hours}$$

$$Q_3 = 30 \times 108 = 3240 \text{ Kcal per 24 hours}$$

$$Q_{\text{product}} = 720 + 540 + 3240 = 4500 \text{ Kcal per 24 hour} = 187 \text{ Kcal / hour} = 218 \text{ W}$$

$$Q_{\text{Misc}} = 10 \% (Q_{\text{Heat Leaks}} + Q_{\text{Product Loads}}) = 10\%(80 + 218) = 30 \text{ w}$$

$$Q_{\text{Misc}} = 30 \text{ Watts}$$

$$Q_{\text{Misc}} = Q_{\text{Electricity}} + Q_{\text{Infiltration}} + Q_{\text{Door Opening}} + Q_{\text{Etc.}}$$

Total Cooling Capacity required is calculated as follows;

$$Q_{\text{Grand Total}} = Q_{\text{Heat Leaks}} + Q_{\text{Product Loads}} + Q_{\text{Misc.}}$$

$$Q_{\text{Grand Total}} = 80 + 218 + 30 = 328 \text{ Watts}$$

$$Q_{\text{Grand Total}} = 328 \text{ Watts}$$

Type of Compressor suitable for this model is recommended Compressor HUAYI Model

NO:1
 试验内容: 储藏温度
 直冷型冰箱
 机型: BP-166(R134a)
 型号: AE1350Y, .66*2100 140
 厂号: 32170X
 温控器位置(n值=5)
 测试条件:

群

冷冻室: -21.9 °C 测温点数: 6 (t1, t2, t3, t4, t5, t6,)

格式 1 汇总统计表

状态	时间	t1	t2	t3	t4	t5	t6	t7	t8	t9	t10	t11	t12	t13	t14	t15	t16	电流 (A)	电能1 (KWh)	功率 (W)	系数 (%)	电能2 (KWh/24h)	C.n	ΔT 秒	
1938-12-22																									
OFF	11:11:53	-19.87	-22.40	-22.29	-18.46	-18.77	-19.30											0.002	0.0279				5	834	
ON	11:25:47	-19.77	-22.35	-22.20	-18.40	-18.70	-19.24											0.907	0.0283				5	947	
OFF	11:41:34	-19.77	-22.27	-22.22	-18.47	-18.83	-19.38											0.002	0.0567	107.8	53.17	1.3938	5	837	
ON	11:55:31	-19.68	-22.27	-22.16	-18.30	-18.69	-19.20											0.915	0.0571				5	927	
OFF	12:10:58	-19.78	-22.30	-22.21	-18.44	-18.72	-19.27											0.001	0.0849	107.7	52.86	1.3875	5	820	
ON	12:24:38	-19.70	-22.30	-22.19	-18.39	-18.71	-19.28											0.919	0.0853				5	925	
OFF	12:40:3	-19.75	-22.26	-22.18	-18.40	-18.71	-19.30											0.000	0.1130	107.6	52.91	1.3894	5	779	
ON	12:53:2	-19.70	-22.28	-22.17	-18.38	-18.69	-19.24											0.912	0.1134				5	958	
OFF	13:9:0	-19.76	-22.26	-22.20	-18.42	-18.73	-19.28											0.002	0.1420	107.3	53.47	1.4023	5	823	
ON	13:22:43	-19.63	-22.23	-22.16	-18.38	-18.71	-19.27											0.909	0.1424				5	1000	
OFF	13:39:23	-19.75	-22.26	-22.16	-18.39	-18.72	-19.29											0.001	0.1721	106.9	53.75	1.4074	5	769	
ON	13:52:12	-19.72	-22.29	-22.15	-18.35	-18.63	-19.23											0.915	0.1720				5	933	
OFF	14:7:45	-19.77	-22.28	-22.16	-18.38	-18.69	-19.27											0.000	0.2004	107.4	53.92	1.4123	5	810	
ON	14:21:21	-19.72	-22.31	-22.16	-18.37	-18.68	-19.25											0.911	0.2008				5	925	
OFF	14:36:46	-19.77	-22.28	-22.19	-18.43	-18.74	-19.30											0.001	0.2285	107.5	53.81	1.4093	5	822	
ON	14:50:23	-19.69	-22.30	-22.18	-18.42	-18.72	-19.27											0.913	0.2290				5	958	
OFF	15:6:26	-19.76	-22.28	-22.18	-18.41	-18.70	-19.28											0.000	0.2575	107.0	53.81	1.4097	5	757	
ON	15:19:3	-19.68	-22.27	-22.14	-18.36	-18.70	-19.27											0.914	0.2579				5	816	

ON	17:13:15	-19.64	-22.26	-22.15	-18.35	-18.65	-19.22
OFF	17:34:32	-19.71	-22.25	-22.14	-18.35	-18.65	-19.25
ON	17:40:57	-19.68	-22.28	-22.16	-18.41	-18.71	-19.27
OFF	18:1:27	-19.71	-22.24	-22.14	-18.39	-18.65	-19.25
ON	18:15:38	-19.60	-22.28	-22.16	-18.41	-18.71	-19.27
OFF	18:31:57	-19.65	-22.20	-22.13	-18.39	-18.71	-19.26
ON	18:44:14	-19.60	-22.30	-22.21	-18.40	-18.70	-19.30
OFF	18:59:28	-19.71	-22.24	-22.16	-18.40	-18.70	-19.27
ON	19:13:20	-19.64	-22.24	-22.11	-18.34	-18.62	-19.17
OFF	19:28:30	-19.69	-22.22	-22.13	-18.35	-18.68	-19.24
ON	19:41:35	-19.63	-22.27	-22.17	-18.40	-18.65	-19.22
OFF	19:56:10	-19.71	-22.24	-22.16	-18.40	-18.65	-19.24
ON	20:10:57	-19.65	-22.26	-22.17	-18.40	-18.71	-19.28
OFF	20:25:19	-19.69	-22.23	-22.15	-18.35	-18.65	-19.19
ON	20:36:40	-19.64	-22.25	-22.15	-18.38	-18.65	-19.24
OFF	20:54:11	-19.73	-22.25	-22.23	-18.43	-18.71	-19.36
ON	21:0:50	-19.61	-22.21	-22.05	-18.31	-18.60	-19.17
OFF	21:21:24	-19.60	-22.20	-22.12	-18.32	-18.55	-19.14
ON	21:35:18	-19.47	-22.09	-22.01	-18.27	-18.55	-19.18
OFF	21:51:10	-19.72	-22.27	-22.19	-18.43	-18.70	-19.32
ON	22:3:59	-19.61	-22.20	-22.09	-18.33	-18.65	-19.18
OFF	22:18:35	-19.74	-22.27	-22.18	-18.41	-18.72	-19.28
ON	22:32:21	-19.66	-22.27	-22.16	-18.36	-18.65	-19.25
OFF	22:47:53	-19.67	-22.11	-22.10	-18.30	-18.63	-19.15
ON	23:1:8	-19.63	-22.24	-22.14	-18.35	-18.65	-19.21
OFF	23:16:12	-19.65	-22.21	-22.14	-18.35	-18.71	-19.23
ON	23:28:58	-19.58	-22.22	-22.13	-18.34	-18.62	-19.17
OFF	23:43:23	-19.68	-22.24	-22.17	-18.41	-18.71	-19.23
ON	23:57:50	-19.67	-22.27	-22.17	-18.37	-18.62	-19.15
1998-12-25							
OFF	0:12:59	-19.64	-22.18	-22.09	-18.32	-18.61	-19.20
ON	0:26:41	-19.60	-22.21	-22.09	-18.33	-18.62	-19.20
OFF	0:42:6	-19.68	-22.22	-22.15	-18.41	-18.71	-19.30
ON	0:54:27	-19.63	-22.24	-22.14	-18.37	-18.65	-19.21
OFF	1:8:54	-19.65	-22.20	-22.09	-18.33	-18.62	-19.17
ON	1:22:52	-19.59	-22.24	-22.12	-18.34	-18.67	-19.25
OFF	1:38:5	-19.65	-22.19	-22.08	-18.30	-18.65	-19.23
ON	1:50:54	-19.61	-22.20	-22.07	-18.32	-18.61	-19.19
OFF	2:0:0	-19.66	-22.20	-22.11	-18.37	-18.66	-19.25
ON	2:19:38	-19.59	-22.22	-22.10	-18.30	-18.64	-19.20
OFF	2:34:20	-19.56	-22.08	-21.96	-18.20	-18.53	-19.12
ON	2:46:58	-19.53	-22.20	-22.09	-18.33	-18.62	-19.19
OFF	3:1:6	-19.63	-22.17	-22.08	-18.34	-18.61	-19.16
ON	3:14:54	-19.58	-22.21	-22.11	-18.36	-18.65	-19.20
OFF	3:30:3	-19.64	-22.16	-22.08	-18.34	-18.61	-19.18
ON	3:42:30	-19.59	-22.20	-22.08	-18.35	-18.63	-19.17
OFF	3:56:55	-19.62	-22.15	-22.09	-18.33	-18.63	-19.20
ON	4:10:44	-19.59	-22.22	-22.11	-18.30	-18.60	-19.23
OFF	4:25:40	-19.59	-22.13	-22.05	-18.30	-18.60	-19.19
ON	4:36:0	-19.55	-22.20	-22.06	-18.32	-18.63	-19.23
OFF	4:53:20	-19.63	-22.18	-22.09	-18.33	-18.64	-19.21
ON	5:7:5	-19.54	-22.10	-22.04	-18.24	-18.57	-19.13
OFF	5:21:30	-19.62	-22.17	-22.08	-18.31	-18.64	-19.21
ON	5:34:45	-19.58	-22.18	-22.08	-18.30	-18.63	-19.19
OFF	5:49:10	-19.62	-22.14	-22.05	-18.27	-18.60	-19.15
ON	6:2:48	-19.49	-22.11	-22.04	-18.20	-18.50	-19.11
OFF	6:17:35	-19.57	-22.12	-22.05	-18.29	-18.64	-19.22
ON	6:29:57	-19.57	-22.18	-22.09	-18.32	-18.64	-19.22
OFF	6:44:0	-19.56	-22.10	-22.01	-18.20	-18.58	-19.17
ON	6:57:52	-19.52	-22.14	-22.03	-18.26	-18.58	-19.15
871	0.914	0.3701	0.4040	107.9	54.00	1.4150	5
917	0.000	0.4040	107.9	54.00	1.4150	5	
745	0.914	0.4044	107.9	54.00	1.4154	5	
870	0.002	0.4305	107.9	54.00	1.4154	5	
851	0.913	0.4309	107.9	54.00	1.4154	5	
931	0.000	0.4367	107.4	53.53	1.4122	5	
785	0.916	0.4331	107.4	53.53	1.4120	5	
914	0.000	0.4304	107.4	53.52	1.4120	5	
882	0.915	0.4308	107.4	53.52	1.4120	5	
910	0.000	0.5141	107.6	53.82	1.4030	5	
785	0.917	0.5144	107.6	53.82	1.4030	5	
861	0.000	0.5409	108.1	53.77	1.4087	5	
829	0.920	0.5413	108.1	53.77	1.4087	5	
904	0.000	0.5684	107.9	53.69	1.4067	5	
817	0.917	0.5688	107.9	53.69	1.4067	5	
925	0.000	0.5307	108.1	53.60	1.4064	5	
759	0.916	0.5370	108.1	53.60	1.4064	5	
874	0.000	0.6233	108.2	53.65	1.4066	5	
834	0.918	0.6237	108.2	53.65	1.4066	5	
952	0.003	0.6323	107.8	53.64	1.4064	5	
709	0.910	0.6327	107.8	53.64	1.4064	5	
876	0.000	0.6768	107.4	53.62	1.4059	5	
820	0.918	0.6752	107.4	53.62	1.4059	5	
982	0.001	0.7072	108.1	53.59	1.4054	5	
750	0.912	0.7076	108.1	53.59	1.4054	5	
898	0.002	0.7343	107.7	53.59	1.4055	5	
827	0.914	0.7353	107.7	53.59	1.4055	5	
924	0.002	0.7630	107.7	53.56	1.4047	5	
750	0.911	0.7633	107.7	53.56	1.4047	5	
503	0.001	0.7303	107.4	53.59	1.4055	5	
822	0.916	0.7309	107.4	53.59	1.4055	5	
925	0.002	0.8160	107.7	53.57	1.4053	5	
741	0.911	0.8190	107.7	53.57	1.4053	5	
807	0.000	0.8450	108.0	53.58	1.4057	5	
836	0.911	0.8453	108.0	53.58	1.4057	5	
913	0.000	0.8727	107.6	53.53	1.4044	5	
709	0.913	0.8732	107.6	53.53	1.4044	5	
900	0.000	0.9003	107.5	53.55	1.4049	5	
818	0.912	0.9008	107.5	53.55	1.4049	5	
888	0.000	0.9274	107.6	53.50	1.4040	5	
752	0.917	0.9279	107.6	53.50	1.4040	5	
850	0.000	0.9534	108.1	53.49	1.4040	5	
820	0.916	0.9539	108.1	53.49	1.4040	5	
909	0.000	0.9812	107.9	53.46	1.4033	5	
747	0.913	0.9816	107.9	53.46	1.4033	5	
865	0.000	1.0070	107.8	53.40	1.4030	5	
829	0.918	1.0080	107.8	53.40	1.4030	5	
890	0.000	1.0349	107.9	53.42	1.4027	5	
740	0.916	1.0354	107.9	53.42	1.4027	5	
920	0.002	1.0630	107.7	53.47	1.4042	5	
825	0.915	1.0635	107.7	53.47	1.4042	5	
871	0.001	1.0897	108.1	53.42	1.4031	5	
789	0.921	1.0902	108.1	53.42	1.4031	5	
871	0.000	1.1163	107.6	53.40	1.4026	5	
812	0.913	1.1167	107.6	53.40	1.4026	5	
897	0.002	1.1430	107.7	53.37	1.4020	5	
732	0.912	1.1439	107.7	53.37	1.4020	5	
849	0.000	1.1695	108.1	53.38	1.4024	5	
820	0.914	1.1699	108.1	53.38	1.4024	5	

