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**HIGH-LEVEL ADVISORY SERVICES FOR THE
BAIKALSK PULP AND PAPER MILL**

SI/RUS/94/801/11-57

RUSSIA

Technical report: Air emission control and abatement in kraft pulping*

Prepared for the Government of the Russian Federation
by the United Nations Industrial Development Organization,
acting as executing agency for the United Nations Development Programme

Based on the work of Engineer Jouni Eerikaeinen

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* This document has not been edited.

I. EXPLANATORY NOTES

Adt/a	air dry metric tons pulp per annum
Adt/d	air dry metric tons pulp per day
BPPM	Baikalsk Pulp and Paper Mill
CHEM	The Centre for Hydrometeorology and Environmental Monitoring
Cl	chlorine
ClO ₂	Chlorine dioxide
CO	carbon monoxide
CS ₂	carbon disulphide
DMDS	dimethyl disulphide
DMS	dimethyl sulphide
H ₂ S	Hydrogen disulphide
IET	Institute for Ecological Toxicology
kg/Adt	kilograms per air dry tons pulp
kgS/Adt	kilograms sulphur per air dry tons pulp calculated as total sulphur
MM	methyl mercaptane
MPC	maximum permissible concentration in milligrams per cubic meter
MPD	maximum permissible discharge in tons per annum
NO _x	nitrous oxides
SCR	selective catalytic reduction
SNCR	selective non-catalytic reduction
SO ₂	sulphur dioxide
RCEP	Regional Committee for Environmental Protection
TCEP	Territorial Committee for Environmental Protection
TPD	temporary permitted discharges in grams per second or tons per annum
TRS	total reduced sulphur

II. ABSTRACT

The objective of the mission was to collect all relevant information concerning government limitations for air pollutants discharged in the Baikal Lake Ecosystem, access air pollution treatment facilities, evaluate their efficiency and propose measures to minimise air emissions. The process modifications proposed by Mr. Olli Jalkanen as a result of his mission in February-March 1995 were used as the starting point of this evaluation.

The Mill is constantly out of regulatory compliance mainly because of very large air emissions (dust, SO₂, CO, NO_x) related to energy production. The specific heat consumption 43 GJ/Adt is twice as much as in Kraft pulping in 70's. Thus the air emissions of five auxiliary coal boilers are very high. The specific sulphur emission from energy production for the pulp mill is ca. 13 kgS/Adt, which is more than six times the recommended level in Nordic countries.

The odour emissions of the Mill are on an acceptable level, ca. 2,6 kgTRS/Adt and the smell of the Mill is lower than in most of the Kraft mills the author has visited. However, the emissions of TRS compounds (H₂S, MM, DMS, DMDS) are many times over the

regulatory limits, which are very strict. The measured concentrations of MM and H₂S in the sanitary zone of the Mill have exceeded the MPC values in some cases.

The information presented to the author show, that the airborne emissions of the Mill to the Baikal Lake and its catchment area present less than 3 % of the total emissions from the industry which is mainly located on the valley of Angara river. Despite of the high specific emissions from the energy production of the Mill, its role in airborne pollution of Baikal Lake is insignificant.

The 33 emission treatment facilities of the Mill are in general at good or satisfactory level with scrubbers, electrostatic precipitators, desulphurization unit, bag filters etc. The efficiency of the lime kiln flue gas scrubber should be improved and dissolver tanks should be equipped with scrubbers.

The air emissions from the proposed future cooking plant will decrease because of the cold blow system. The strong odour gases from cooking are proposed to be burned in the Bark boiler NR. 5. The weak odour gases from cooking and black/white liquor tanks are proposed to be cooled and combusted in the Power boiler NR. 8. Both boilers are equipped with desulphurizing equipment (Lifac in boiler 8 and scrubber in bark boiler 5).

The emissions related to energy production should be decreased with the proposed process changes and implementing of an energy efficiency program. The estimated target heat consumption with 200 000 Adt/a production in future is 50-55 % and power consumption 60-65 % of the present consumption figures. The specific sulphur emissions will decrease with ca. 50-55 % to ca. 5,5-6,0 kg S/Adt. The TRS emissions will decrease ca. 70-75 %.

The investment costs for odour abatement, lime kiln scrubbers and recovery boiler dissolvers is ca. 4,3 MUSD.

The regulatory limits for dust and NO_x at the present production level will not be met with the proposed changes. Low NO_x burners or SNCR technology and improving of the efficiency of the electrostatic precipitator is recommended for the power boiler NR. 8. Complying with the methyl mercaptane MPD limit is probably not possible with present available odour abatement technologies.

III. TABLE OF CONTENTS

I. EXPLANATORY NOTES.....	1
II. ABSTRACT.....	1
III. TABLE OF CONTENTS.....	3
INTRODUCTION.....	4
IV. GOVERNMENT LIMITATIONS FOR AIR POLLUTANT DISCHARGES IN THE BAIKAL LAKE ECOSYSTEM.....	4
A. REGULATORY AUTHORITIES.....	4
B. AIR EMISSION REGULATIONS.....	5
C. SAMPLING, MEASURING AND REPORTING PROCEDURES.....	5
D. SUMMARY ON AIR QUALITY MEASUREMENTS.....	6
E. REVIEW OF PAST AIR EMISSIONS.....	7
F. ENVIRONMENTAL IMPACTS OF AIR EMISSIONS.....	7
G. REGULATORY COMPLIANCE.....	7
V. AIR EMISSION TREATMENT FACILITIES AT THE MILL AND MEASURES TO MINIMISE AIR EMISSIONS.....	8
RECOMMENDATIONS.....	10
1. PROPOSED PROCESS CHANGES AND THEIR INFLUENCE ON AIR EMISSION ABATEMENT.....	10
1.1. Emissions related to energy production.....	10
1.2. Odour abatement.....	11
1.3. Recovery boiler dissolvers.....	12
1.4. Lime kiln flue gases.....	12
2. SUMMARY OF AIR EMISSION ABATEMENT WITH PROPOSED CHANGES.....	13
3. PRELIMINARY INVESTMENT COST ESTIMATE.....	13
VI. LITTERATURE CITED.....	14
VII. ANNEXES.....	14

INTRODUCTION

PI-Consulting Ltd was commissioned on 16.06.1995 by UNIDO to provide independent expert advice on modifications to the processes employed at the Baikalsk Pulp and Paper Mill to minimise/eliminate impacts of potential emergency and continuous air pollutant releases on the Baikal ecosystem. This work is based on the pulping process modifications recommended by Mr. Olli Jalkanen, who visited the Mill earlier in 1995.

The mission was conducted by Senior Consultant Mr. Jouni Eerikäinen. The work started on 31st July 1995 and this report was delivered to UNIDO on 22nd August 1995. The mission at the Baikalsk Pulp and Paper mill was carried out between 1-.12.08.1995.

IV. GOVERNMENT LIMITATIONS FOR AIR POLLUTANT DISCHARGES IN THE BAIKAL LAKE ECOSYSTEM

A. Regulatory authorities

The regulatory agency for air emissions of the facility is the "Regional Committee for Environmental Protection & Natural Resources Conservation" (RCEP), located in Irkutsk. The "Territorial Committee for Environmental Protection & Natural Resources Conservation" (TCEP) in Baikalsk reports to RCEP and carries out air, water and soil sampling and measuring in Sludjansk district including more than hundred plants and enterprises. Baikalsk City is a part of Sludjansk district. RCEP regulates and gives the limit values for air pollutants. TCEP has 3 specialists for water quality control and 3 specialists for air quality control.

"The Centre for Hydrometeorology and Environmental Monitoring" (CHEM) in Baikalsk is responsible of the regular control of air quality in the Baikalsk City area. It reports to TCEP on non compliance of the measured data with the regulatory limits.

"Institute for Ecological Toxicology" (IET) of Ministry of Environmental Protection of Russia is a research institute dedicated to study the ecosystem of Lake Baikal and its environmental impacts of anthropogenic origin. It is located in Baikalsk and started the research and education already in sixties when the BPPM was built. IET has no regulatory authority role, but delivers scientific data for public and environmental authorities.

TCEP and CHEM work in close co-operation with the analytical laboratory of BPPM which analyses the air quality in the sanitary area twice a month.

The following persons were met during the visit:

TCEP:	Ms. Ludmila Innokentevna Kalashnikovna,	Deputy Chief
CHEM:	Mr. Anatolyi Polovinskyi,	Chief of the Centre
	Ms. Ludmila Panchenko,	Chief of the Laboratory
IET	Dr. Albert M. Beim,	Director

B. Air emission regulations

The State law on environmental protection from 1987 and the State law for atmospheric protection regulate the air emissions. RCEP has issued permission on air emissions to BPPM, valid until 01.01.1996, see Annex 4. Maximum Permitted Discharges in grams per second and in tons per year, (MPD) and Temporary Permitted Discharges (TPD) are given to 18 components. The calculation of MPD values is based on recommendations issued by "Hydrometeorolozdat" 1987. The calculation considers, that the emissions from the Mill will not raise the ground level concentration of the compound above MPC.

Maximum Permitted Concentrations mg/m³ (MPC) and Temporary Permitted Concentrations (TPC) in the sanitary area ca. 1 km around the Mill are stated by RCEP.

C. Sampling, measuring and reporting procedures

CHEM controls the air quality with two stationary stations (NR. 47 and 48) located in Baikalsk City. Also monitoring laboratory in a car is used for sampling and analysing of Cl₂, CS₂ and H₂S. In 1994 10 723 analysis were done for 9 pollutants which are hazardous for human health and the results are analysed statistically. The samples are taken with absorption test tubes three times per day at 08.00, 14.00 and 20.00 hrs. The compounds analysed are dust, SO₂, CO, NO_x, H₂S, CS₂, Cl₂, MM and benzenopyrene. Also snow samples are analysed. The analyses are made according to GOST standards RRD 5204 186-89 mainly with photometric methods using characteristic filters for each compound.

IET takes samples from ground level air and precipitation samples from snow in Baikal lake and its catchment area. Ca. 100 km protection zone is surrounding the Baikal Lake. Helicopter is used for air sampling from mountains. IET also studies the impact of air emissions to humans, insects, mammals, lichens and to the morphology of needles of coniferous trees. IET has published several articles and research literature of the Baikal lake ecosystem and of the environmental impacts of the industry.