OFF	7:12:9	-19.58	-22.11	-22.02	-18.22	-18.54	-19.14	0.000	1.1956	107.9	53.32	1.4009	5	857
ON	7:24:31	-19.54	-22.15	-22.08	-18.29	-18.63	-19.20	0.913	1.1960				5	742
OFF	7:38:45	-19.48	-22.00	-21.92	-18.19	-18.54	-19.12	0.001	1.2218	108.4	53.33	1.4013	5	854
ON	7:52:5	-19.61	-22.22	-22.13	-18.34	-18.68	-19.23	0.918	1.2222				5	800
OFF	8:8:0	-19.62	-22.15	-22.08	-18.31	-18.63	-19.17	0.001	1.2508	107.9	53.35	1.4019	5	955
ON	8:20:19	-19.55	-22.12	-21.99	-18.21	-18.56	-19.14	0.914	1.2514				5	739
OFF	8:34:1	-19.61	-22.14	-22.04	-18.26	-18.62	-19.15	0.001	1.2761	108.0	53.34	1.4018	5	822
ON	8:47:49	-19.53	-22.12	-22.01	-18.25	-18.55	-19.11	0.916	1.2765				5	828
OFF	9:1:20	-19.60	-22.13	-22.05	-18.30	-18.63	-19.20	0.000	1.3010	108.6	53.26	1.4000	5	811
ON	9:14:8	-19.43	-22.04	-21.91	-18.15	-18.48	-19.07	0.916	1.3014				5	768

1998-12-23 9:14:8 (Fmax)=-18.15 °C

霜 33沉霜霜霜霜霜霜霜(Fmin)=-22.40 °C

霜霜霜霜霜 (ton)=88.80 °C (tm)=88.80 °C

(toff)=88.80 °C

电流=0.916 (A)

耗电量=1.4000 (KWh/24h)

(ON=压缩机通电,OFF=压缩机断电,*on=化霜加热器通电,*off=化霜加热器断电)

(max=状态变化之间冷冻室最热点时刻,min=状态变化之间冷冻室最冷点时刻)

(Fmax=冷冻室最热点,Fmin=冷冻室最冷点,d=化霜开始冷冻室最热点等于-18°C时刻)

(tm=ton值与上一状态平均值的再平均值)

(toff=吨藏室t10,t11,t12最冷点的平均值,tn=toff值与上一状态平均值的再平均值)

(*max=化霜开始冷冻室最热点时刻)

制表时间:1998-12-23 9:25:46

NO:2

试验内容:储藏温度

直冷型冰箱

机型:BD-168(R134a)

型号:AE1350Y .66*2100 150

厂商:32'70%

温控器位置Cn值=5

温度条件:

冷冻室:-21.9 °C 测温点数:8(t1, t2, t3, t4, t5, t6, t7, t8,)

格式 1 汇总统计表

状态	时间	t1	t2	t3	t4	t5	t6	t7	t8	t9	t10	t11	t12	t13	t14	t15	t16	电流 (A)	电能1 (KWh)	功率 (W)	系数 (%)	电能2 (KWh/24h)	Cn	ΔT	
1998-12-22																									
OFF	11:19:9	-20.29	-20.22	-17.11	-23.94	-22.63	-22.57	-21.80	-22.03									0.000	0.0392				5		
ON	11:39:24	-20.11	-20.22	-17.13	-23.63	-22.64	-22.60	-21.84	-22.07									0.944	0.0397				5	1215	
OFF	12:0:17	-20.33	-20.27	-17.18	-23.98	-22.65	-22.59	-21.82	-22.06									0.002	0.0872	100.3	57.04	1.4074	5	1013	
ON	12:26:23	-20.12	-20.21	-17.09	-23.59	-22.60	-22.53	-21.78	-22.00									0.952	0.0876				5	1200	
OFF	12:57:21	-20.36	-20.29	-17.15	-23.98	-22.61	-22.55	-21.81	-22.05									0.003	0.1419	105.3	58.91	1.5064	5	1858	
ON	13:18:36	-20.03	-20.15	-17.00	-23.48	-22.47	-22.41	-21.60	-21.88									0.934	0.1424				5	1275	
OFF	13:46:6	-20.43	-20.33	-17.28	-24.04	-22.63	-22.58	-21.84	-22.02									0.002	0.1909	105.8	58.08	1.4804	5	1650	
ON	14:0:38	-20.11	-20.22	-17.11	-23.60	-22.58	-22.53	-21.81	-22.00									0.938	0.1913				5	1232	
OFF	14:34:23	-20.37	-20.31	-17.18	-23.96	-22.60	-22.54	-21.78	-22.03									0.000	0.2402	105.9	57.93	1.4829	5	1665	
ON	14:55:9	-20.18	-20.28	-17.19	-23.67	-22.60	-22.63	-21.89	-22.11									0.932	0.2408				5	1240	
OFF	15:24:15	-20.38	-20.31	-17.18	-23.98	-22.61	-22.57	-21.82	-22.07									0.003	0.2920	105.7	58.02	1.4854	5	1740	
ON	15:45:16	-20.06	-20.25	-17.13	-23.63	-22.55	-22.59	-21.77	-22.05									0.946	0.2925				5	1261	
OFF	16:11:27	-20.45	-20.36	-17.25	-24.04	-22.69	-22.65	-21.89	-22.15									0.004	0.3388	106.2	57.61	1.4759	5	1571	
ON	16:31:53	-20.24	-20.32	-17.20	-23.68	-22.66	-22.61	-21.86	-22.09									0.940	0.3392				5	1226	
OFF	16:58:45	-20.38	-20.28	-17.20	-23.95	-22.60	-22.57	-21.81	-22.06									0.003	0.3867	106.2	57.49	1.4734	5	1612	
ON	17:19:0	-20.12	-20.22	-17.14	-23.62	-22.60	-22.56	-21.81	-22.03									0.947	0.3871				5	1215	
OFF	17:44:37	-20.33	-20.23	-17.17	-23.91	-22.58	-22.55	-21.79	-22.05									0.003	0.4325	106.4	57.30	1.4693	5	1537	
ON	18:4:58	-20.07	-20.17	-17.12	-23.57	-22.57	-22.51	-21.75	-21.99									0.950	0.4329				5	1221	
OFF	18:30:53	-20.36	-20.26	-17.21	-23.97	-22.62	-22.56	-21.77	-22.01									0.000	0.4789	106.7	57.16	1.4668	5	1555	
ON	18:51:5	-20.13	-20.22	-17.14	-23.59	-22.58	-22.54	-21.76	-21.99									0.946	0.4794				5	1212	
OFF	19:16:53	-20.31	-20.20	-17.14	-23.88	-22.55	-22.52	-21.74	-21.99									0.003	0.5252	106.8	57.06	1.4650	5	1548	
ON	19:37:6	-20.09	-20.17	-17.09	-23.53	-22.53	-22.48	-21.70	-21.94									0.948	0.5258				5	1213	
OFF	20:3:10	-20.28	-20.16	-17.12	-23.87	-22.61	-22.61	-21.83	-22.06									0.002	0.5719	106.4	56.99	1.4640	5	1564	
ON	20:23:21	-20.01	-20.12	-17.08	-23.50	-22.47	-22.39	-21.59	-21.81									0.934	0.5723				5	1211	

OFF 21:33:58 -20.26 -20.14 -17.09 -23.79 -22.48 -22.44 -21.64 -21.89
ON 21:53:36 -20.13 -20.20 -17.12 -23.53 -22.53 -22.50 -21.76 -22.03
OFF 22:19:8 -20.32 -20.22 -17.17 -23.90 -22.59 -22.55 -21.77 -22.03
ON 22:38:50 -20.12 -20.21 -17.14 -23.57 -22.58 -22.53 -21.75 -21.97
OFF 23:5:11 -20.20 -20.12 -17.13 -23.86 -22.48 -22.44 -21.68 -21.92
ON 23:24:59 -20.09 -20.16 -17.09 -23.49 -22.49 -22.44 -21.65 -21.90
OFF 23:51:13 -20.31 -20.21 -17.14 -23.81 -22.47 -22.47 -21.72 -22.01
1998-12-23
ON 0:11:6 -20.11 -20.20 -17.13 -23.54 -22.52 -22.48 -21.69 -21.91
OFF 0:38:31 -20.29 -20.21 -17.15 -23.87 -22.53 -22.49 -21.72 -21.95
ON 0:58:32 -20.10 -20.19 -17.13 -23.56 -22.55 -22.48 -21.69 -21.91
OFF 1:24:50 -20.36 -20.25 -17.16 -23.89 -22.55 -22.47 -21.73 -21.98
ON 1:45:0 -20.14 -20.22 -17.17 -23.56 -22.55 -22.50 -21.73 -21.93
OFF 2:12:12 -20.29 -20.19 -17.15 -23.85 -22.51 -22.47 -21.67 -21.92
ON 2:32:43 -20.11 -20.22 -17.15 -23.53 -22.53 -22.50 -21.73 -21.96
OFF 2:57:43 -20.33 -20.27 -17.25 -23.90 -22.55 -22.54 -21.75 -22.06
ON 3:17:31 -20.08 -20.13 -17.12 -23.50 -22.49 -22.46 -21.67 -21.90
OFF 3:44:3 -20.29 -20.20 -17.19 -23.86 -22.52 -22.50 -21.73 -21.99
ON 4:4:11 -20.10 -20.20 -17.17 -23.55 -22.58 -22.48 -21.71 -21.94
OFF 4:30:18 -20.32 -20.21 -17.21 -23.87 -22.55 -22.50 -21.73 -22.02
ON 4:50:12 -20.14 -20.23 -17.19 -23.56 -22.56 -22.52 -21.70 -21.90
OFF 5:15:20 -20.23 -20.17 -17.14 -23.86 -22.56 -22.55 -21.75 -21.99
ON 5:35:19 -20.16 -20.18 -17.11 -23.53 -22.52 -22.47 -21.68 -21.92
OFF 6:2:5 -20.32 -20.23 -17.12 -23.87 -22.54 -22.47 -21.69 -21.94
ON 6:21:59 -20.23 -20.32 -17.16 -23.66 -22.67 -22.64 -21.87 -22.09
OFF 6:49:23 -20.40 -20.31 -17.16 -23.99 -22.64 -22.57 -21.78 -22.02
ON 7:3:44 -20.16 -20.26 -17.13 -23.66 -22.66 -22.59 -21.81 -22.03
OFF 7:34:54 -20.30 -20.16 -17.03 -23.83 -22.49 -22.47 -21.72 -21.97
ON 7:54:54 -20.12 -20.22 -17.15 -23.61 -22.59 -22.54 -21.75 -21.98
OFF 8:20:35 -20.30 -20.22 -17.17 -23.91 -22.62 -22.54 -21.74 -22.02
ON 8:40:23 -20.10 -20.18 -17.11 -23.57 -22.55 -22.48 -21.71 -21.91
OFF 9:3:32 -20.35 -20.22 -17.19 -23.93 -22.65 -22.61 -21.82 -22.07
ON 9:23:22 -20.06 -20.13 -17.09 -23.52 -22.55 -22.50 -21.70 -21.93

0.001 0.0024 100.7 50.79 1.4598 5 1500
0.934 0.6630 5 1178
0.003 0.7081 100.3 50.78 1.4596 5 1532
0.947 0.7086 5 1182
0.001 0.7552 100.2 50.81 1.4604 5 1581
0.949 0.7556 5 1188
0.000 0.8020 100.2 50.82 1.4606 5 1574
0.929 0.8025 5 1193
0.000 0.8509 100.0 50.88 1.4622 5 1645
0.929 0.8513 5 1201
0.001 0.8979 100.3 50.88 1.4621 5 1578
0.928 0.8384 5 1210
0.001 0.9464 100.1 50.91 1.4628 5 1632
0.942 0.9469 5 1231
0.003 0.9912 100.5 50.81 1.4607 5 1500
0.933 0.9916 5 1138
0.001 1.0385 100.1 50.83 1.4611 5 1592
0.950 1.0389 5 1208
0.004 1.0851 100.3 50.82 1.4607 5 1567
0.940 1.0856 5 1194
0.003 1.1302 100.6 50.77 1.4599 5 1508
0.949 1.1307 5 1199
0.000 1.1781 100.4 50.79 1.4605 5 1606
0.941 1.1785 5 1194
0.002 1.2270 100.2 50.84 1.4619 5 1644
0.942 1.2274 5 1221
0.002 1.2721 100.7 50.78 1.4604 5 1510
0.930 1.2726 5 1200
0.004 1.3182 100.6 50.76 1.4601 5 1541
0.939 1.3187 5 1188
0.003 1.3599 107.0 50.67 1.4581 5 1389
0.933 1.3604 5 1190

(ON=压缩机通电,OFF=压缩机断电,*on=化霜加热器通电,*off=化霜加热器断电)
(max=状态变化之间冷冻室最热点时刻,min=状态变化之间冷冻室最冷点时刻)
(Fmax=冷冻室最热点,Fmin=冷冻室最冷点,d=化霜开始冷冻室最热点等于-18℃时刻)
(ton=贮藏室t10,t11,t12最热点的平均值,tm=ton值与上一状态平均值的再平均值)
(toff=贮藏室t10,t11,t12最冷点的平均值,tn=toff值与上一状态平均值的再平均值)
(*max=化霜开始冷冻室最热点时刻)

1998-12-22 13:18:36 1998-12-22 13:46:6 (Fmax)=-17.00 °C
1998-12-22 13:46:6 (Fmin)=-24.04 °C
霜霜霜霜 (ton)=88.80 °C (tm)=88.80 °C
(toff)=88.80 °C (tn)=88.80 °C
电流=0.933 (A)
耗电量=1.4581 (KWh/24h)

制表时间:1998-12-23 9:25:46

NO:1
 试验内容:满载温度
 直冷型冰柜
 机号:55-168(R13-1a)
 型号:AE1330F, .603x2100 140
 厂号:32705
 温控器位置Cn值=5
 温度条件:

冷冻室:-21.9 °C 调温点数:6(t1, t2, t3, t4, t5, t6)

格式 1 汇总统计表

状态	时间	t1	t2	t3	t4	t5	t6	t7	t8	t9	t10	t11	t12	t13	t14	t15	t16	电流 (A)	电能1 (kWh)	功率 (W)	系数 (%)	电能2 (kWh/24h)	ΔT 秒
1988-12-18																							
ON	16:50:27	-21.12	-22.18	-22.57	-22.50	-22.01	-22.23											0.907	0.0904	107.4	59.49	1.5305	887
OFF	17:55:14	-23.01	-24.00	-23.27	-23.23	-23.00	-24.01											0.903	0.0269	107.4			804
ON	17:15:13	-21.14	-22.17	-22.57	-22.52	-22.04	-22.32											0.906	0.0272	107.0	58.65	1.5333	898
OFF	17:25:10	-22.89	-23.50	-23.14	-23.12	-22.95	-23.79											0.900	0.0522	107.0			802
ON	17:35:13	-21.05	-22.08	-22.45	-22.36	-21.92	-22.17											0.903	0.0520	107.0	58.47	1.5333	825
OFF	17:53:7	-22.84	-23.81	-23.06	-23.00	-22.90	-23.79											0.903	0.0775	107.0			806
ON	18:3:15	-21.05	-22.08	-22.46	-22.37	-21.91	-22.15											0.900	0.1027	107.2	56.46	1.5305	830
OFF	18:17:8	-22.85	-23.85	-23.09	-23.03	-22.90	-23.84											0.906	0.1051	107.0			590
ON	18:27:4	-21.13	-22.12	-22.51	-22.43	-21.98	-22.20											0.901	0.1280	107.5	58.32	1.5233	831
OFF	18:40:55	-22.84	-23.85	-23.08	-23.05	-22.88	-23.80											0.911	0.1284	107.0			603
ON	18:50:56	-21.04	-22.07	-22.45	-22.40	-21.95	-22.21											0.901	0.1530	107.9	58.23	1.5272	822
OFF	19:4:40	-22.79	-23.81	-23.02	-22.93	-22.72	-23.80											0.905	0.1534	107.0			603
ON	19:14:43	-20.85	-21.88	-22.25	-22.18	-21.73	-22.01											0.903	0.1781	107.3	58.21	1.5293	826
OFF	19:28:31	-22.77	-23.83	-23.07	-23.03	-22.85	-23.80											0.905	0.1785	107.0			837
ON	19:38:28	-20.92	-22.00	-22.36	-22.28	-21.83	-22.11											0.900	0.2029	107.5	56.12	1.5233	815
OFF	19:52:3	-22.72	-23.74	-22.97	-22.94	-22.77	-23.68											0.903	0.2034	107.0			802
ON	20:2:5	-20.81	-21.85	-22.19	-22.14	-21.68	-21.95											0.900	0.2277	107.0	58.05	1.5246	809
OFF	20:15:34	-22.72	-23.73	-22.97	-22.90	-22.77	-23.63											0.915	0.2281	107.0			597
ON	20:25:31	-21.02	-22.03	-22.40	-22.33	-21.90	-22.17											0.902	0.2523	107.8	58.00	1.5230	806
OFF	20:38:57	-22.74	-23.73	-22.99	-22.93	-22.75	-23.63											0.912	0.2520	107.0			596
ON	20:48:53	-21.02	-22.02	-22.40	-22.34	-21.90	-22.17											0.901	0.2770	107.0	57.95	1.5229	814
OFF	21:2:27	-22.83	-23.86	-23.00	-22.90	-22.78	-23.72											0.901	0.2774	107.0			805
ON	21:12:32	-21.02	-22.03	-22.38	-22.30	-21.86	-22.10											0.903	0.3015	107.1	57.87	1.5193	810
OFF	21:26:2	-22.74	-23.73	-22.98	-22.91	-22.81	-23.72											0.903	0.3015	107.0			611
ON	21:36:13	-20.91	-21.90	-22.24	-22.19	-21.83	-22.08											0.901	0.3205	107.2	57.81	1.5176	825
OFF	21:45:56	-22.76	-23.77	-22.99	-22.93	-22.83	-23.74											0.905	0.3203	107.0			613
ON	22:0:17	-20.83	-21.80	-22.16	-22.10	-21.72	-21.93											0.901	0.3514	107.0	57.75	1.5160	821
OFF	22:13:58	-22.70	-23.72	-22.95	-22.92	-22.76	-23.69											0.913	0.3518	107.0			619
ON	22:24:17	-20.83	-21.83	-22.19	-22.13	-21.73	-22.00											0.901	0.3768	107.3	57.71	1.5149	834
OFF	22:38:11	-22.73	-23.82	-23.04	-23.02	-22.80	-23.76											0.908	0.3772	107.0			625
ON	22:48:30	-20.83	-21.83	-22.19	-22.13	-21.73	-22.03											0.900	0.4018	107.1	57.69	1.5157	823
OFF	23:2:23	-22.72	-23.77	-22.95	-22.94	-22.76	-23.67											0.907	0.4022	107.0			618
ON	23:12:43	-20.85	-21.84	-22.20	-22.14	-21.74	-22.00											0.900	0.4267	107.2	57.60	1.5160	823
OFF	23:26:20	-22.67	-23.64	-22.88	-22.88	-22.70	-23.57											0.912	0.4272	107.0			613
ON	23:36:39	-20.87	-21.86	-22.24	-22.15	-21.71	-21.97											0.901	0.4517	107.5	57.60	1.5160	820
OFF	23:50:19	-22.67	-23.63	-22.92	-22.89	-22.72	-23.57											0.913	0.4522	107.0	57.61	1.5110	827
1988-12-19																							
ON	0:9:49	-20.83	-21.83	-22.27	-22.22	-21.72	-21.86											0.900	0.4770	107.0			833
OFF	0:14:59	-22.71	-23.71	-22.92	-22.87	-22.77	-23.67																

5-10 min

ON	0:49:2	-20.79	-21.81	-22.20	-22.14	-21.68	-21.92	0.906	0.5023	57.36	1.5101	5	628
OFF	1:2:47	-22.04	-23.03	-22.84	-22.81	-22.70	-23.57	0.001	0.5270	107.7	1.5095	5	825
ON	1:13:16	-20.70	-21.78	-22.15	-22.10	-21.64	-21.91	0.908	0.5275	57.52	1.5095	5	629
OFF	1:26:39	-22.68	-23.66	-22.89	-22.88	-22.75	-23.59	0.001	0.5521	107.6	1.5094	5	828
ON	1:37:17	-20.87	-21.91	-22.27	-22.18	-21.73	-21.98	0.910	0.5526	57.50	1.5094	5	618
OFF	1:50:43	-22.60	-23.64	-22.83	-22.91	-22.77	-23.63	0.000	0.5769	107.2	1.5088	5	812
ON	2:1:4	-20.60	-21.88	-22.25	-22.21	-21.74	-21.90	0.911	0.5773	57.47	1.5088	5	615
OFF	2:14:35	-22.61	-23.68	-22.86	-22.85	-22.67	-23.58	0.001	0.6010	107.6	1.5082	5	811
ON	2:24:56	-20.84	-21.86	-22.25	-22.18	-21.72	-21.90	0.909	0.6021	57.44	1.5082	5	621
OFF	2:36:33	-22.09	-23.71	-22.94	-22.93	-22.74	-23.64	0.001	0.6263	107.5	1.5079	5	817
ON	2:48:51	-20.80	-21.91	-22.28	-22.24	-21.76	-22.01	0.909	0.6270	57.42	1.5079	5	618
OFF	3:2:22	-22.62	-23.60	-22.88	-22.86	-22.70	-23.57	0.001	0.6512	107.6	1.5074	5	811
ON	3:12:10	-20.82	-21.84	-22.23	-22.17	-21.70	-21.94	0.910	0.6517	57.39	1.5074	5	618
OFF	3:26:14	-22.64	-23.67	-22.83	-22.82	-22.72	-23.65	0.001	0.6757	107.5	1.5065	5	804
ON	3:36:21	-20.70	-21.81	-22.10	-22.10	-21.64	-21.89	0.906	0.6761	57.36	1.5065	5	617
OFF	3:49:53	-22.61	-23.60	-22.84	-22.82	-22.67	-23.56	0.000	0.7004	107.5	1.5061	5	812
ON	4:0:9	-20.82	-21.83	-22.19	-22.16	-21.71	-21.97	0.911	0.7008	57.85	1.5061	5	616
OFF	4:13:41	-22.58	-23.60	-22.80	-22.78	-22.66	-23.51	0.000	0.7250	107.1	1.5055	5	812
ON	4:23:53	-20.80	-21.84	-22.19	-22.11	-21.69	-21.95	0.905	0.7253	57.84	1.5055	5	612
OFF	4:37:19	-22.60	-23.61	-22.85	-22.88	-22.72	-23.56	0.000	0.7494	107.2	1.5055	5	800
ON	4:47:34	-20.85	-21.81	-22.18	-22.12	-21.69	-21.94	0.910	0.7498	57.82	1.5048	5	615
OFF	5:1:5	-22.61	-23.62	-22.84	-22.82	-22.65	-23.56	0.001	0.7741	107.7	1.5045	5	811
ON	5:11:29	-20.70	-21.76	-22.14	-22.09	-21.64	-21.91	0.914	0.7746	57.29	1.5045	5	624
OFF	5:25:7	-22.57	-23.56	-22.79	-22.78	-22.63	-23.53	0.001	0.7994	107.1	1.5041	5	818
ON	5:35:24	-20.79	-21.79	-22.15	-22.05	-21.61	-21.85	0.910	0.7994	57.28	1.5041	5	617
OFF	5:48:54	-22.64	-23.60	-22.82	-22.86	-22.73	-23.56	0.001	0.8235	107.2	1.5038	5	810
ON	5:58:16	-20.71	-21.72	-22.07	-22.10	-21.60	-21.87	0.910	0.8241	57.26	1.5038	5	622
OFF	6:12:47	-22.61	-23.62	-22.86	-22.83	-22.66	-23.53	0.001	0.8484	107.1	1.5033	5	811
ON	6:23:16	-20.70	-21.73	-22.12	-22.05	-21.58	-21.82	0.913	0.8483	57.23	1.5033	5	629
OFF	6:36:48	-22.61	-23.61	-22.82	-22.78	-22.61	-23.53	0.001	0.8732	107.0	1.5033	5	812
ON	6:47:13	-20.71	-21.70	-22.10	-22.01	-21.57	-21.85	0.910	0.8737	57.21	1.5023	5	625
OFF	7:0:10	-22.54	-23.56	-22.78	-22.78	-22.64	-23.53	0.001	0.8979	107.7	1.5023	5	807
ON	7:11:44	-20.60	-21.66	-22.04	-22.00	-21.57	-21.84	0.908	0.8982	57.19	1.5023	5	624
OFF	7:24:33	-22.49	-23.49	-22.74	-22.72	-22.58	-23.46	0.001	0.9225	108.1	1.5023	5	809
ON	7:35:1	-20.73	-21.74	-22.12	-22.02	-21.55	-21.81	0.914	0.9230	57.16	1.5020	5	628