TCEP uses absorption tubes and bags for sampling in the sanitary area of BPPM and in surrounding. The analyses are made with GOST standards based on classical analytical chemistry. TCEP has a gas chromatography and a liquid chromatography in its laboratory. The instruments are calibrated once a year according to standards and law. Ms Kalashnikova would like to use portable quick gas analysers, but they are expensive and not certified by the authorities. The samples are normally taken ca. once per month for toxic substances and ca 2-6 times per year for less harmful substances. The compounds mostly measured are H₂S, MM, DMS, DMDS, SO₂, NO_x, CO and dust.

The Sanitary Laboratory of the BPPM analyses the air quality in the sanitary area of the Mill and reports to TCEP.

D. Summary on air quality measurements

The main results are listed below:

Table 1. Baikalsk City air quality control data from 1994 prepared by CHEM

Compound	NR. of samples	Average concentration	Max. concentration	Month of max. conc.	Exceeding of max.perm. concentration
	pcs.	mg/m ³	mg/m ³		%
dust	1 611	0,1070	0,5999	3	0,3
SO ₂	1 613	0,0003	0,0039	1	0,0
CO	1 619	0,9573	5,0000	2	0,0
NO ₂	1 613	0,0353	0,4799	4	6,8
H ₂ S	1 619	0,0007	0,0089	3	0,1
CS ₂	505	0,0054	0,0679	1	2,0
Cl	1 613	0,0008	0,0799	3	0,0

The highest concentrations have occurred in cold season between January and April. NO₂ concentration have exceeded the max. permissible concentrations in 6,8 % of the samples. The high CS₂ concentrations were explained as a reaction product from hydrogen sulphide and carbon monoxide.

The air quality measurements carried out by the Sanitary Laboratory of BPPM and reported to TCEP are shown below:

Table 2. Air quality measurement data from BPPM sanitary area, January-March 1995

Comp. measured	MPC mg/m ³	Nr. of samples	NR. of detected comp.	NR. of exceedings of MPC	Min. mg/m ³	Average mg/m ³	Max. mg/m ³
Turpentine	2,0	26	26	-	0,1234	0,3579	0,6572
ClO ₂	0,1	26		-			
H ₂ S	0,008	26	26	4	0,00037	0,0035	0,0142
SO ₂	0,5	26	20	-	0,0019	0,0197	0,0958
Phenols	0,01	26	20	1	0,0003	0,0017	0,0076
MM	0,0001	13	12	12	0,0005	0,0039	0,0091
CS ₂							

Methyl Mercaptane (MM) and Hydrogen Sulphide (H₂S) concentrations are the most problematic compounds. In order to reduce their concentrations below MPC, the emissions should be reduced to 18,3 t/a for H₂S and to 0,3 t/a for MM. In the present permission of BPPM the MPD for H₂S is 9,15 t/a and for MM 0,15 t/a. The actual emissions in 1994 were 110,2 t/a for H₂S and 66,9 t/a for MM.

E. Review of past air emissions

The emissions statistics from 1990..1994 are shown in Annex 5.

F. Environmental impacts of air emissions

According to the research work by IET no signs of pollution has been observed in humans, mammals, insects and in needles of coniferous trees in the area of Baikal lake. In an area of ca. 360 km² around BPPM a very sensitive Usnaja lichen is disappeared. The emissions from industry, cities and traffic affecting to the Baikal lake are presented in detail in Annex 6. It is clearly shown, that the impact of BPPM on the emissions and fall out of dust, sulphur, carbon monoxide and nitrogen on the aquatory and water catchment area is negligible and below 3 % from the total emissions of the area. The prevailing winds from north west carry atmospheric emissions from Angara river and Irkutsk industrialised area to the Baikal lake. The most polluting industry in Irkutsk consists of coal mining, oil refining and coal power stations. The impact of BPPM on the SO₂ concentration and fall out in the southern part of Baikal lake is very local and represents only a minor part of the emissions in comparison with the emissions coming from the Angara river area.

The smell of TRS compounds in the vicinity of BPPM is rather low compared with Kraft mills with higher sulphidity. The smell can be detected at day time in adjacent hills, when the prevailing winds from Northwest blow the exhausts gases to the hills. During the night the direction of the wind turns back to the lake. Based on the study of Pavlov /1/, the at the distance of 6 km from the Mill SO₂ concentration is below 0,05 mg/m² and the impact of air emissions from BPPM covers an area within ca. 3-5 km radius from the Mill.

Pleshanov /2/ has observed, that if the level of BPPM emissions will remain at the present level, the trees in South East coast and valleys will be exposed to unfavourable conditions with micro diseases.

G. Regulatory compliance

According to the discussion with Ms Kalashnikova TCEP, the Mill is continuously out of regulatory compliance. The electrostatic precipitators are causing dust emission problems, when they are not working well. The coal power boilers fall out regularly because of reparations due to cracks in tubes etc. When the boiler is started again with heavy fuel oil, the electrostatic precipitator is out of use for a while before the flue gas temperature has raised sufficiently. This causes peak dust and smoke emissions lasting 2-3 hours. Other problematic compounds are especially MM and also DMDS.

TCEP would like to tighten the MPC levels. Written violation notices are given almost weekly to BPPM e.g. from dust emissions and TCEP receives complaints from the neighbouring inhabited area. However BPPM is not the only mill, which is exceeding the MPC values and giving reasons for violation notices in Sludjansk territory.

The Mill can not meet the MPD requirements for air emissions and is obligated to pay fines according to the exceeding of MPD and TPD values. The fines in 1994 were 116 million Rubles (ca. 29 Thousand USD)

Table 3. Emissions and MPD values in 1994

Compound	Emission in 1994 (t/a)	MPD (t/a)
Dust	3660,8	370,41
Sulphur dioxide SO ₂	2960,3	1750,00
Carbon oxide CO	811,5	468,50
Nitrous oxides NO _x	2551,0	595,52
Hydrogen sulphide H ₂ S	110,2	9,15
Methyl mercaptane MM	66,9	0,15
Dimethyl sulphide DMS	160,7	5,38
Dimethyl disulphide DMDS	128,2	7,68
Chlorine Cl ₂	3,1	1,54
Chlorine dioxide ClO ₂	4,2	2,85
Turpentine	46,4	18,25
Alkaline aerosols	14,0	7,02
Total	105217,3	3236,45

V. AIR EMISSION TREATMENT FACILITIES AT THE MILL AND MEASURES TO MINIMISE AIR EMISSIONS

The Mill has identified 126 air emission sources, 105 of them are operating constantly. 93 % of emissions are treated in 33 treatment equipment. The emissions are measured in 1989-90 by a research institute. The process description and emission sources are described in detail in Annex 7. All emission sources are numbered and the stacks and vents are shown in lay-out Annex 8.

In general the treatment facilities represent a good technology from sixties and seventies. Some innovative catalytic treatment facilities are installed for treatment of foul condensates and hot well relief gases. A catalytic "Emulgator" is installed after one of the two lime kiln scrubbers.

The main sources of emissions are related to energy production. Four recovery boilers and five coal power boilers are equipped with electrostatic precipitators. The power boiler NR. 8 is connected to "Lifac" desulphurizing equipment based on semidry lime method. Two bark boilers and the sludge furnaces are equipped with scrubbers.

In recent years the emission abatement in Kraft pulping is concentrated to decrease sulphur emissions. NO_x emissions are normally quite low from recovery boilers and dust emissions can be easily reduced with conventional scrubbers, electrostatic precipitators (E.P.) and bag filters. Chlorine and chlorine dioxide emissions are also relatively small and decreasing due to shift to ECF or TCF bleaching.

Sulphur emissions in Nordic countries e.g. in Finland are at present on a level of ca. 2,5 kg S/Adt including both TRS (Total Reduced Sulphur including H₂S, MM, DMS and DMDS) and SO₂ (sulphur dioxide). The sulphur content in each emission component is calculated using molecular weights and the sum of sulphur is expressed as kilograms sulphur per produced air dry pulp ton, kg S/Adt. Sulphur emissions are divided to strong and weak odour gases from the process and to SO₂ emissions from recovery boilers, bark boilers, auxiliary boilers and lime kiln.

Odour gases in a Kraft pulp mill has always been a nuisance and technologies have been developed recently in order to reduce the bad smell of Kraft pulp mills. Strong odour gases originate from blow heat recovery vent, turpentine recovery vent, evaporator hot well vent, foul condensate stripping, foul condensate storage tanks and continuous digester relief. Strong odour gas flows are small, ca 200..1500 Nm³/h and TRS concentrations are high. Weak odour gases are collected from the washing plant and from various black liquor tanks. The volumes of weak odour gases vary very much, 15 000...80 000 Nm³/h depending on the type of process, sulphidity level and from how many sources the odour is to be reduced.

The sulphur emissions in 1994 from the measured sources are presented in Annex 9. The dominant source of TRS gases is the relief gas from the accumulator tanks, ca. 54 % of the total TRS emissions. The relief gases from the hot wells of the evaporation plant are treated together with foul condensates in four catalytic scrubbers. The scrubber capacity is 100 m³/h. It is ca 16 m high, 3 m in diameter consisting of Antimony/PE pellet catalyst beds. Foul condensate and hot well gases are fed to the bottom of the scrubber through bubble nozzles. Air is mixed in 1:5...1:10 proportion and TRS compounds are oxidised to sodium thiosulphate and sodium sulphate. The cleaned condensate is used in the washing plant.

The weak odour gases consist of vent gases from the white liquor dosing tank and vent gases from black liquor and white liquor tanks. The significance of weak odour gases from washer hoods from washing plant, chip bins, various chests and towers from washing, screening and bleaching plant is small. Thus the odour abatement is concentrated only to sources presented in Annex 10.

The emissions kgS/Adt are compared to the emissions in the Finnish Kraft pulp mills in seventies in Annex 9. Following conclusions can be made from the comparison and from the discussions with regulatory authorities:

- The specific SO₂ emissions are more than six time higher compared with Finnish mills
- Main part of the fines are caused by the emissions related to the energy production: SO₂, NO_x and dust
- Total TRS emissions are in acceptable level compared to Finnish mills, but the local MPC levels of MM and H₂S are often exceeded
- Emissions from the recovery boiler dissolving tanks are high
- Emissions from lime kiln flue gas scrubbers are twice higher than the acceptable level
- The malfunctioning of power boilers and E.P:s causes very often short time smoke and dust emissions

RECOMMENDATIONS

1. Proposed process changes and their influence on air emission abatement

Mr. Olli Jalkanen, whose target was to identify new cleaner technologies has recommended the following process changes:

- New cooking with cold blow
- Improved washing
- Closed new screening
- Oxygen delignification

An investment to a new batch cooking is recommended and it has a great influence in TRS gas releases and overall energy efficiency. Other recommendations would improve mainly energy efficiency and consequently reduce the air emissions from the energy production.