(ON=压缩机通电,OFF=压缩机断电,xon=化霜加热器通电,xoff=化霜加热器断电)
(max=状态变化之回冷室最热点时刻,min=状态变化之回冷室最冷点时刻)
(Fmax=冷冻室最热点,Fmin=冷冻室最冷点,t=化霜开始冷冻室最热点等于-18℃时刻)
(ton=化霜室t10,t11,t12最冷点的平均值,t=ton值与上一状态平均值的再平均值)
(toff=化霜室t10,t11,t12最冷点的平均值,t=toff值与上一状态平均值的再平均值)
(xmax=化霜开始冷冻室最热点时刻)

1998-12-19 7:11:4 (Fmax)=-20.60 °C
(Fmin)=-24.00 °C
(tm)=88.80 (tr)=88.80 °C
(ton)=88.80 °C (toff)=88.80 °C
电流=0.914 (A)
耗电量=1.5020 (KWh/24h)

制表时间:1998-12-19 7:35:23

NO:2
试验内容:储藏温度
直冷型冰箱
机型号:R166(R134a)
型号:HE1350T.66*2100 150
厂商:32'70%
温控器位置:U值=3
温度条件:
冷冻室:-21.9 °C 霜量点:8(t1, t2, t3, t4, t5, t6, t7, t8,)

格式1 汇总表

冷冻室	t1	t2	t3	t4	t5	t6	t7	t8	t9	t10	t11	t12	t13	t14	t15	t16	电流	电能1	功率	系数	电能2	C/D	—T
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直冷型冰箱
 型号:BD-168(R134a)
 型号:AE1350Y.66*2100 140
 方向:32/70%
 温控器位置:Ch值=1
 温度条件:

冷冻室:-21.9 °C 测温点数:0(t1, t2, t3, t4, t5, t6,)

格式 1 汇总表

状态	时间	t1	t2	t3	t4	t5	t6	t7	t8	t9	t10	t11	t12	t13	t14	t15	t16	电流 (A)	电能1 (kWh)	功率 (W)	系数 (%)	电能2 (kWh/24h)	△T 秒
ON	11:45:25	-12.15	-13.12	-13.67	-13.61	-13.01	-13.21											1.010	0.0004				194
OFF	11:48:39	-11.85	-12.84	-13.10	-13.19	-12.52	-12.81											0.000	0.0079	138.4	26.40	0.6213	685
ON	11:59:14	-11.45	-12.34	-12.65	-12.63	-12.27	-12.47											1.013	0.0083				199
OFF	12:2:33	-11.23	-12.10	-12.25	-12.27	-11.80	-12.11											0.000	0.0160	138.4	24.24	0.6567	583
ON	12:12:26	-11.21	-12.09	-12.30	-12.26	-11.96	-12.16											1.012	0.0160				199
OFF	12:15:45	-11.00	-11.94	-11.99	-12.00	-11.59	-11.98											0.002	0.0242	138.0	24.65	0.6730	582
ON	12:25:27	-11.10	-11.98	-12.10	-12.11	-11.84	-12.08											1.014	0.0247				204
OFF	12:28:51	-10.89	-11.86	-11.83	-11.87	-11.48	-11.90											0.000	0.0325	135.9	25.08	0.6851	568
ON	12:38:19	-11.02	-11.90	-12.03	-11.97	-11.69	-11.94											1.013	0.0329				208
OFF	12:41:47	-10.93	-11.91	-11.85	-11.87	-11.49	-11.93											0.001	0.0403	136.6	25.42	0.6951	567
ON	12:51:14	-10.96	-11.90	-12.06	-12.00	-11.72	-11.95											1.013	0.0414				204
OFF	12:54:38	-10.91	-11.84	-11.77	-11.76	-11.35	-11.79											0.002	0.0492	138.7	25.60	0.7004	566
ON	13:4:4	-10.92	-11.84	-12.00	-11.94	-11.56	-11.89											1.017	0.0490				209
OFF	13:7:39	-10.80	-11.78	-11.74	-11.77	-11.38	-11.81											0.000	0.0570	137.1	25.83	0.7073	567
ON	13:16:50	-10.83	-11.77	-11.92	-11.86	-11.59	-11.84											1.015	0.0580				208
OFF	13:20:18	-10.80	-11.75	-11.69	-11.69	-11.29	-11.72											0.002	0.0660	136.4	25.96	0.7162	561
ON	13:29:39	-10.82	-11.70	-11.86	-11.80	-11.52	-11.78											1.016	0.0665				203
OFF	13:33:2	-10.82	-11.74	-11.70	-11.71	-11.32	-11.74											0.002	0.0744	139.9	26.04	0.7167	562
ON	13:42:24	-10.81	-11.67	-11.81	-11.75	-11.40	-11.72											1.015	0.0749				205
OFF	13:45:49	-10.72	-11.67	-11.62	-11.62	-11.20	-11.66											0.003	0.0827	137.3	26.14	0.7202	563
ON	13:55:2	-10.77	-11.67	-11.83	-11.80	-11.50	-11.75											1.018	0.0833				204
OFF	13:58:26	-10.71	-11.68	-11.60	-11.58	-11.17	-11.62											0.002	0.0911	138.5	26.19	0.7214	560
ON	14:7:40	-10.80	-11.70	-11.83	-11.76	-11.44	-11.68											1.016	0.0915				210
OFF	14:11:10	-10.70	-11.67	-11.61	-11.61	-11.21	-11.65											0.001	0.0995	137.1			

ON=压缩机通电, OFF=压缩机断电, kon=化霜加热器通电, *off=化霜制热器断电
 (max=状态变化之间冷冻室最热点时刻, min=状态变化之间冷冻室最冷点时刻)
 (fmax=冷冻室最热点, fmin=冷冻室最冷点, d=化霜开始冷冻室最热点等于-18°C时刻)
 (t10, t11, t12最热点的平均值, t13, t14最冷点的平均值, t15, t16最冷点的再平均值)
 (toff=化霜开始冷冻室最热点时刻)
 (*max=化霜开始冷冻室最热点时刻)

制表时间:1998-12-19 14:13:37

NO:2
 试验内容:储藏温度
 直冷型冰箱
 机型:BD-168(R134a)
 型号:AE1350Y.66*2100 150
 方向:32/70%
 温控器位置:Ch值=1
 温度条件:

冷冻室:-21.9 °C 测温点数:8(t1, t2, t3, t4, t5, t6, t7, t8,)

10:1
 试验内容: 箱式温度
 直冷型冰箱
 机型号: BD-168(R134a)
 型号: K2130V, 60x2100-140
 方向: 32° 70%
 温控器位置: 直冷=5
 温度等级:

冷冻室: -21.9 °C 测温点数: 6 (t1, t2, t3, t4, t5, t6,)

格式 1 汇总表

状态	时间	t1	t2	t3	t4	t5	t6	t7	t8	t9	t10	t11	t12	t13	t14	t15	t16	电流 (A)	电能1 (kWh)	功率 (W)	系数 (%)	电能2 (kWh/24h)	Cn	ΔT 秒	
1998-12-18																									
ON	16:50:27	-21.12	-22.18	-22.57	-22.50	-22.01	-22.29											0.907	0.0604	107.4	39.49	1.5365	5	887	
OFF	17:5:14	-23.01	-24.06	-23.27	-23.23	-23.06	-24.01											0.900	0.0209	107.4			5	604	
ON	17:15:18	-21.14	-22.17	-22.57	-22.52	-22.04	-22.32											0.900	0.0272	107.0	58.65	1.5388	5	838	
OFF	17:23:16	-22.89	-23.90	-23.14	-23.12	-22.95	-23.79											0.900	0.0522	107.0			5	602	
ON	17:35:18	-21.05	-22.08	-22.45	-22.36	-21.92	-22.17											0.903	0.0526	107.9	58.47	1.5388	5	829	
OFF	17:53:7	-22.84	-23.84	-23.08	-23.06	-22.90	-23.79											0.913	0.0775	107.9			5	608	
ON	18:34:15	-21.05	-22.08	-22.45	-22.37	-21.91	-22.15											0.900	0.0779	107.2	58.43	1.5388	5	808	
OFF	18:17:8	-22.85	-23.85	-23.09	-23.09	-22.96	-23.84											0.908	0.1027	107.9			5	608	
ON	18:27:4	-21.13	-22.12	-22.51	-22.43	-21.98	-22.20											0.901	0.1031	107.9	58.23	1.5272	5	822	
OFF	18:40:55	-22.84	-23.85	-23.03	-23.05	-22.89	-23.60											0.911	0.1284	107.9			5	603	
ON	18:50:58	-21.04	-22.07	-22.43	-22.40	-21.95	-22.21											0.906	0.1580	107.9	58.23	1.5272	5	822	
OFF	19:4:40	-22.79	-23.81	-23.02	-22.93	-22.72	-23.60											0.906	0.1584	107.9			5	603	
ON	19:14:43	-20.85	-21.89	-22.25	-22.18	-21.73	-22.01											0.903	0.1781	107.9	58.21	1.5263	5	828	
OFF	19:28:31	-22.77	-23.83	-23.07	-23.09	-22.95	-23.86											0.909	0.1785	107.9			5	597	
ON	19:38:28	-20.92	-22.00	-22.36	-22.28	-21.83	-22.11											0.900	0.2029	107.9	58.12	1.5258	5	815	
OFF	19:52:13	-22.72	-23.74	-22.97	-22.94	-22.77	-23.68											0.908	0.2034	107.9			5	602	
ON	20:2:15	-20.81	-21.85	-22.19	-22.14	-21.68	-21.95											0.900	0.2277	107.9	58.00	1.5248	5	809	
OFF	20:15:34	-22.72	-23.78	-22.97	-22.96	-22.77	-23.63											0.915	0.2281	107.9			5	597	
ON	20:25:31	-21.02	-22.03	-22.40	-22.33	-21.90	-22.17											0.902	0.2523	107.8	58.00	1.5236	5	806	
OFF	20:38:57	-22.74	-23.78	-22.99	-22.98	-22.75	-23.63											0.912	0.2526	107.6			5	596	
ON	20:48:53	-21.02	-22.02	-22.40	-22.34	-21.90	-22.17											0.904	0.2774	107.6	57.95	1.5220	5	814	
OFF	21:2:27	-22.83	-23.86	-23.06	-22.96	-22.78	-23.72											0.901	0.3015	107.1			5	605	
ON	21:12:52	-21.02	-22.03	-22.39	-22.30	-21.86	-22.10											0.903	0.3019	107.1	57.87	1.5193	5	810	
OFF	21:26:23	-22.74	-23.75	-22.96	-22.97	-22.81	-23.72											0.901	0.3265	107.2			5	611	
ON	21:36:13	-20.91	-21.96	-22.34	-22.29	-21.83	-22.08											0.909	0.3269	107.2	57.81	1.5170	5	823	
OFF	21:49:58	-22.70	-23.77	-23.00	-22.98	-22.83	-23.74											0.909	0.3269	107.2			5	619	
ON	22:0:17	-20.88	-21.90	-22.26	-22.19	-21.72	-21.99											0.901	0.3514	107.0	57.75	1.5160	5	821	
OFF	22:13:58	-22.70	-23.72	-22.95	-22.92	-22.76	-23.69											0.913	0.3518	107.0			5	619	
ON	22:24:17	-20.88	-21.89	-22.31	-22.25	-21.78	-22.00											0.901	0.3768	107.5	57.71	1.5149	5	834	
OFF	22:38:11	-22.78	-23.82	-23.04	-23.02	-22.86	-23.70											0.908	0.3772	107.5			5	625	
ON	22:48:36	-20.86	-21.83	-22.31	-22.26	-21.78	-22.03											0.900	0.4018	107.1	57.69	1.5137	5	829	
OFF	23:2:25	-22.72	-23.77	-22.95	-22.94	-22.76	-23.67											0.907	0.4022	107.1			5	618	
ON	23:12:43	-20.85	-21.84	-22.25	-22.19	-21.74	-22.00											0.900	0.4267	107.2	57.66	1.5130	5	823	
OFF	23:26:26	-22.07	-23.64	-22.88	-22.88	-22.70	-23.57											0.912	0.4272	107.2			5	613	
ON	23:36:39	-20.87	-21.86	-22.24	-22.15	-21.71	-21.97											0.901	0.4517	107.5	57.66	1.5130	5	826	
OFF	23:50:19	-22.67	-23.63	-22.82	-22.89	-22.72	-23.57											0.913	0.4522	107.5			5	627	
ON	0:0:46	-20.83	-21.88	-22.27	-22.22	-21.72	-21.98											0.900	0.4770	107.0	57.61	1.5119	5	833	