The basis for the recommendations below is that the modifications proposed by Mr. Jalkanen will be implemented.

The Mill personnel has identified process modifications, which will improve the air emission abatement. The most important modifications are:

- Polysulphide cooking with low TRS emissions
- Modernisation of boilers 7, 9, 10 and 11 including Low NOx burners or SNCR or SCR technology and reconstruction of E.P.
- Replacement of the E.P. for recovery boiler 4

The process modifications and recommended technology for air emission abatement is discussed below.

1.1. Emissions related to energy production

A modern Kraft pulp mill is self sufficient in electrical power and heat energy without external fuels and excess power is sold out. BPPM sells ca. 14 % of the produced heat to the Baikalsk City. 78 % of electrical power and 74 % of the heat for the Mill is produced in five coal power boilers using quite low calorific value coal, see Power and Heat production in Annex 11.

The specific energy consumption figures GJ/Adt and GWh/Adt are shown in Heat and Power Balance, Annex 11. Compared with the normal technology in Kraft pulping in 70's the specific heat consumption of process is ca. 175 % higher and power consumption ca. 24 % higher. Thus energy saving is an important issue both for the economy and environmental impacts of the mill. The water consumption 331 m³/Adt reflects the situation. In conventional and modern Kraft mills the water consumption is ca. 20..40 m³/Adt. Huge amounts of water is used in BPPM especially in screening and bleaching but also in other departments. Condensate return percentage is quite low. The effluent

treatment plant uses large amount of energy for aerating of large waste water volumes including cooling waters.

Obviously the energy related air emissions SO₂, NO_x, CO and dust should be reduced by using energy more efficiently. Heat and energy production is responsible from 82% of sulphur emissions and of main part of dust, NO_x and CO emissions of the Mill. Thus an professional energy audit and energy saving program is recommended to the Mill. The modernisation program recommended for the mill will decrease the energy consumption significantly, but still a great deal of energy should be saved after reconstruction with a special energy efficiency program.

The NO_x abatement with low NO_x, SNCR or SCR technology should be considered after implementation of the energy efficiency program and taking care of the real problem, which is high energy consumption.

The time reserved for the air emission abatement study does not allow to go very deep in energy saving issues. However, a rough estimate has been prepared for a target heat and power consumption based on future production 200 000 Adt/a, see Annex 11. Because the Mill has several external heat and power consumers like the paper machine, effluent treatment plant and Baikalsk City, the Mill can not be self sufficient in energy. The estimated specific target heat consumption in future is 52 % and power consumption 63 % of the present consumption figures including external consumers.

The heat and power production is evaluated for 200 000 Adt/a production with the target figures. The following conclusion can be made from the figures in Annex 12:

- One recovery boiler and two power boilers will be idle after improvements.
- Lifac should be operating all the time in order to reduce SO₂ emissions.
- Specific sulphur emissions related to energy production for the Mill will decrease with 54 %

1.2. Odour abatement

The planned odour abatement system is shown in Annex 13. The principle is to combust the odour gases in boilers, which are equipped with sulphur removal equipment in order to avoid SO₂ emissions.

The strong odour gases are treated as follows:

The blow and digester relief gases 300 Nm³/h are collected with AISI 316 DN 100 pipeline to the Bark boiler 5. The system consists of a steam ejector, condensate drums and water seal with pumps, droplet separator, flame arresters, rupture disks placed in 30 m distances, emergency shutdown, fan and a specially designed heavy fuel oil combustor fitted in the boiler secondary air zone. The present burner may also be reconstructed to odour gas combustion. A closed flare is used as a reserve burner. It is connected to the pipeline and separated with flame arrester from the system. The combustion efficiency and SO₂ removal efficiency of the flare is quite low, ca. 70%, but it is much cheaper than a dedicated auxiliary burner or auxiliary boiler.

The weak odour gases are treated as follows:

The weak odour gases 9 000 Nm³/h from black liquor and white liquor tanks in the evaporation plant are collected via pipeline to a cooling scrubber. The weak odour gases from the blow and filtrate tanks and brown stock filters in the cooking plant are also collected to the cooling scrubber. After the cooling scrubber the odour gas flow 18 000 Nm³/h is conducted with a fan to a heat exchanger preheater and heated with medium pressure steam in order to remove humidity from the flow. The preheated flow is then conducted via AISI 316 DN 800 pipeline to the coal power boiler 8 tertiary air feed level. The boiler is equipped with Lifac desulphurization equipment. In case coal power boiler 8 cannot be used for odour treatment, alkali (white liquor or NaOH) is fed to the cooling scrubber instead of water in order to remove H₂S and MM from the weak odour gas. In this case the washed odour gas is conducted to the atmosphere via a separate stack.

The characteristic properties of the boilers are given in Annex 11. The air feeds are shown in the table below:

Table 4. Boilers for odour gas combustion

		Coal power boiler 8	Bark boiler 5
Odour gas flow	Nm ³ /h	18 000	300
Primary air flow	Nm ³ /h	61 000	22 000
Secondary air flow	Nm ³ /h	40 000	14 000
Tertiary air flow	Nm ³ /h	40 000	

1.3. Recovery boiler dissolvers

The recovery boiler dissolver tanks should be equipped with scrubbers in order to avoid alkaline dust and TRS emissions. Weak white liquor is pumped to the scrubbers and a part of the circulation is conducted to the dissolver tank for green liquor preparation.

1.4. Lime kiln flue gases

The emissions from the lime kiln flue gas scrubbers are unexpectedly high. Normally similar scrubbers are used for lime kiln flue gas treatment and the TRS emissions are only ca 20..60 % of the present emissions. The alkali content of the lime mud was measured during the visit and it was 0,57% which is a bit high but within the reasonable limits (0,4..0,6 %). The recommendations proposed in the report of Mr. Olli Jalkanen would probably help the situation: By improving the separation, washing and drying of lime mud the alkali and sodium sulphide content of the lime mud can be reduced and the dry solid content increased. However, it is recommended to study the present operation parameters like burning temperatures in lime kiln zones, lime mud properties and the mechanical condition of the inside parts of the scrubber. It is important to reduce Na₂S content of lime mud as much as possible e.g., with increased vacuum air flow in lime mud filtration or with small hydrogen peroxide addition. Na₂S will thus be oxidised to sodium thiosulphate and sodium sulphate.

2. Summary of air emission abatement with proposed changes

The summary on the present emissions and emissions after modifications described above with present production capacity 120 253 Adt/a and future capacity 200 000 Adt/a/a is given below:

Table 5. Summary on air emission abatement with proposed changes

Production	Emissions in 1994		Limit values	Future emissions with proposed changes			Reduction
	120 253 t/a			120 253 t/a	200 000 t/a		
Component	kg/Adt	t/a	MPD t/a	kg/Adt	t/a	t/a	% kg/Adt
Dust	30,44	3 660,8	370,41	12,71	1 528,42	2 541,0	- 58
SO ₂	24,62	2 960,3	1759,00	11,04	1 327,59	2 208,0	- 55
CO	6,75	811,5	468,50	3,61	434,11	721,0	- 47
NO _x	21,21	2 551,0	595,52	11,34	1 363,67	2 267,0	-47
TRS	2,62	315,5		0,71	85,38	141,4	- 73
TOTAL	85,64	10 299,1		39,41	4 739,17	7 878,4	
MM	0,56	66,90	0,15	0,15	18,13	30,15	-73

Even with the proposed improvements in process and cleaning technology the regulatory compliance with MPD values can not be met for dust, NO_x and TRS emissions. The NO_x emissions may be further decreased ca. 50-70 % with better combustion control, Low NO_x burners or SNCR technology. Dust can be reduced by improving the efficiency of the electrostatic precipitator of coal Power boiler 8. The most difficult item will be complying with methyl mercaptane MPD levels, which is probably impossible with the odour abatement technologies available at present.

3. Preliminary investment cost estimate

The preliminary investment cost estimate is given below:

Treatment of strong odour gases in Bark boiler 5:

Equipment:

- Odour gas burner with heavy fuel oil as support fuel
- Flare as a reserve combustor
- Steam ejector
- Fan
- Droplet separators
- Water seal with pumps
- Rupture disks and flame arresters
- Pressure relief and vacuum relief valves
- Emergency shutdown valve and bypass to the flare
- Automation & instrumentation, interlocking
- Electrical works
- Piping and ductwork

Erection and civil works	
Design and project management	
Total:	MUSD 1,4
Treatment of weak odour gases in the coal Power boiler:	
Cooling scrubber	
Preheater heat exchanger	
Fan	
New odour gas feed nozzles to the boiler, 2-3 pcs	
Droplet separators	
Emergency shut off valve and bypass to the stack	
Alkali feed system to the cooling scrubber	
Pressure and vacuum relief valves	
Automation & instrumentation, interlocking	
Electrical works	
Piping and ductwork	
Erection and civil works	
Design and project management	
Total:	MUSD 2,0
4 scrubbers to the recovery boiler dissolvers	MUSD 0,6
Lime kiln operation control	MUSD 0,3
TOTAL INVESTMENT COSTS TO AIR EMISSION ABATEMENT	MUSD 4,3

VI. LITTERATURE CITED

1. - Pavlov, B. K., The content intensitivity and distribution of air pollutants of BPPM, Monitoring of anthropogenic changes of mountain-taiga ecosystemsm, Moscow, Ecology, 1995, 208 p.
2. Pleshanov, A.S., Information about the present state of the forest of Baikal region, Institute of plant physiology and biochemistry, Siberian section of RAS, 1995

VII. ANNEXES

1. Job description
2. Senior counterpart staff
3. List of people met
4. Air emission permission
5. Air emission statistics 1990-1994
6. Air emissions on Baikal Lake area
7. Process descriptions and emission sources
8. The lay-out of the Mill and air emission sources
9. Sulphur emissions in 1994
10. Sulphur emissions after modifications
11. Power and heat production in 1994
12. Power and heat balance
13. Target power and heat production

ANNEX 1.