5-10 min

1300-12-10

OFF	16:50:12	-25.28	-25.31	-25.33	-25.78	-25.44	-25.82	-25.38	0.000	0.0205	107.6	63.01	1.0487	5	617	
ON	17:06:25	-23.20	-23.03	-23.18	-23.04	-23.49	-22.95	-23.25	-23.04	0.000	0.0522	107.6	63.01	1.0487	5	1051
OFF	17:24:09	-24.39	-25.00	-25.05	-25.33	-25.11	-25.05	-25.51	-25.04	0.026	0.0526	108.0	63.02	1.0509	5	602
ON	17:34:2	-23.24	-23.12	-23.19	-23.10	-23.54	-23.01	-23.32	-23.13	0.001	0.0834	108.0	63.02	1.0509	5	1026
OFF	17:51:6	-25.08	-23.12	-25.10	-25.59	-25.15	-25.08	-25.52	-25.01	0.024	0.0838	108.1	62.85	1.0476	5	617
ON	18:1:25	-23.15	-22.90	-23.00	-22.97	-23.36	-22.78	-23.09	-22.79	0.003	0.1146	108.1	62.85	1.0476	5	1029
OFF	18:18:34	-24.90	-21.97	-25.01	-25.47	-25.05	-25.00	-25.51	-25.02	0.027	0.1151	108.0	62.80	1.0447	5	618
ON	18:28:52	-23.16	-23.00	-23.05	-22.82	-23.28	-22.70	-23.08	-22.84	0.003	0.1453	108.0	62.80	1.0447	5	1002
OFF	18:45:34	-24.69	-24.59	-24.56	-25.47	-25.06	-24.59	-25.48	-24.96	0.028	0.1457	108.0	62.42	1.0421	5	602
ON	18:55:36	-23.39	-23.24	-23.30	-23.20	-23.57	-23.03	-23.33	-23.10	0.003	0.1750	108.0	62.42	1.0421	5	969
OFF	19:11:45	-24.80	-24.82	-24.85	-25.35	-24.86	-25.31	-24.83	0.026	0.1755	108.0	62.42	1.0421	5	614	
ON	19:21:55	-22.85	-22.84	-22.92	-22.80	-23.22	-22.75	-23.05	-22.89	0.002	0.2047	108.8	62.24	1.0384	5	973
OFF	19:38:12	-24.71	-24.80	-24.77	-25.26	-24.82	-24.72	-25.24	-24.66	0.028	0.2051	108.3	62.18	1.0369	5	601
ON	19:48:13	-23.23	-23.10	-23.16	-23.05	-23.41	-22.87	-23.18	-22.94	0.000	0.2344	108.3	62.18	1.0369	5	973
OFF	20:4:20	-24.79	-24.88	-24.85	-25.33	-24.82	-24.83	-25.23	-24.76	0.029	0.2346	108.3	62.08	1.0359	5	597
ON	20:14:23	-23.12	-22.90	-23.05	-22.96	-23.30	-22.83	-23.08	-22.90	0.000	0.2655	108.0	62.08	1.0359	5	918
OFF	20:30:11	-24.00	-24.64	-24.60	-25.14	-24.75	-24.68	-25.18	-24.64	0.034	0.2659	108.0	62.08	1.0359	5	613
ON	20:40:24	-23.01	-22.87	-22.95	-22.88	-23.24	-22.71	-23.07	-22.82	0.001	0.2930	108.9	61.98	1.0337	5	964
OFF	20:56:28	-24.67	-24.73	-24.63	-25.13	-24.75	-24.64	-25.13	-24.61	0.028	0.2933	108.3	61.88	1.0309	5	606
ON	21:6:36	-23.00	-22.89	-22.95	-22.87	-23.25	-22.75	-23.10	-22.80	0.002	0.3219	108.3	61.88	1.0309	5	951
OFF	21:22:27	-24.59	-24.66	-24.68	-25.19	-24.72	-24.67	-25.13	-24.60	0.024	0.3223	108.6	61.81	1.0294	5	606
ON	21:32:33	-22.92	-22.85	-22.92	-22.83	-23.19	-22.68	-23.00	-22.74	0.001	0.3510	108.6	61.81	1.0294	5	949
OFF	21:48:22	-24.55	-24.57	-24.57	-25.15	-24.58	-24.63	-25.11	-24.50	0.026	0.3515	108.6	61.73	1.0279	5	612
ON	21:58:34	-22.92	-22.77	-22.84	-22.75	-23.11	-22.61	-22.90	-22.65	0.002	0.3801	108.6	61.73	1.0279	5	951
OFF	22:14:25	-24.60	-24.68	-24.66	-25.16	-24.70	-24.65	-25.12	-24.63	0.026	0.3805	108.6	61.66	1.0263	5	609
ON	22:24:34	-22.94	-22.79	-22.84	-22.75	-23.14	-22.64	-22.94	-22.70	0.002	0.4091	108.6	61.66	1.0263	5	947
OFF	22:40:21	-24.57	-24.64	-24.64	-25.12	-24.70	-24.60	-25.10	-24.62	0.028	0.4095	108.7	61.61	1.0252	5	598
ON	22:50:19	-23.01	-22.90	-22.97	-22.87	-23.27	-22.75	-23.04	-22.83	0.001	0.4575	108.7	61.61	1.0252	5	930
OFF	23:5:49	-24.60	-24.64	-24.65	-25.13	-24.67	-24.63	-25.10	-24.61	0.025	0.4600	108.7	61.54	1.0237	5	613
ON	23:16:2	-22.91	-22.78	-22.86	-22.76	-23.13	-22.61	-22.94	-22.71	0.002	0.4604	108.7	61.54	1.0237	5	911
OFF	23:31:43	-24.56	-24.63	-24.63	-25.13	-24.63	-24.62	-25.09	-24.59	0.023	0.4609	108.7	61.54	1.0237	5	614
ON	23:41:57	-22.87	-22.72	-22.79	-22.71	-23.10	-22.59	-22.86	-22.65	0.002	0.4953	108.7	61.46	1.0227	5	941
OFF	23:57:36	-24.53	-24.61	-24.61	-25.11	-24.63	-24.59	-25.00	-24.53	0.027	0.4957	108.1	61.45	1.0218	5	597
ON	0:7:35	-22.83	-22.86	-22.97	-22.88	-23.20	-22.74	-23.01	-22.77	0.002	0.5233	108.1	61.45	1.0218	5	930
OFF	0:23:10	-24.54	-24.60	-24.60	-25.10	-24.63	-24.58	-25.07	-24.56	0.026	0.5242	108.5	61.43	1.0211	5	592
ON	0:33:2	-23.02	-22.92	-22.98	-22.80	-23.25	-22.76	-23.07	-22.82	0.002	0.5526	108.5	61.43	1.0211	5	925
OFF	0:43:27	-24.50	-24.57	-24.61	-25.09	-24.67	-24.59	-25.06	-24.53	0.019	0.5526	108.0	61.40	1.0204	5	597
ON	0:58:24	-23.00	-22.85	-22.93	-22.87	-23.23	-22.74	-23.05	-22.80	0.002	0.5806	108.0	61.40	1.0204	5	931
OFF	1:13:53	-24.54	-24.62	-24.59	-25.12	-24.68	-24.59	-25.09	-24.57	0.026	0.6093	108.7	61.41	1.0200	5	594
ON	1:23:40	-23.01	-22.86	-22.93	-22.85	-23.19	-22.68	-23.01	-22.73	0.002	0.6097	108.5	61.37	1.0197	5	598
OFF	1:39:30	-24.61	-24.67	-24.66	-25.17	-24.72	-24.63	-25.12	-24.60	0.028	0.6375	108.5	61.37	1.0197	5	924
ON	1:49:28	-23.02	-22.90	-23.01	-22.89	-23.25	-22.76	-23.05	-22.84	0.002	0.6662	108.5	61.34	1.0188	5	608
OFF	2:4:52	-24.52	-24.59	-24.56	-25.05	-24.66	-24.59	-25.06	-24.56	0.029	0.6679	108.5	61.34	1.0188	5	940
ON	2:15:0	-22.93	-22.79	-22.83	-22.79	-23.14	-22.62	-22.98	-22.72	0.002	0.6950	108.0	61.30	1.0182	5	937
OFF	2:30:40	-24.49	-24.57	-24.58	-25.07	-24.63	-24.56	-25.03	-24.56	0.028	0.7234	108.0	61.27	1.0175	5	598
ON	2:40:54	-22.92	-22.72	-22.80	-22.72	-23.11	-22.59	-22.86	-22.63	0.002	0.7514	108.5	61.24	1.0166	5	931
OFF	2:50:31	-24.52	-24.59	-24.56	-25.06	-24.64	-24.55	-25.03	-24.57	0.025	0.7519	108.5	61.24	1.0166	5	600
ON	3:0:20	-22.88	-22.83	-22.90	-22.82	-23.17	-22.68	-22.97	-22.73	0.002	0.7797	108.4	61.22	1.0164	5	924
OFF	3:11:43	-24.45	-24.53	-24.52	-25.02	-24.56	-24.55	-24.93	-24.51	0.028	0.7862	108.4	61.22	1.0164	5	597
ON	3:31:52	-22.84	-22.72	-22.79	-22.69	-23.07	-22.55	-22.85	-22.62	0.002	0.8080	108.0	61.20	1.0160	5	921
OFF	3:47:23	-24.45	-24.53	-24.51	-25.03	-24.58	-24.51	-25.00	-24.46	0.022	0.8084	108.0	61.20	1.0160	5	597
ON	3:57:17	-22.83	-22.75	-22.85	-22.73	-23.13	-22.60	-22.90	-22.72	0.001	0.8361	108.4	61.18	1.0156	5	919
OFF	4:12:41	-24.47	-24.52	-24.53	-25.03	-24.61	-24.54	-25.02	-24.54	0.025	0.8646	108.0	61.18	1.0154	5	597
ON	4:22:38	-22.93	-22.80	-22.86	-22.78	-23.12	-22.61	-22.94	-22.70	0.003	0.8924	108.0	61.15	1.0147	5	921
OFF	4:37:53	-24.45	-24.53	-24.51	-25.02	-24.55	-24.52	-24.98	-24.45	0.021	0.9200	108.0	61.15	1.0147	5	597
ON	4:47:56	-22.90	-22.79	-22.84	-22.78	-23.12	-22.65	-22.93	-22.73	0.002	0.9481	108.4	61.13	1.0141	5	919
OFF	5:3:15	-24.48	-24.54	-24.53	-25.02	-24.61	-24.54	-25.04	-24.53	0.025	0.9766	108.0	61.13	1.0141	5	596
ON	5:13:11	-22.91	-22.79	-22.90	-22.80	-23.10	-22.64	-23.01	-22.78	0.002	1.0051	108.0	61.13	1.0141	5	937
OFF	5:28:48	-24.52	-24.60	-24.58	-25.07	-24.60	-24.57	-25.07	-24.53	0.023	1.0336	108.0	61.13	1.0141	5	596
ON	5:38:44	-22.95	-22.85	-22.92	-22.76	-23.10	-22.65	-22.94	-22.70	0.003	1.0621	108.0	61.13	1.0141	5	921
OFF	5:53:51	-24.45	-24.47	-24.43	-24.93	-24.40	-24.35	-24.45	-24.45	0.020	1.0906	108.0	61.12	1.0141	5	596
ON	6:3:51	-22.92	-22.83	-22.92	-22.82	-23.13	-22.69	-22.97	-22.80	0.002	1.1191	108.0	61.12	1.0141	5	938
OFF	6:12:53	-24.42	-24.50	-24.49	-24.94	-24.47	-24.43	-24.43	-24.43	0.020	1.1476	108.0	61.12	1.0141	5	596

室内: 抽成温度
 型号: AF1356V .66x2100 150
 向: 32.70%
 控制位置: On值=3
 温度: 21.5 °C (温度点: t1, t2, t3, t4, t5, t6, t7, t8, t9, t10, t11, t12, t13, t14, t15, t16, t17, t18, t19)