Job description

UNITED NATIONS INDUSTRIAL DEVELOPMENT ORGANIZATION

JOB DESCRIPTION

SI/RUS/94/801 - 11-57

Post Title: Consultant in Air emission control and abatement in kraft pulping

Duration: 0.7 m/m (2 weeks in the field, 1 week homebased)

Date required: ASAP

Duty station: Baikalsk, Russia
homebased

Purpose of the project:

To provide independent expert advice on modifications to the processes employed at the Baikalsk Pulp and Paper Mill designed to minimize/eliminate impacts of potential emergency and continuous pollutant releases on the Baikal Ecosystem.

Duties:

The consultant, in close co-operation with the mill management, other national and international consultants, government agencies and institutions is expected to:

1st mission: (2 weeks in the field)

- a. collect all relevant information concerning government limitations for air pollutants discharges in the Baikal Lake Ecosystem;
- b. Access the actual air pollution treatment facilities available in the mill, evaluate its effectiveness and propose measures to minimize/eliminate air emission;
- c. to prepare a report setting out the findings of the mission and with recommendations of measures to minimize/eliminate air emission in the mill;

2nd mission: (homebased, 1 week)

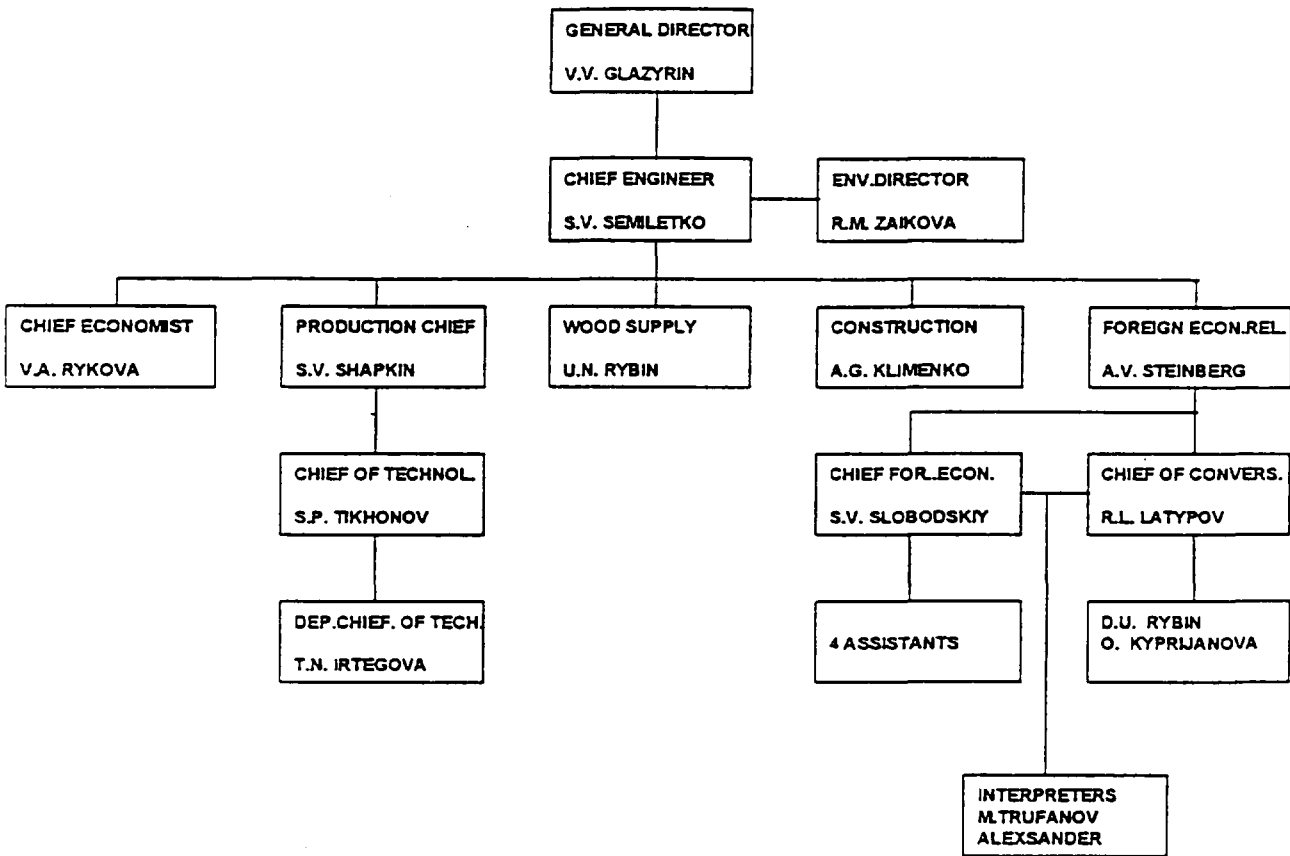
- a. evaluate the impact that the proposal(s) for modifying/reprofiling the mill to be prepared by other international experts will have in the elimination/minimization of air emissions;
- b. to prepare a report setting out the findings and with comments on the proposal (s) for modifying/reprofiling the mill and their impacts on air emissions;

ANNEX 2.

Senior counterpart staff

Glazyrin, Valeri Vasiljevich, general director
 Semiletko, Sergei Vasiljevich, chief engineer
 Rybin, Juri Nikolajevich, deputy manager for timber supply
 Shapkin, Sergei Vladimirovich, production chief
 Steinberg, Anatoli Vladimirovich, vice president, foreign economical relations
 Klimenko, Anatoli Grigorjevich, deputy of director, construction

BAIKALSK PULP AND PAPER MILL
 ORGANISATION



ANNEX 3.

List of people met

List of people met

Baikalsk Pulp and Paper Mill:

Baikalsk, Irkutsk Region, 665 914 Russia

Tel: +395 42 6 3 46

Glazyrin, Valeri Vasiljevich,
Shapkin, Sergei Vladimirovich,
Zaikova, Raisa Matvejenna,

Latipov, Rem Lufturahmanovitch

General Manager

Production Manager

Deputy Chief Engineer in Environmental
protection

Chief of conversion division

The Centre for Hydrometeorology and Environmental Monitoring

Baikalsk, Irkutsk Region, 665914 Russia

Prombaza, BCGMS

Tel: +395 42 49 66

Mr. Anatolyi Polovinskyi,
Ms. Ludmila Panchenko,

Chief of the Centre

Chief of the Laboratory

Institute for Ecological Toxicology

Baikalsk, P.O.B. 48, Irkutsk Region, 665 914 Russia

Tel: +395 42 29 38

Dr. Albert M. Beim,
Mr. Andrei Beim

Director

Research Scientist

Territorial Committee for Environmental Protection

Baikalsk, P.O.B. 33, Irkutsk Region, 665 914 Russia

Tel: +395 42 20 39

Ms. Ludmila Innokentevna Kalashnikovna,

Deputy Chief

ANNEX 4.

Air emission permission

edl
Me

27.07.95.
1-6-1383



МИНПРИРОДЫ РОССИЙСКОЙ ФЕДЕРАЦИИ

Иркутский областной комитет по охране окружающей среды и природных ресурсов

664047, г. Иркутск, ул. Парковая, 16, тел. 27-49-69

Permission
РАЗРЕШЕНИЕ

for the discharge of pollutants to atmosph.
на выброс загрязняющих веществ в атмосферу
by stationary pollution sources
стационарными источниками загрязнения

ВРРМ

Given to
Р. таво

Байкальскому ЦБК

наименование предприятия, организации, ведомственная принадлежность, реквизиты

Req. Com. for Environ. protection

Given by

Орган, выдавший разрешение
природных ресурсов

Областной комитет по охране окружающей среды и его реквизиты

Valid for from

Срок действия с 01.07.95 до 01.01.96

Регистрационный номер ОК-172/СРК

Дата выдачи 19.07.95

Registr. No.

И.о. председателя комитета



Malevskiy

А.Л.Малевский

БАЙКАЛЬСКИЙ
ОБЛАСТНОЙ КОМИТЕТ
ПО ОХРАНЕ ОКРУЖАЮЩЕЙ
СРЕДЫ И ПРИРОДНЫХ
РЕСУРСОВ
31 07 1995

The list & number of pollutants permitted

Перечень и количество загрязняющих веществ,
разрешённых к выбросу в атмосферу
for air emission

Загрязняющее вещество	ТАО Лимит ВСВ Суммарный выброс Total emission		Норматив ПДВ МРД Суммарный выброс т/год t/year
	т/год t/year	г/с	
<i>Inorganic dust</i> Пыль неорганическая	720,000		370,406
Пыль древесная <i>wooden dust</i>	0,5585		0,5585
Зола каменноугольная <i>coal ash</i>	1602,500		1223,725
Сернистый ангидрид <i>SO₂</i>	1750,000		1750,000
Сероводород <i>H₂S</i>	94,500		9,150
Метилмеркаптан <i>MM</i>	35,026		0,150
Диметилсульфид <i>DMS</i>	19,102		5,3765
Диметилдисульфид <i>DMDS</i>	7,6815		7,6815
<i>Turpentine</i> Скипидар	23,191		18,24575
Окислы азота <i>NOx</i>	1763,2325		585,5175
Окислы углерода <i>COx</i>	468,500		468,500
Аэрозоль щелочи <i>Alk. aerosole</i>	7,017		7,017
Двуокись хлора <i>ClO₂</i>	2,850		2,850
Хлор <i>Cl</i>	1,5425		1,5425
Фенолы <i>Phenols</i>	0,1885		0,1885
Метанол <i>Methanol</i>	0,00045		0,00045
Пятиокись ванадия <i>V₂O₅</i>	0,25615		0,25615
Бенз(а)пирен <i>Benzo(a)pyrene</i>	0,001168		0,001168

По каждому источнику в отдельности величины выбросов загрязняющих веществ в атмосферу
зафиксированы в книге в приложении

которая составляет неотъемлемую часть настоящего разрешения.

Начальник отдела нормирования

Гальцева

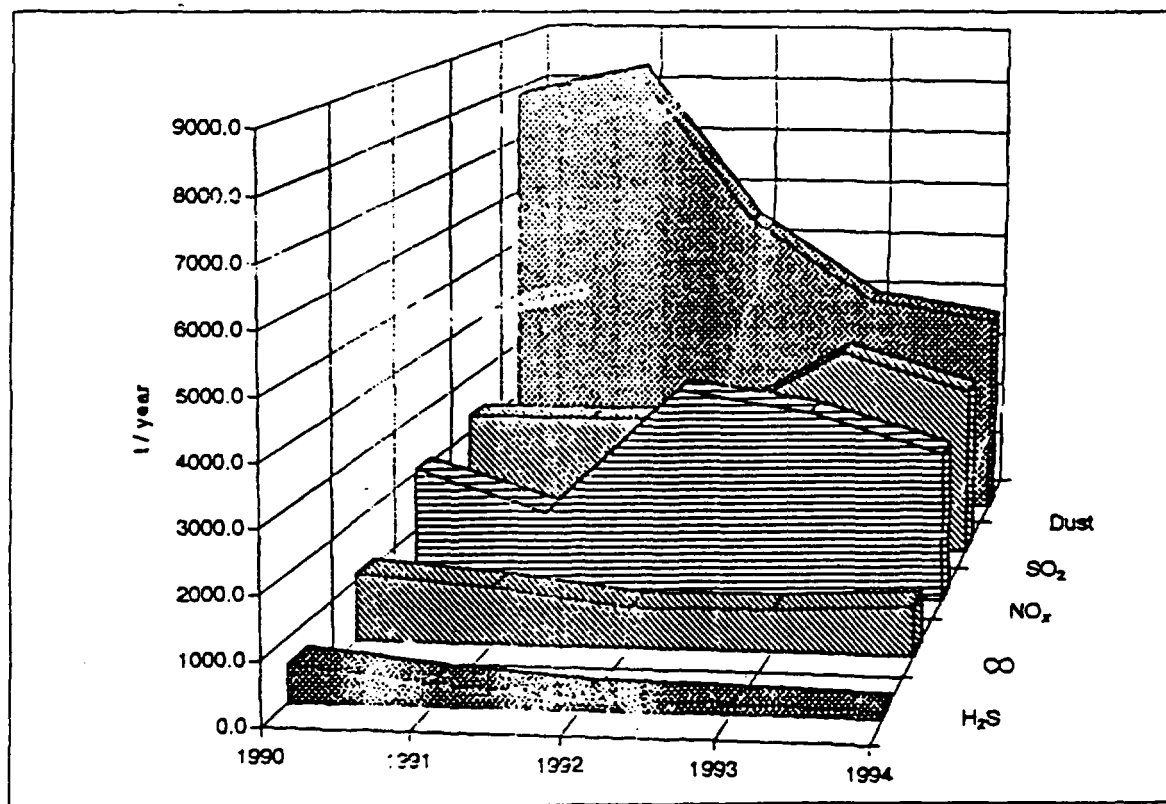
И.Н.Гальцева

ANNEX 5.

Air emission statistics 1990-1994

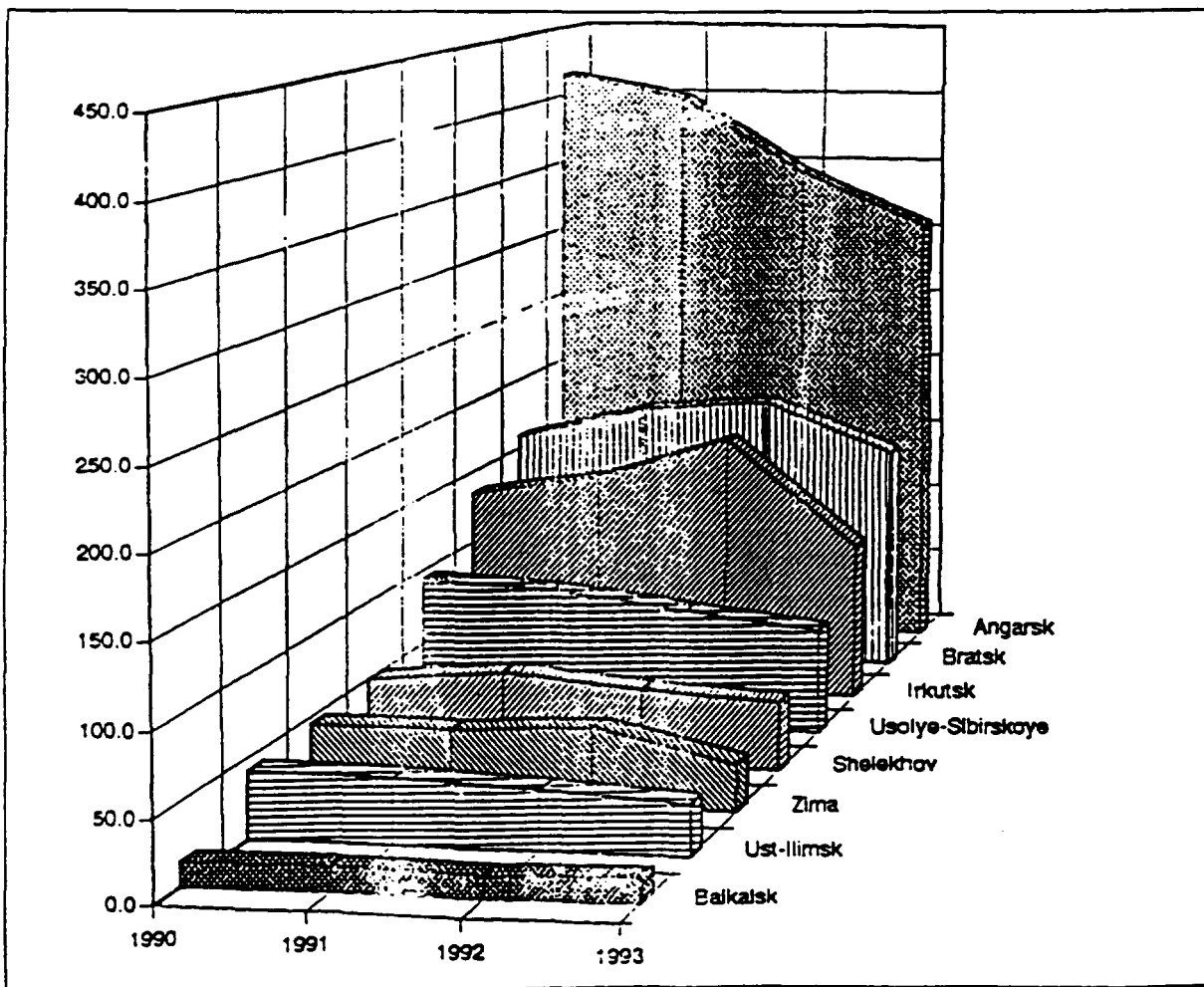
Harmful substances discharges into atmosphere from stationary sources of the BPPM

INGREDIENTS	FACTUAL DISCHARGES (t./year)				
	1990	1991	1992	1993	1994
H ₂ S	592.2	359.6	199.8	157.5	110.2
CO	1109.0	937.1	664.7	694.7	811.5
NO _x	2061.6	1355.9	3556.4	3220.0	2551.0
SO ₂	2300.7	2305.6	2304.7	3623.0	2960.3
Dust	7857.0	8350.5	5497.0	4005.0	3660.8



The dynamics of the summary harmful substances discharges into atmosphere from stationary sources situated around Lake Baikal
(thousand t. / year)

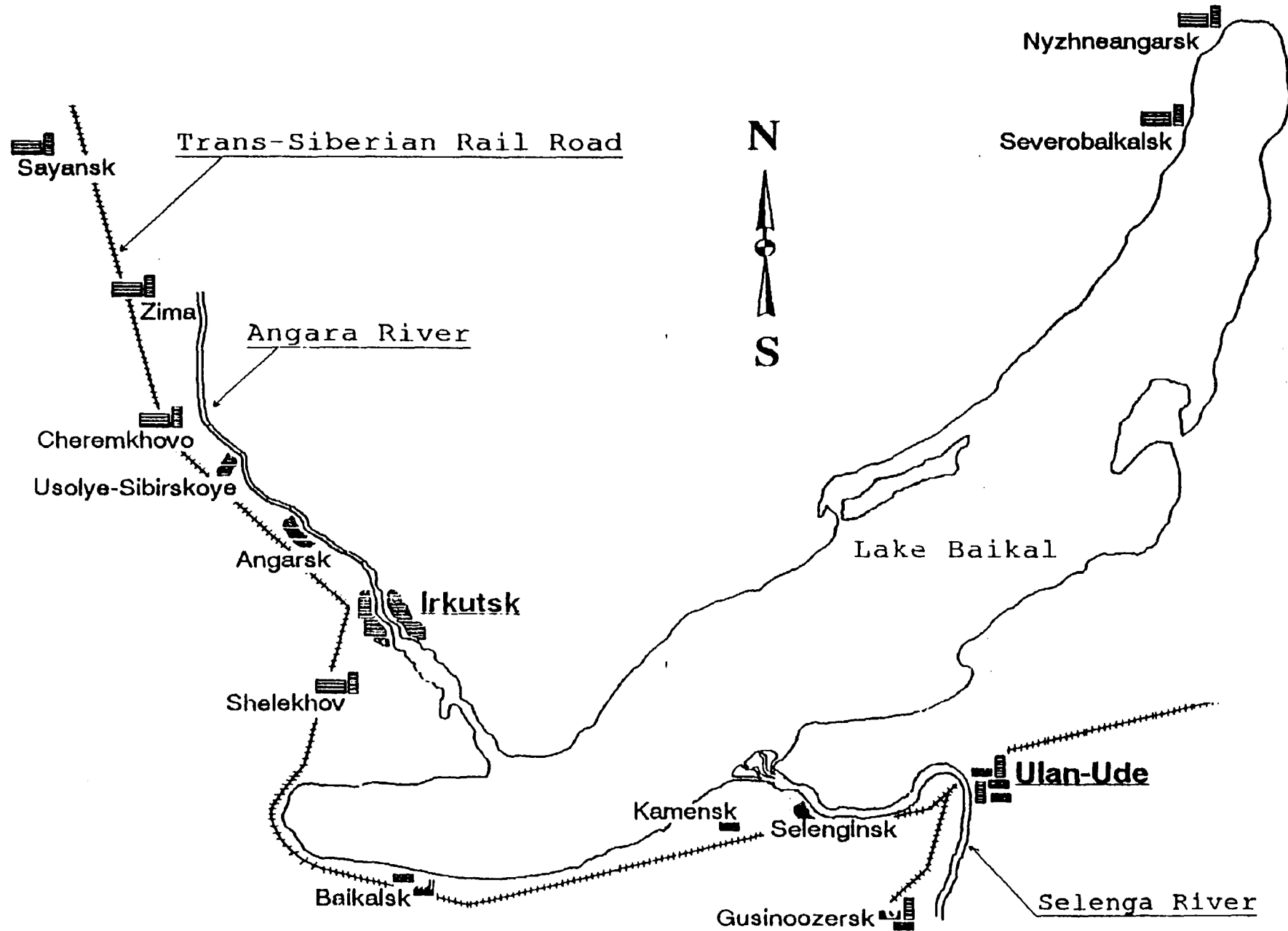
CITY	SUMMARY DISCHARGES (th. t/year)			
	1990	1991	1992	1993
Baikalsk	14.9	15.2	13.5	15.3
Ust-Ilimsk	42.1	40.5	36.6	30.9
Zima	45.4	44.5	49.7	29.4
Shelekhov	49.3	57.4	49.0	43.8
Usolye-Sibirskoye	93.9	88.8	77.9	67.5
Irkutsk	134.3	148.9	177.6	104.3
Bratsk	157.9	180.0	187.3	153.8
Angarsk	414.9	399.2	345.3	306.9