格式 1- 汇总表

状态	时间	t1	t2	t3	t4	t5	t6	t7	t8	t9	t10	t11	t12	t13	t14	t15	t16	电流 (A)	电耗1 (kWh)	功率 (W)	系数 (%)	电耗2 (kWh/24h)	ΔT 秒
OFF	1998-12-19 7:40:30	-21.90	-21.82	-21.93	-21.81	-22.25	-21.71	-21.93	-21.78									0.001	0.0037			0.0003	748
ON	7:53:41	-17.97	-17.84	-17.88	-17.82	-18.28	-17.68	-18.01	-17.81									0.974	0.0042	124.3	28.01	0.8758	291
OFF	8:3:53	-17.49	-17.46	-17.48	-17.50	-17.56	-17.35	-17.72	-17.50									0.001	0.0142	124.3	28.01	0.8758	560
ON	8:13:21	-17.23	-17.16	-17.25	-17.24	-17.42	-17.03	-17.31	-17.12									0.984	0.0147	126.6	31.03	0.9953	317
OFF	8:18:38	-17.01	-17.02	-17.02	-17.04	-17.04	-16.95	-17.32	-17.02									0.982	0.0263			0.9953	544
ON	8:27:42	-17.04	-16.94	-16.97	-16.99	-17.13	-16.82	-17.06	-16.88									0.993	0.0376	123.9	38.41	1.0504	324
OFF	8:33:0	-16.90	-16.87	-16.89	-17.32	-17.01	-16.85	-17.24	-16.92									0.992	0.0381			1.0504	335
ON	8:41:59	-16.89	-16.82	-16.87	-16.94	-17.00	-16.75	-17.02	-16.82									0.992	0.0457	127.5	34.51	1.0883	328
OFF	8:47:27	-16.84	-16.82	-16.81	-17.29	-16.88	-16.74	-17.16	-16.80									0.982	0.0501			1.0883	329
ON	8:56:16	-16.93	-16.84	-16.90	-16.91	-17.03	-16.72	-16.99	-16.76									0.992	0.0619	127.7	35.28	1.1193	332
OFF	9:1:46	-16.80	-16.83	-16.84	-17.29	-16.94	-16.78	-17.18	-16.80									0.983	0.0623			1.1334	325
ON	9:10:33	-16.97	-16.89	-16.93	-16.97	-17.12	-16.81	-17.08	-16.88									0.983	0.0742	126.6	35.91	1.1334	322
OFF	9:16:11	-16.80	-16.84	-16.85	-17.32	-16.83	-16.82	-17.22	-16.80									0.980	0.0746			1.1334	322
ON	9:24:53	-16.75	-16.75	-16.75	-16.85	-16.88	-16.71	-16.85	-16.80									0.983	0.0803	126.8	36.33	1.1483	329
OFF	9:30:32	-16.74	-16.72	-16.72	-17.21	-16.84	-16.74	-17.16	-16.80									0.984	0.0876			1.1483	327
ON	9:39:19	-16.79	-16.76	-16.75	-16.89	-16.90	-16.63	-16.88	-16.88									0.991	0.0980	126.7	36.72	1.1694	330
OFF	9:44:58	-16.77	-16.79	-16.79	-17.24	-16.85	-16.83	-17.19	-16.78									0.985	0.0984			1.1694	322
ON	9:53:41	-16.85	-16.76	-16.79	-16.84	-16.92	-16.64	-16.89	-16.71									0.993	0.1114	127.6	37.90	1.1692	359
OFF	9:59:20	-16.88	-17.01	-16.79	-17.26	-17.07	-16.73	-17.13	-16.81									0.987	0.1119			1.1692	328
ON	10:8:37	-16.83	-16.74	-16.80	-16.84	-16.93	-16.69	-16.95	-16.72									0.992	0.1239	127.6	37.24	1.1763	340
OFF	10:13:43	-16.76	-16.79	-16.80	-17.23	-16.81	-16.73	-17.18	-16.84									0.985	0.1244			1.1763	327
ON	10:22:30	-16.81	-16.76	-16.81	-16.87	-17.04	-16.76	-17.00	-16.81									0.992	0.1358	126.9	37.31	1.1793	324
OFF	10:27:54	-16.83	-16.87	-16.76	-17.11	-16.75	-16.65	-17.01	-16.89									0.985	0.1363			1.1793	322
ON	10:30:40	-16.82	-16.73	-16.81	-16.86	-16.96	-16.69	-16.91	-16.75									0.993	0.1462	127.8	37.11	1.1811	334
OFF	10:42:20	-16.83	-16.82	-16.84	-17.25	-16.90	-16.76	-17.12	-16.73									0.993	0.1486			1.1811	322
ON	10:51:27	-16.81	-16.75	-16.81	-16.85	-16.98	-16.71	-16.90	-16.78									0.989	0.1600	127.8	37.55	1.1891	330
OFF	10:56:41	-16.75	-16.77	-16.76	-17.24	-16.88	-16.75	-17.16	-16.82									0.993	0.1600			1.1891	322
ON	11:5:23	-16.83	-16.74	-16.81	-16.85	-16.95	-16.68	-16.92	-16.70									0.984	0.1611	127.3	37.70	1.1891	341
OFF	11:11:4	-16.83	-16.85	-16.83	-17.50	-16.88	-16.75	-17.15	-16.77									0.988	0.1736			1.1891	317
ON	11:19:41	-16.83	-16.76	-16.81	-16.84	-16.94	-16.87	-16.87	-16.80									0.980	0.1832	127.6	37.78	1.1891	317
OFF	11:25:19	-16.73	-16.69	-16.67	-17.10	-16.81	-16.63	-17.03	-16.81														317

(ON=压缩机通电, OFF=压缩机断电, tON=压缩机通电, tOFF=压缩机断电, tON=tOFF=压缩机通电/断电时间)
 (MAX=状态变化之最大值, MIN=状态变化之最小值, tMAX=tMIN=状态变化之最大值/最小值)
 (FMAX=冷冻室最高温度, FMIN=冷冻室最低温度, tFMAX=tFMIN=冷冻室最高/最低温度)
 (tON=tOFF=tON=tOFF=冷冻室最高/最低温度, tON=tOFF=冷冻室最高/最低温度)
 (tON=tOFF=tON=tOFF=冷冻室最高/最低温度, tON=tOFF=冷冻室最高/最低温度)
 (MAX=压缩机开始冷冻室最高温度, MIN=压缩机开始冷冻室最低温度, tMAX=tMIN=压缩机开始冷冻室最高/最低温度)

1998-12-19 8:33:19 (FMAX)=-16.63 °C
 1998-12-19 7:46:36 (FMIN)=-22.25 °C
 1998-12-19 7:46:36 (tON)=88.80 °C
 1998-12-19 7:46:36 (tOFF)=88.80 °C
 电流=0.932 (A)
 耗电量=1.1803 (kWh/24h)

制表时间: 1998-12-19 11:30:59

格式 1 记录统计列表

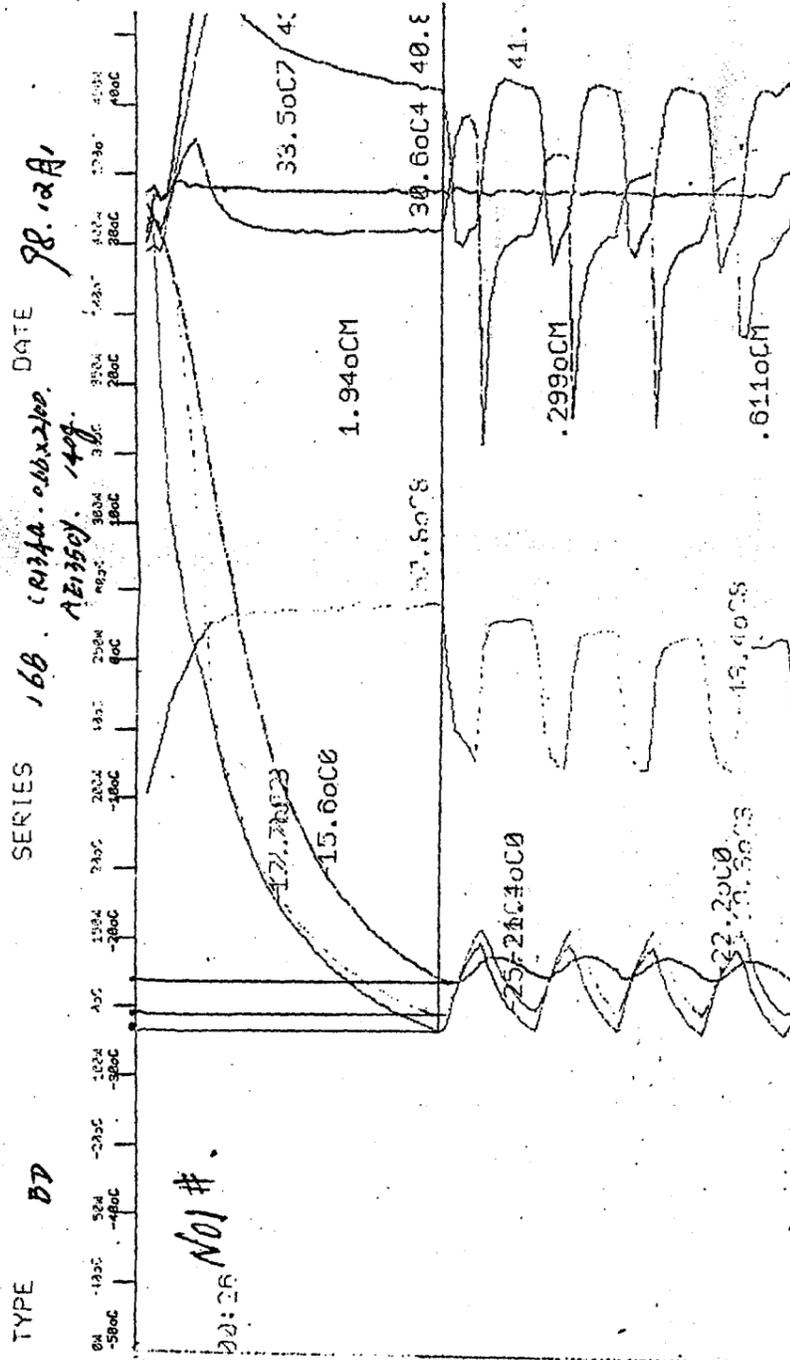
状态	时间	t1	t2	t3	t4	t5	t6	t7	t8	t9	t10	t11	t12	t13	t14	t15	t16	电流 (A)	电能1 (kWh)	功率 (W)	系数 (%)	电能2 (kWh/24h)	ΔT 秒
ON	11:42:33	-14.02	-13.93	-13.89	-13.73	-14.17	-13.65	-13.93	-13.79									1.028	0.0005				242
OFF	11:46:41	-13.03	-13.02	-13.03	-13.88	-13.50	-13.44	-13.82	-13.62									0.603	0.0096	133.7	31.27	1.0701	532
ON	11:53:33	-13.54	-13.50	-13.54	-13.61	-13.74	-13.40	-13.70	-13.53									1.015	0.0101				226
OFF	11:59:21	-13.42	-13.44	-13.47	-13.75	-13.64	-13.42	-13.78	-13.51									0.601	0.0188	137.8	30.76	1.0632	323
ON	12:08:00	-13.02	-13.55	-13.57	-13.65	-13.72	-13.47	-13.67	-13.50									0.002	0.0193				233
OFF	12:11:58	-13.42	-13.41	-13.43	-13.75	-13.52	-13.33	-13.71	-13.40									1.013	0.0285	136.8	30.90	1.0600	515
ON	12:20:34	-13.60	-13.53	-13.58	-13.67	-13.75	-13.48	-13.74	-13.56									0.000	0.0375	135.0			239
OFF	12:24:33	-13.35	-13.30	-13.35	-13.67	-13.47	-13.20	-13.63	-13.35									1.017	0.0380	135.8	31.13	1.0707	512
ON	12:33:50	-13.59	-13.50	-13.63	-13.68	-13.75	-13.52	-13.75	-13.58									0.600	0.0465	135.8			230
OFF	12:37:11	-13.32	-13.30	-13.38	-13.70	-13.47	-13.27	-13.62	-13.34									1.021	0.0474		31.23	1.0733	508
ON	12:45:29	-13.32	-13.48	-13.52	-13.60	-13.68	-13.42	-13.68	-13.46									0.601	0.0503	138.0			232
OFF	12:49:21	-13.27	-13.28	-13.29	-13.62	-13.40	-13.23	-13.63	-13.35									1.021	0.0567		31.24	1.0775	511
ON	12:57:52	-13.49	-13.41	-13.47	-13.55	-13.62	-13.38	-13.62	-13.46									0.004	0.0658	137.8			237
OFF	13:14:49	-13.35	-13.35	-13.37	-13.68	-13.50	-13.28	-13.63	-13.37									1.013	0.0662		31.30	1.0801	512
ON	13:10:21	-13.61	-13.55	-13.58	-13.73	-13.43	-13.43	-13.71	-13.53									0.003	0.0754	130.1			243
OFF	13:14:24	-13.26	-13.32	-13.32	-13.65	-13.49	-13.26	-13.65	-13.40									1.018	0.0760		31.33	1.0813	516
ON	13:23:00	-13.49	-13.42	-13.46	-13.60	-13.61	-13.33	-13.58	-13.41									0.000	0.0850	136.3			238
OFF	13:26:58	-13.30	-13.30	-13.32	-13.64	-13.44	-13.20	-13.55	-13.20									1.021	0.0850		31.41	1.0856	510
ON	13:35:34	-13.50	-13.45	-13.45	-13.63	-13.63	-13.40	-13.60	-13.42									0.600	0.0940	137.5			235
OFF	13:39:29	-13.27	-13.26	-13.27	-13.60	-13.38	-13.15	-13.47	-13.18									1.022	0.0932		31.40	1.0878	513
ON	13:48:44	-13.50	-13.46	-13.51	-13.60	-13.63	-13.40	-13.64	-13.47									0.600	0.1041	137.2			235
OFF	13:51:58	-13.26	-13.25	-13.26	-13.60	-13.35	-13.14	-13.49	-13.20									1.028	0.1047		31.41	1.0888	511
ON	14:00:30	-13.45	-13.32	-13.36	-13.45	-13.51	-13.30	-13.54	-13.38									0.003	0.1137	136.8			238
OFF	14:04:28	-13.27	-13.27	-13.28	-13.60	-13.40	-13.19	-13.55	-13.20									1.020	0.1143		31.44	1.0903	511
ON	14:12:33	-13.47	-13.39	-13.45	-13.51	-13.58	-13.35	-13.57	-13.41														