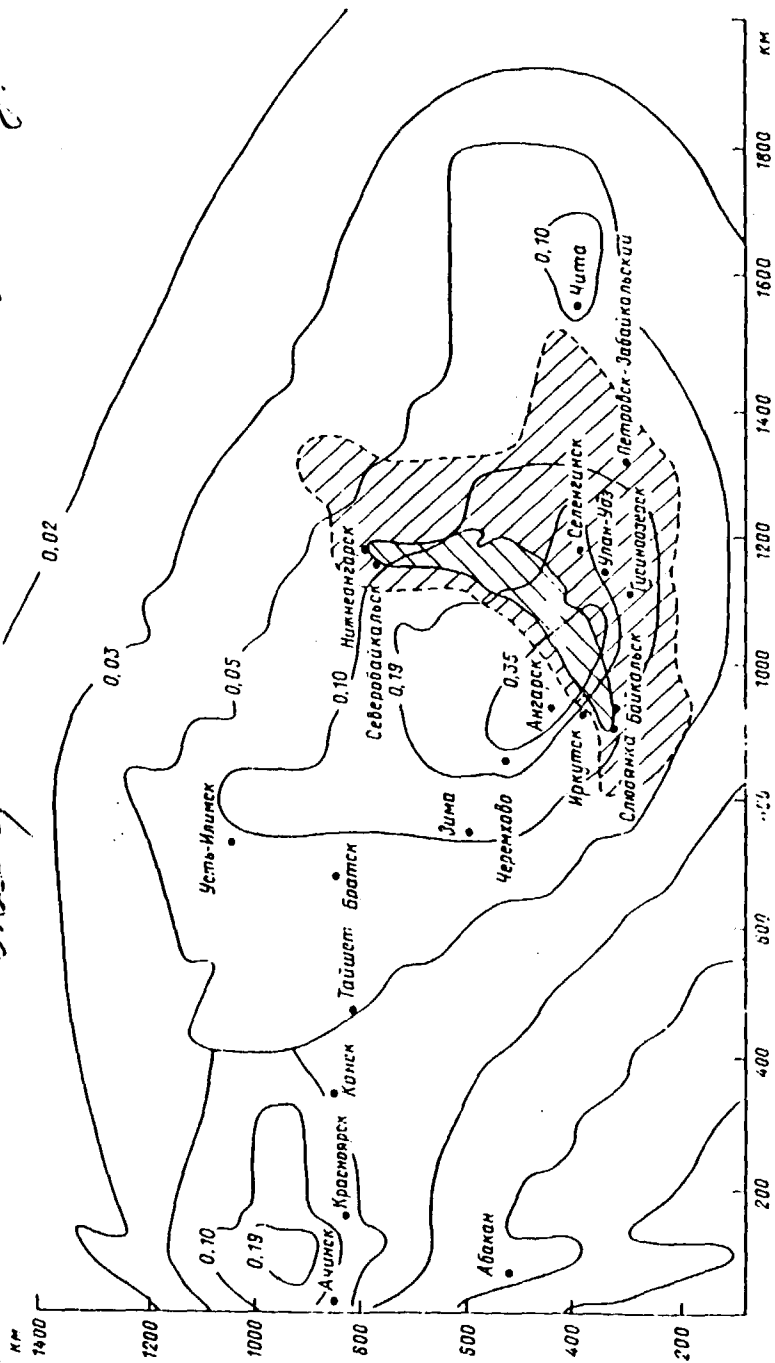
ANNEX 6.

Air emissions on Baikal Lake area

5. CL. O. OC. 10. 21. Stationary sources of all emissions situated around Lake Baikal



29
 Lake's base sediment
 may fall out of sulfur dioxide



Выпадение серы от выбросов промышленных предприятий 24 городов, г/(м²·год).
 Заштрихована водосборная площадь оз. Байкал.

Суммарные выпадения серы и азота на акваторию оз. Байкал и на водосборную площадь и вклад от различных городов

Источник выбросов	Сера		Азот	
	на акваторию Байкала	на водосборную площадь	на акваторию Байкала	на водосборную площадь
Суммарный выброс 21 городов, тыс. т/год	4,3	23,3	0,42	2,3
В том числе, %				
Ангарск, Черемхово, Шелехово, Усолье-Сибирское, Иркутск	63	56	57	54
Байкальск	10	11	11	12
Слюдянка, Северо-байкальск, Нижнеангарск	2	1,5	3	2
Селенгинск	1	1	1	1
Улан-Удэ, Петровск-Забайкальский, Гусиноозерск	2	1,5	2	1
Красноярск, Назарово	6	11	4	9
Лысьинск, Канск, Братск, Свирск, Чита, Тайшет, Кыта, Зима	4	10	7	13
КАТЭЖ (проект), тыс. т/год	2	3	2	3
	10	5	13	5
	1,1	9,7	0,39	2,8

ний дает Ангарско-Черемховский бассейн (63 % по сере и 57 % по азоту). За ним следуют Иркутск и Улан-Удэ, причем Улан-Удэ, Петровск-Забайкальский и Гусиноозерск в силу преобладания западных ветров вносят больший вклад загрязнения в поверхность водосбора, а не на озеро.

Соотношения по азоту примерно аналогичные.

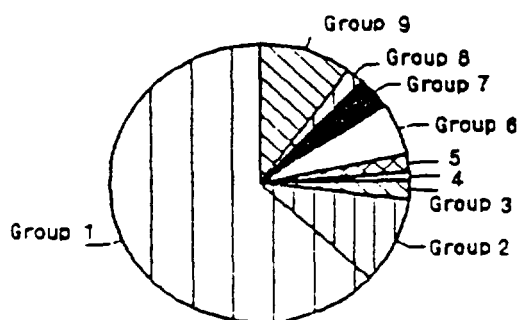
Выпадения от г. Назарово совместно с г. Красноярском составляют 2 % на Байкал и 2,8 % на водосбор. Введение в строй Березовской ГРЭС-1 увеличит выпадения серы и азота в 2,7 раза. Осуществление полной программы КАТЭЖа, планируемой ранее (8 Березовских ГРЭС) привело бы к выпадениям азота на оз. Байкал, сравнимым с выпадениями от всех ближних городов, и выпадением серы, составляющим 30 % от них.

В заключение надо отметить, что полученные результаты носят оценочный характер. Подлежат уточнению расчеты выпадений от источников, находящихся в непосредственной близости от оз. Байкал, поскольку применение моделей дальнего переноса для них вносит большие погрешности в ближней зоне. Необходимо также оценить влияние рельефа на перенос и выпадения примеси в районе Байкала.

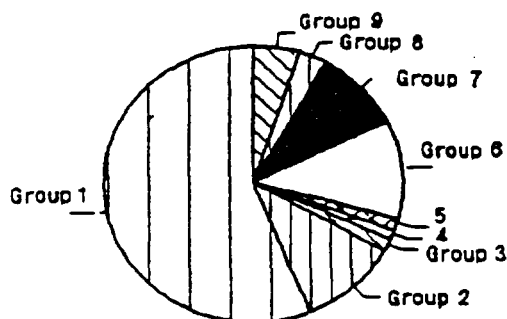
Summary fall of sulfur and nitrogen on the aquatory of Lake Baikal and its water catchment area and contribution of various cities

EMISSION SOURCE		SULPHUR Fall		NITROGEN Fall	
		on Lake Baikal aquatory	on water catchment area	on Lake Baikal aquatory	on water catchment area
Total emission of 24 cities (thous. t. / year)		4.3	23.3	0.42	2.3
Group	Including, %				
1	Angarsk, Cherekhovo	63.0	56.0	57.0	54.0
2	Shelekhov, Usolye - Sibirskoye, Irkutsk	10.0	11.0	11.0	12.0
3	Baikalsk	2.0	1.5	3.0	2.0
4	Sludyanka, Severobai- kalsk, Nyzhneangarsk	1.0	1.0	1.0	1.0
5	Selenginsk	2.0	1.5	2.0	1.0
6	Ulan-Ude, Petrovsk - Zabaikalsky	6.0	11.0	4.0	9.0
7	Gusinozersk	4.0	10.0	7.0	13.0
8	Krasnoyarsk, Nazarovo	2.0	3.0	2.0	3.0
9	Achinsk, Kansk, Chita Bratsk, Svirsk, Zima, Kyakhta, Taishet	10.0	5.0	13.0	5.0
KAHEC (project) (thous. t. / year)		1.4	9.7	0.39	2.8

SULFUR fall
on Lake Baikal aquatory



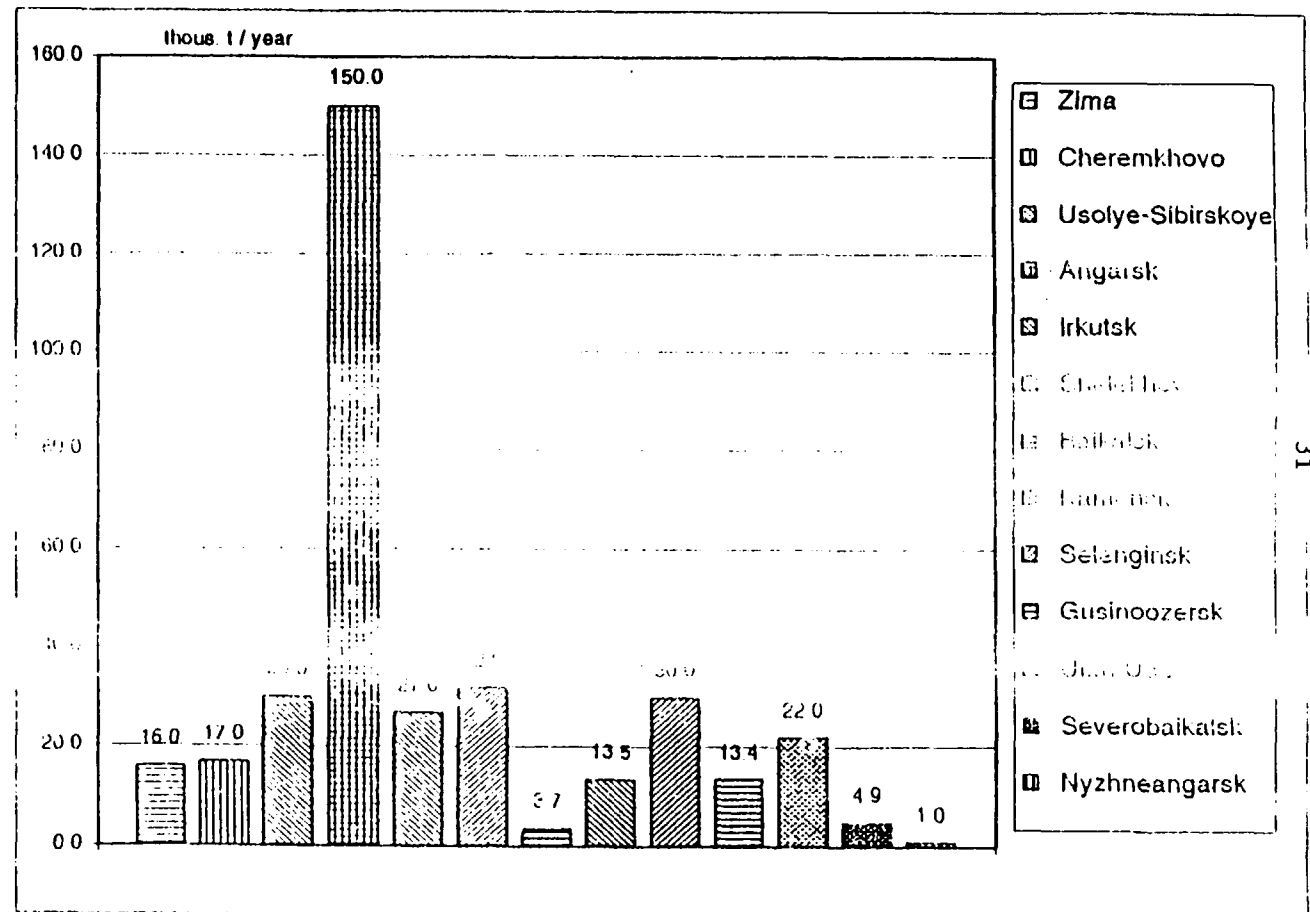
SULFUR fall
on water catchment area



air pollution emissions (t/year) into atmosphere from automobile transport and stationary sources situated around Lake Baikal

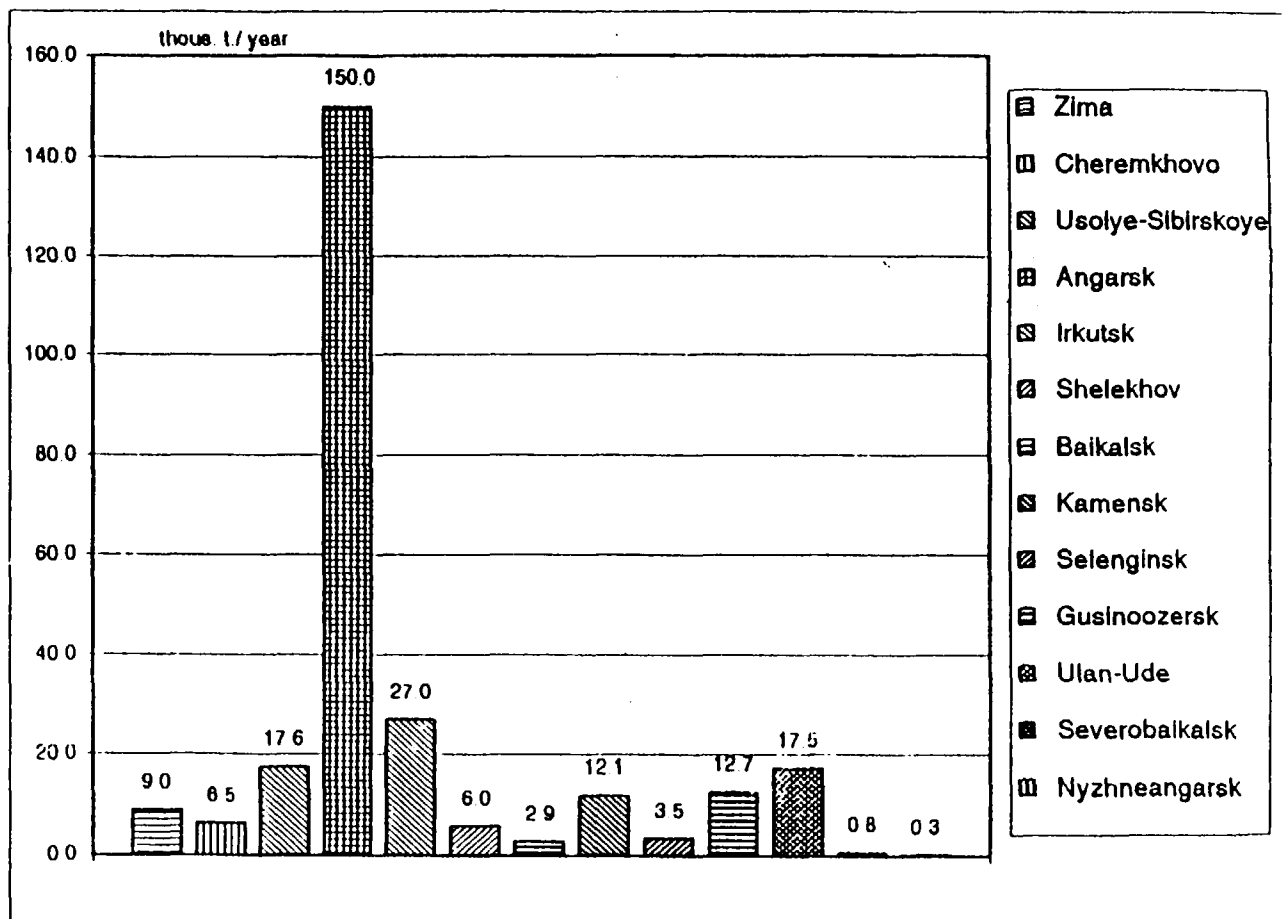
DUST (thousand t./year)

City	Dust (thous.t/year)
Zima	16.0
Cheremkhovo	17.0
Usolye-Sibirskoye	30.0
Angarsk	150.0
Irkutsk	27.0
Shel'nov	32.0
Baikal'sk	3.7
Kamensk	13.5
Selenginsk	30.0
Gusinoozersk	13.4
Ulan-Ude	22.0
Severobaikalsk	4.9
Nyzhneangarsk	1.0



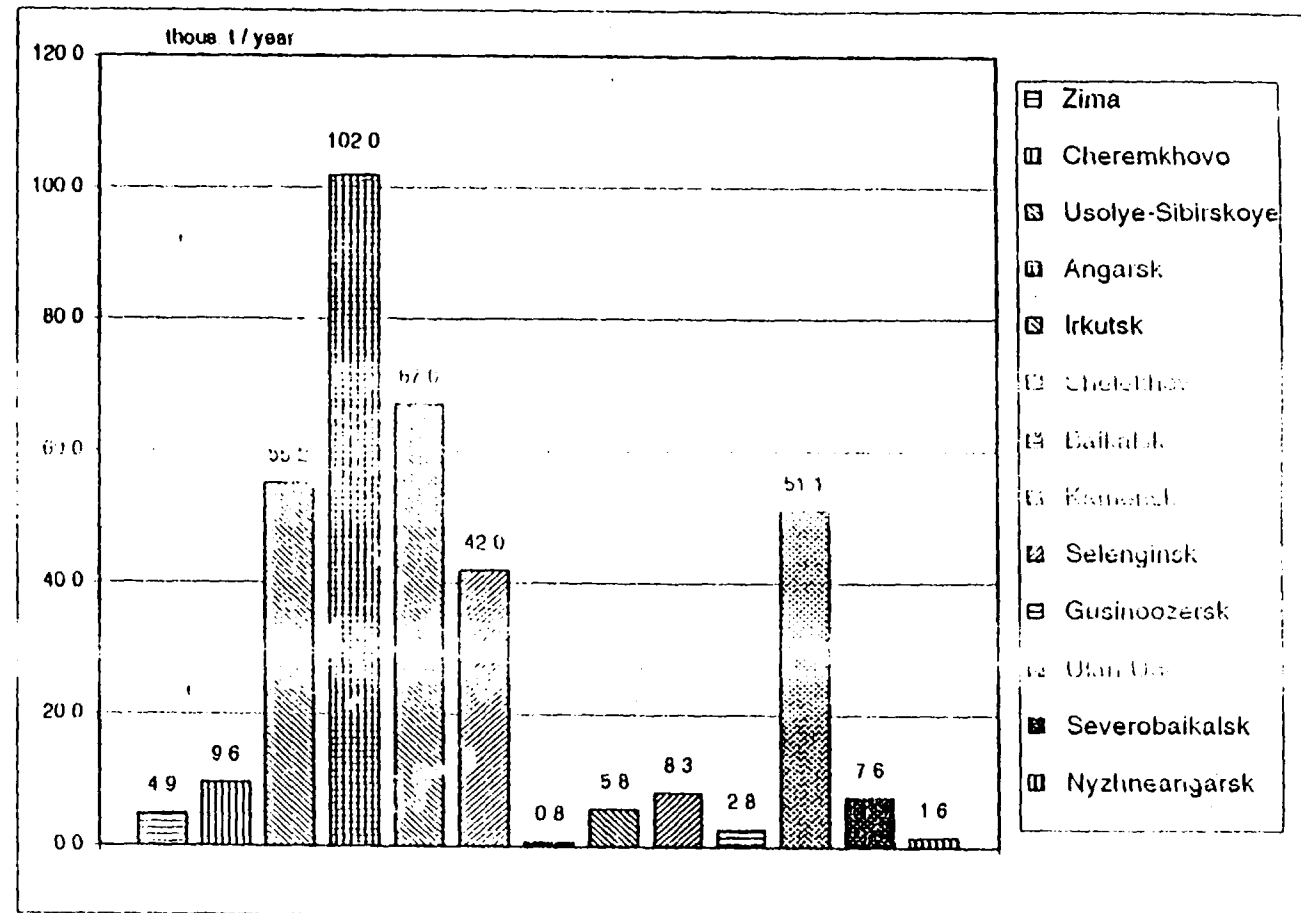
Major substances discharges into atmosphere from automobile transport and stationary sources situated around Lake Baikal
SO₂ (thousand t./year)