(ON=压缩机运行, OFF=压缩机停止, *OFF=化霜加热器运行, *OFF=化霜加热器停止)
 (max=冷态最高温度, min=冷态最低温度, *max=冷态最高温度, *min=冷态最低温度)
 (Fmax=冷态最高温度, Fmin=冷态最低温度, *Fmax=冷态最高温度, *Fmin=冷态最低温度)
 (tmax=冷态最高温度, tmin=冷态最低温度, *tmax=冷态最高温度, *tmin=冷态最低温度)
 (tmax=冷态最高温度, tmin=冷态最低温度, *tmax=冷态最高温度, *tmin=冷态最低温度)
 (tmax=冷态最高温度, tmin=冷态最低温度, *tmax=冷态最高温度, *tmin=冷态最低温度)
 (tmax=冷态最高温度, tmin=冷态最低温度, *tmax=冷态最高温度, *tmin=冷态最低温度)

制表时间: 1988-12-13 14:13:37

1978-12-18

1986.12.16 14:41:58
 31.42 31.33 31.07 31.06 31.17 31.40 31.46
 -22.24 -22.15 -22.20 -22.59 -22.07 -22.25 -22.61 -22.00
 时间=65.92 分钟
 测试时间:符合要求
 结果=合格



T₀ — 箱内温度: Temp inside the Cabinet. T₀ — 排气管温度: Temp of Discharge tube
 T₁ — 冷媒出口温度: Temp outlet the Cond. } get data on the panel.
 T₂ — 吸气入口: Temp inlet the comp.
 T₃ — 感温探头温度: Temp of the bulb
 T₄ — 回气管温度: Temp. of the Suction tube
 T₇ — 环境: Temp of the Ambient.
 T₆ — 压缩机: Temp of the Comp. shell.

NO:1
 试验内容:冷却速度 pull down.
 直冷型冰箱
 机型号:50-106(R134a)
 型号:AE1350Y.60*2100 140
 厂向:32°70'
 温控器位置:0值=5
 测试时间:30分钟

温度条件:

冷感室:-21.0 °C 测温点数:6(t1, t2, t3, t4, t5, t6,)

开始	t1	t2	t3	t4	t5	t6	t7	t8	t9	t10	t11	t12	t13	t14	t15	t16
1938.12.18 13:35:15	31.91	31.11	31.03	31.38	31.34	31.43										
结束	1938.12.18 14:43:53															

时间=30.68 分钟
 测试时间:符合要求

结果=合格

NO:2
 试验内容:冷却速度
 直冷型冰箱
 机型号:50-106(R134a)
 型号:AE1350Y.60*2100 150
 厂向:32°70'
 温控器位置:0值=5
 测试时间:30分钟

温度条件:

冷感室:-21.0 °C 测温点数:6(t1, t2, t3, t4, t5, t6, t7, t8,)

开始	t1	t2	t3	t4	t5	t6	t7	t8	t9	t10	t11	t12	t13	t14	t15	t16
1938.12.18 13:41:38	31.42	31.38	31.37	31.06	31.36	31.17	31.46	31.36								
结束	1938.12.18 14:47:33															

时间=66.32 分钟
 测试时间:符合要求

结果=合格

GRAPH

NO.11
 试验内容: 瞬态温度
 直接程序器
 机型: 50-100 (R134a)
 型号: AE1330T, .60x2100 (140)
 厂商: 32703
 温控器位置: Ch值=3
 温度条件:

*With package and
 "m" package of 6.*

冷冻室: -21.9 °C 测温点数: 6 (t1, t2, t3, t4, t5, t6)

格式 1 汇总表

状态	时间	t1	t2	t3	t4	t5	t6	t7	t8	t9	t10	t11	t12	t13	t14	t15	t16	电流 (A)	电能1 (KWh)	功率 (W)	系数 (%)	电能2 (KWh/24h)	Cn	ΔT 秒	
1998-12-21																									
ON	16:42:47	-19.71	-22.31	-22.18	-18.41	-18.62	-19.22											0.917	0.0005	106.2	61.71	1.5929	5	1204	
OFF	17:2:51	-19.80	-22.30	-22.20	-18.45	-18.65	-19.26											0.601	0.0361	106.2			5	747	
ON	17:15:18	-19.74	-22.32	-22.19	-18.41	-18.62	-19.21											0.907	0.0365	106.5			5	988	
OFF	17:31:40	-19.80	-22.31	-22.20	-18.45	-18.66	-19.28											0.001	0.0658	106.5			5	1166	
ON	17:31:12	-19.72	-22.30	-22.20	-18.41	-18.62	-19.20											0.927	0.0663	107.5			5	1086	
OFF	18:9:18	-19.78	-22.27	-22.21	-18.44	-18.65	-19.28											0.002	0.0988	107.5			5	731	
ON	18:21:29	-19.81	-22.38	-22.28	-18.48	-18.70	-19.29											0.908	0.0991	107.1			5	1000	
OFF	18:35:9	-19.80	-22.29	-22.20	-18.41	-18.61	-19.22											0.000	0.1289	107.1			5	865	
ON	18:32:34	-19.73	-22.30	-22.22	-18.44	-18.65	-19.25											0.920	0.1293	107.5			5	1012	
OFF	19:3:26	-19.77	-22.25	-22.15	-18.37	-18.59	-19.21											0.000	0.1596	107.5			5	752	
ON	19:21:58	-19.73	-22.31	-22.20	-18.42	-18.64	-19.22											0.914	0.1600	107.3			5	999	
OFF	19:38:37	-19.71	-22.24	-22.17	-18.43	-18.62	-19.19											0.000	0.1898	107.3			5	979	
ON	19:34:56	-19.74	-22.37	-22.27	-18.51	-18.76	-19.36											0.922	0.1903	107.5			5	1010	
OFF	20:11:46	-19.80	-22.30	-22.23	-18.45	-18.69	-19.28											0.002	0.2205	107.5			5	748	
ON	20:24:14	-19.75	-22.33	-22.23	-18.46	-18.70	-19.29											0.914	0.2210	106.9			5	1058	
OFF	20:41:52	-19.79	-22.28	-22.18	-18.42	-18.85	-19.43											0.000	0.2525	106.9			5	883	
ON	20:50:35	-19.75	-22.35	-22.23	-18.48	-18.72	-19.31											0.920	0.2530	107.7			5	1013	
OFF	21:13:28	-19.79	-22.30	-22.20	-18.46	-18.69	-19.29											0.000	0.2833	107.7			5	759	
ON	21:26:7	-19.67	-22.23	-22.13	-18.40	-18.69	-19.33											0.922	0.2837	107.1			5	947	
OFF	21:41:54	-19.82	-22.34	-22.25	-18.51	-18.76	-19.30											0.002	0.3119	107.1			5	1081	
ON	21:59:55	-19.73	-22.32	-22.21	-18.46	-18.69	-19.27											0.920	0.3122	107.5			5	1059	
OFF	22:17:34	-19.79	-22.28	-22.23	-18.46	-18.70	-19.29											0.000	0.3439	107.5			5	739	
ON	22:29:53	-19.72	-22.30	-22.19	-18.43	-18.67	-19.24											0.907	0.3443	107.1			5	953	
OFF	22:45:46	-19.74	-22.29	-22.22	-18.45	-18.70	-19.32											0.000	0.3727	107.1			5	850	
ON	22:53:58	-19.75	-22.33	-22.22	-18.46	-18.69	-19.26											0.915	0.3731	107.2			5	983	
OFF	23:10:19	-19.80	-22.30	-22.23	-18.51	-18.71	-19.33											0.001	0.4024	107.2			5	759	
ON	23:23:58	-19.68	-22.33	-22.15	-18.38	-18.62	-19.24											0.912	0.4029	106.9			5	959	
OFF	23:44:57	-19.79	-22.31	-22.21	-18.48	-18.71	-19.32											0.000	0.4315	106.9			5	800	
ON	23:59:23	-19.73	-22.35	-22.24	-18.50	-18.73	-19.30											0.911	0.4319	107.0			5	1038	
1998-12-22																									
OFF	0:10:41	-19.78	-22.27	-22.18	-18.45	-18.70	-19.29											0.002	0.4628	107.0			5	728	
ON	0:28:49	-19.77	-22.38	-22.24	-18.49	-18.69	-19.28											0.910	0.4631	106.9			5	934	
OFF	0:44:23	-19.81	-22.33	-22.21	-18.50	-18.74	-19.32											0.001	0.4909	106.9			5	850	
ON	0:53:59	-19.75	-22.30	-22.24	-18.51	-18.75	-19.33											0.914	0.4913	106.9			5	993	
OFF	1:13:12	-19.72	-22.26	-22.19	-18.48	-18.76	-19.34											0.002	0.5209	106.9			5	749	
ON	1:27:41	-19.82	-22.35	-22.22	-18.47	-18.77	-19.32											0.906	0.5212	107.0			5	1038	

OFF	2:18:27	-19.77	-22.26	-22.20	-18.41	-18.69	-19.28	0.000	0.5818	107.0	54.61	1.4255	5	1018
ON	2:30:32	-19.75	-22.34	-22.23	-18.45	-18.74	-19.32	0.908	0.5824					725
OFF	2:47:50	-19.82	-22.29	-22.16	-18.39	-18.68	-19.26	0.000	0.6131	106.6				1038
ON	3:2:28	-19.77	-22.36	-22.22	-18.42	-18.70	-19.27	0.515	0.6137					678
OFF	3:19:22	-19.79	-22.31	-22.21	-18.41	-18.71	-19.29	0.001	0.6433	106.3				1014
ON	3:31:56	-19.74	-22.35	-22.22	-18.42	-18.72	-19.28	0.907	0.6442					754
OFF	3:48:13	-19.80	-22.34	-22.24	-18.45	-18.74	-19.31	0.001	0.6730	107.1				967
ON	4:2:28	-19.77	-22.38	-22.24	-18.44	-18.74	-19.30	0.913	0.6734					865
OFF	4:18:53	-19.74	-22.23	-22.19	-18.39	-18.71	-19.28	0.002	0.7028	107.0				985
ON	4:32:14	-19.77	-22.33	-22.21	-18.43	-18.72	-19.30	0.911	0.7031					791
OFF	4:48:17	-19.78	-22.29	-22.17	-18.38	-18.69	-19.28	0.000	0.7321	107.0				973
ON	5:2:37	-19.79	-22.39	-22.28	-18.46	-18.73	-19.31	0.910	0.7324					860
OFF	5:18:52	-19.75	-22.35	-22.19	-18.39	-18.72	-19.28	0.002	0.7616	107.1				975
ON	5:32:15	-19.75	-22.30	-22.17	-18.38	-18.66	-19.21	0.907	0.7619					753
OFF	5:48:17	-19.81	-22.33	-22.22	-18.44	-18.74	-19.31	0.009	0.7905	106.8				962
ON	6:2:11	-19.75	-22.37	-22.27	-18.44	-18.72	-19.33	0.910	0.7910					844
OFF	6:18:24	-19.83	-22.35	-22.25	-18.47	-18.76	-19.35	0.009	0.8200	107.0				973
ON	6:32:30	-19.78	-22.33	-22.22	-18.44	-18.73	-19.31	0.909	0.8204					846
OFF	6:48:35	-19.78	-22.29	-22.20	-18.42	-18.73	-19.33	0.000	0.8491	106.8				905
ON	7:1:51	-19.75	-22.32	-22.20	-18.42	-18.69	-19.24	0.908	0.8496					790
OFF	7:17:57	-19.82	-22.35	-22.21	-18.41	-18.75	-19.29	0.002	0.8784	107.1				966
ON	7:32:11	-19.68	-22.27	-22.14	-18.38	-18.70	-19.31	0.917	0.8788					854
OFF	7:47:32	-19.80	-22.31	-22.22	-18.43	-18.73	-19.30	0.002	0.9060	107.0				927

(ON=压缩机通电, OFF=压缩机断电, *on=化霜加热器通电, *off=化霜加热器断电)
 (max=状态变化之间冷冻室最热点时刻, min=状态变化之间冷冻室最冷点时刻)
 (Fmax=冷冻室最热点, Fmin=冷冻室最冷点, d=化霜开始冷冻室最热点等于-18℃时刻)
 (ton=冷冻室t10, t11, t12最热点的平均值, tm=ton值与上一状态平均值的再平均值)
 (toff=冷冻室t10, t11, t12最冷点的平均值, toff=toff值与上一状态平均值的再平均值)
 (tm)=88.80 ℃ (toff)=88.80 ℃ (toff)=88.80 ℃
 (*max=化霜开始冷冻室最热点时刻)

制表时间: 1998-12-22 7:43:28

试验内容: 储藏温度
 直冷型冰箱
 机型: BD-168(A134a)
 型号: AE1350Y .66*2100 (150)
 厂商: 82/70%
 温控器位置: On值=5
 温度条件:

冷冻室: -21.9 ℃ 测温点数: 8 (t1, t2, t3, t4, t5, t6, t7, t8,)

格式 1 汇总表

状态	时间	t1	t2	t3	t4	t5	t6	t7	t8	t9	t10	t11	t12	t13	t14	t15	t16	电流 (A)	电能1 (kWh)	功率 (%)	系数 (%)	电能2 (kWh/24h)	ΔT 秒	
OFF	7:48:46	-20.43	-20.32	-16.99	-24.26	-22.52	-22.53	-21.98	-22.14									0.001	0.0086					
ON	8:11:52	-20.10	-20.17	-16.85	-25.77	-22.45	-22.48	-21.93	-22.11									0.933	0.0092					1386
OFF	8:33:50	-20.42	-20.27	-16.96	-24.22	-22.58	-22.61	-22.04	-22.25									0.003	0.0584	105.8	54.77	1.4029		1678
ON	9:1:42	-20.19	-20.23	-16.92	-23.84	-22.56	-22.58	-21.98	-22.16									0.936	0.0588					1312
OFF	9:33:35	-20.40	-20.20	-16.94	-24.14	-22.52	-22.55	-21.96	-22.18									0.002	0.1147	105.3	57.10	1.4574		1913
ON	9:55:28	-20.23	-20.29	-16.98	-23.84	-22.58	-22.57	-21.96	-22.13									0.952	0.1151					1313
OFF	10:25:56	-20.41	-20.28	-17.00	-24.16	-22.54	-22.55	-21.94	-22.15									0.003	0.1687	105.5	57.47	1.4601		1828
ON	10:47:42	-20.17	-20.23	-16.95	-23.81	-22.56	-22.53	-21.90	-22.07									0.938	0.1691					1306
OFF	11:17:10	-20.40	-20.28	-16.94	-24.10	-22.53	-22.50	-21.87	-22.10									0.001	0.2208	105.4	57.48	1.4601		1763
ON	11:38:30	-20.13	-20.23	-16.92	-23.60	-22.65	-22.63	-21.99	-22.17									0.932	0.2213					1260

ON	12:31:35	-20.20	-20.27	-15.97	-23.77	-22.59	-22.57	-21.94	-22.14	0.929	0.2763	57.91	1.4773	5	1501
OFF	13:11:42	-20.43	-20.32	-17.03	-24.12	-22.58	-22.56	-21.92	-22.10	0.003	0.3297	105.5	1.4773	5	1504
ON	13:23:15	-20.25	-20.32	-17.05	-23.82	-22.64	-22.60	-21.91	-22.10	0.924	0.3302	53.02	1.4731	5	1293
OFF	13:53:42	-20.43	-20.35	-17.16	-24.18	-22.59	-22.69	-22.01	-22.27	0.003	0.3635	105.1	1.4731	5	1627
ON	14:15:11	-20.19	-20.26	-17.01	-23.71	-22.56	-22.54	-21.89	-22.09	0.929	0.3639	56.25	1.4644	5	1289
OFF	14:47:9	-20.44	-20.39	-17.15	-24.17	-22.64	-22.59	-21.93	-22.12	0.000	0.4399	105.3	1.4644	5	1918
ON	15:08:50	-20.21	-20.29	-17.05	-23.73	-22.57	-22.55	-21.90	-22.09	0.925	0.4405	58.23	1.4643	5	1301
OFF	15:38:53	-20.45	-20.37	-17.11	-24.12	-22.62	-22.59	-21.91	-22.14	0.001	0.4932	105.4	1.4643	5	1803
ON	16:09:37	-20.28	-20.35	-17.10	-23.80	-22.67	-22.63	-21.91	-22.13	0.938	0.4937	55.26	1.5677	5	1304
OFF	16:41:1	-20.52	-20.50	-17.15	-24.22	-22.61	-22.61	-22.09	-22.23	0.002	0.5601	104.4	1.5677	5	2604
ON	17:12:21	-20.26	-20.31	-17.10	-23.82	-22.61	-22.61	-21.94	-22.13	0.925	0.5636	55.81	1.4565	5	1400
OFF	17:44:56	-20.43	-20.40	-17.15	-24.16	-22.65	-22.65	-21.95	-22.21	0.003	0.6175	105.5	1.4565	5	1649
ON	17:53:14	-20.20	-20.32	-17.11	-23.82	-22.67	-22.64	-21.90	-22.10	0.938	0.6175	58.16	1.4565	5	1342
OFF	18:24:5	-20.46	-20.31	-17.15	-24.12	-22.67	-22.65	-21.95	-22.15	0.002	0.6639	105.2	1.4565	5	1614
ON	18:55:45	-20.28	-20.28	-17.03	-23.69	-22.69	-22.59	-21.89	-22.12	0.932	0.6663	58.33	1.4867	5	1300
OFF	19:13:46	-20.43	-20.33	-17.23	-24.21	-22.78	-22.70	-22.02	-22.25	0.001	0.7138	106.4	1.4867	5	1677
ON	19:53:17	-20.20	-20.24	-17.05	-23.77	-22.74	-22.69	-21.89	-22.06	0.949	0.7162	58.93	1.4829	5	1294
OFF	20:11:55	-20.43	-20.29	-17.14	-24.06	-22.66	-22.62	-21.87	-22.10	0.002	0.7637	106.9	1.4829	5	1598
ON	20:22:53	-20.35	-20.26	-17.10	-23.71	-22.67	-22.63	-21.90	-22.11	0.949	0.7641	58.06	1.4820	5	1258
OFF	20:50:43	-20.49	-20.37	-17.24	-24.16	-22.75	-22.70	-22.02	-22.28	0.005	0.8134	106.4	1.4820	5	1670
ON	21:11:36	-20.18	-20.27	-17.13	-23.74	-22.73	-22.70	-21.97	-22.20	0.947	0.8138	57.97	1.4607	5	1253
OFF	21:36:41	-20.40	-20.29	-17.14	-24.07	-22.70	-22.66	-21.91	-22.16	0.005	0.8620	106.8	1.4607	5	1628
ON	21:53:26	-20.21	-20.27	-17.07	-23.71	-22.69	-22.64	-21.89	-22.10	0.940	0.8625	58.02	1.4820	5	1244
OFF	22:23:7	-20.44	-20.34	-17.11	-24.03	-22.69	-22.65	-21.90	-22.15	0.002	0.9147	105.6	1.4820	5	1779
ON	22:49:54	-20.32	-20.40	-17.18	-23.83	-22.78	-22.74	-21.98	-22.21	0.943	0.9151	57.99	1.4815	5	1247
OFF	23:17:56	-20.45	-20.32	-17.11	-24.05	-22.68	-22.62	-21.88	-22.11	0.002	0.9646	105.9	1.4815	5	1682
ON	23:38:49	-20.24	-20.32	-17.10	-23.74	-22.69	-22.63	-21.85	-22.03	0.932	0.9650	58.00	1.4798	5	1253
OFF	0:5:1	-20.45	-20.36	-17.17	-24.11	-22.73	-22.70	-21.95	-22.19	0.004	1.0163	105.8	1.4820	5	1752
ON	0:28:56	-20.22	-20.33	-17.16	-23.78	-22.78	-22.71	-21.99	-22.20	0.937	1.0169	57.98	1.4802	5	1257
OFF	0:58:8	-20.45	-20.37	-17.18	-24.09	-22.71	-22.63	-21.85	-22.11	0.004	1.0647	105.7	1.4802	5	1630
ON	1:17:6	-20.23	-20.32	-17.09	-23.67	-22.62	-22.59	-21.83	-22.02	0.926	1.0653	57.80	1.4798	5	1258
OFF	1:45:7	-20.41	-20.34	-17.17	-24.06	-22.72	-22.72	-21.93	-22.19	0.003	1.1147	105.9	1.4798	5	1681
ON	2:6:10	-20.20	-20.30	-17.12	-23.70	-22.70	-22.66	-21.89	-22.11	0.937	1.1153	57.83	1.4785	5	1269
OFF	2:33:41	-20.38	-20.29	-17.13	-24.02	-22.66	-22.63	-21.88	-22.12	0.000	1.1636	105.9	1.4785	5	1645
ON	2:54:29	-20.20	-20.31	-17.16	-23.77	-22.70	-22.70	-21.94	-22.17	0.942	1.1640	57.83	1.4785	5	1248
OFF	3:22:55	-20.40	-20.31	-17.09	-24.04	-22.68	-22.64	-21.88	-22.14	0.004	1.2142	105.9	1.4785	5	1706
ON	3:44:2	-20.21	-20.26	-16.83	-23.62	-22.59	-22.56	-21.84	-22.07	0.939	1.2147	57.80	1.4792	5	1267
OFF	4:13:46	-20.40	-20.30	-16.77	-24.02	-22.63	-22.59	-21.84	-22.08	0.000	1.2670	105.5	1.4792	5	1784
ON	4:34:26	-20.17	-20.26	-16.68	-23.66	-22.63	-22.59	-21.86	-22.07	0.924	1.2674	57.81	1.4781	5	1240
OFF	5:1:27	-20.35	-20.28	-16.79	-24.06	-22.71	-22.64	-21.90	-22.17	0.002	1.3150	105.8	1.4781	5	1621
ON	5:22:12	-20.14	-20.22	-16.75	-23.64	-22.61	-22.58	-21.83	-22.05	0.946	1.3155	57.80	1.4780	5	1245
OFF	5:50:22	-20.40	-20.36	-16.95	-24.11	-22.74	-22.69	-21.94	-22.21	0.004	1.3651	105.9	1.4780	5	1690
ON	6:11:4	-20.19	-20.30	-16.89	-23.68	-22.66	-22.64	-21.93	-22.15	0.943	1.3656	57.77	1.4774	5	1242
OFF	6:38:25	-20.38	-20.26	-16.92	-23.96	-22.60	-22.59	-21.87	-22.13	0.001	1.4139	106.0	1.4774	5	1641
ON	6:59:20	-20.09	-20.17	-16.89	-23.62	-22.61	-22.56	-21.83	-22.04	0.949	1.4143	57.75	1.4768	5	1255
OFF	7:27:10	-20.37	-20.27	-17.01	-24.02	-22.65	-22.67	-21.92	-22.17	0.002	1.4633	105.8	1.4768	5	1670
ON	7:48:1	-20.21	-20.29	-17.00	-23.70	-22.70	-22.64	-21.88	-22.09	0.936	1.4638	57.80	1.4768	5	1251

(ON=压缩机通电,OFF=压缩机断电,*ON=化霜加热器通电,*OFF=化霜加热器断电)
 (max=状态变化之间冷冻室最热点时刻,min=状态变化之间冷冻室最冷点时刻)
 (Fmax=冷冻室最热点,Fmin=冷冻室最冷点,d=化霜开始冷冻室最热点等于-18℃时刻)
 (ton=化霜室t10,t11,t12最热点的平均值,tm=ton值与上一状态平均值的再平均值)
 (toff=化霜室t10,t11,t12最冷点的平均值,tn=toff值与上一状态平均值的再平均值)
 (*max=化霜开始冷冻室最热点时刻)

 1998-12-22 4:34:26 (Fmax)=-10.68 °C
 1998-12-21 7:48:46 (Fmin)=-24.26 °C
 1998-12-21 7:48:46 (ton)=88.80 °C
 1998-12-21 7:48:46 (toff)=88.80 °C
 耗电量=1.4768 (kWh/24h)

制表时间:1998-12-22 7:48:28