City	SO ₂ (thous.t/year)
Zima	9.0
Cheremkhovo	6.5
Usolye-Sibirskoye	17.6
Angarsk	150.0
Irkutsk	27.0
Shelekhov	6.0
Baikalsk	2.9
Kamensk	12.1
Selenginsk	3.5
Gusinozersk	12.7
Ulan-Ude	17.5
Severobaikalsk	0.8
Nyzhneangarsk	0.3



CO in the atmosphere from automobile transport and stationary sources situated around Lake Baikal
CO (thousand t./year)

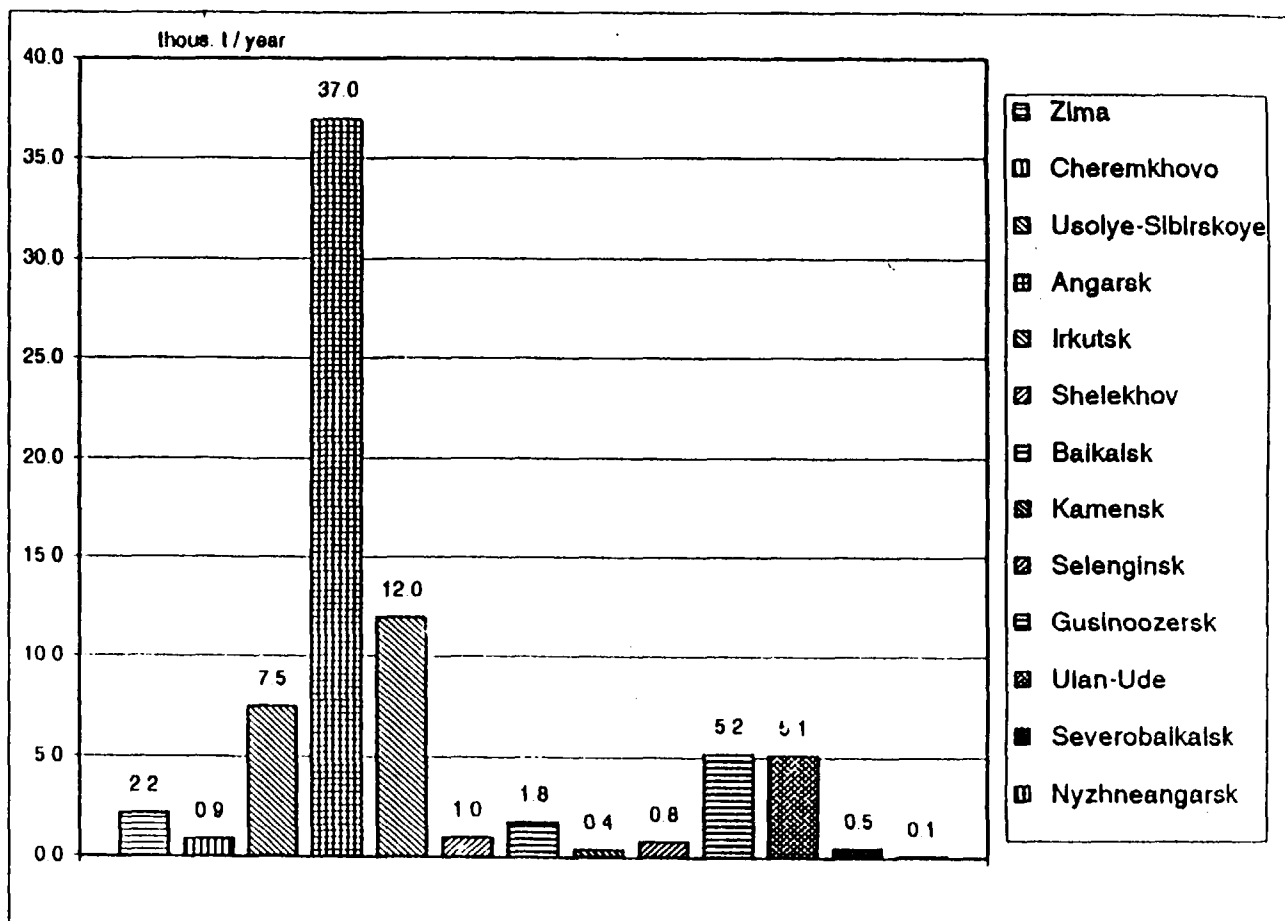
City	CO (thous.t/year)
Zima	4.9
Cheremkhovo	9.6
Usolye-Sibirskoye	55.2
Angarsk	102.0
Irkutsk	67.0
Shelkhanov	42.0
Baikalsk	0.8
Kamensk	5.8
Selenginsk	8.3
Gusinoozersk	2.8
Ulan-Ude	51.1
Severobaikalsk	7.6
Nyzhneangarsk	1.6



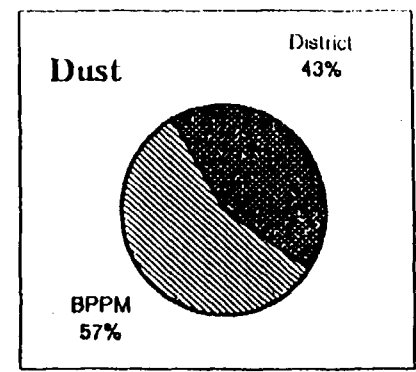
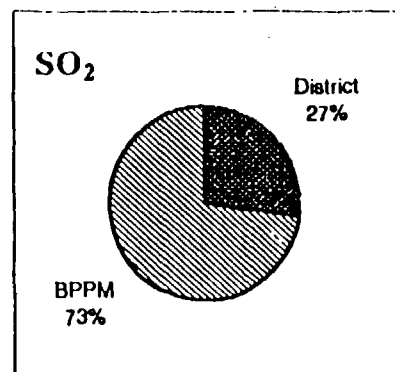
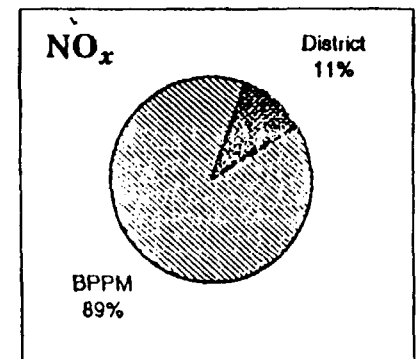
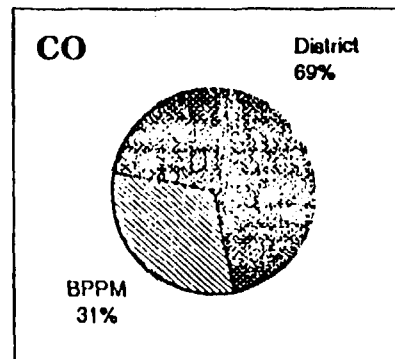
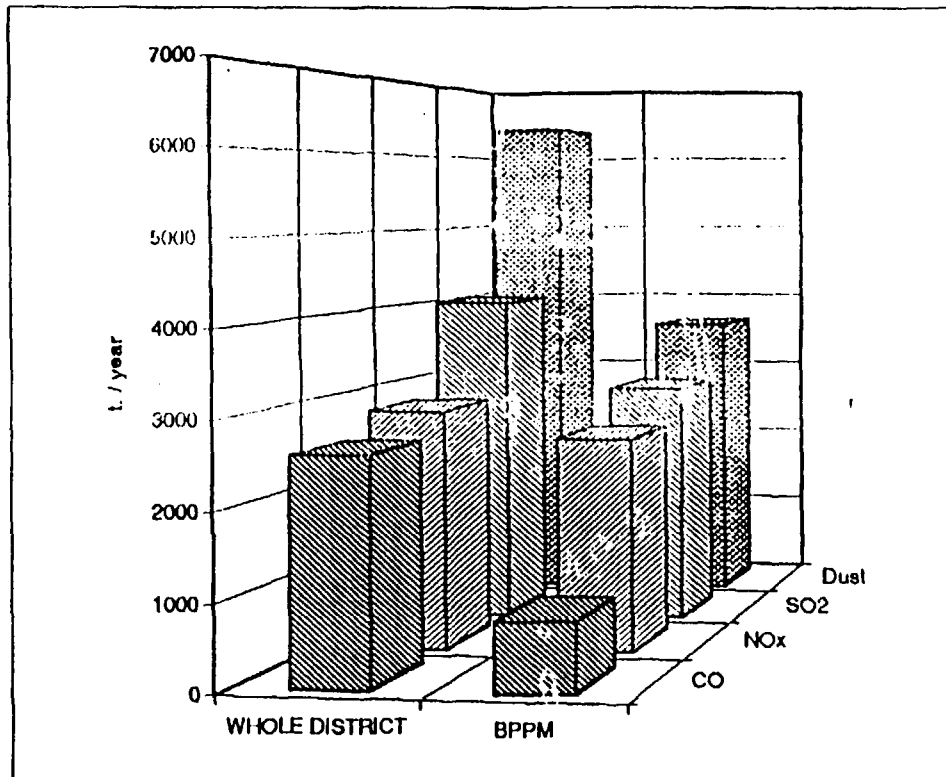
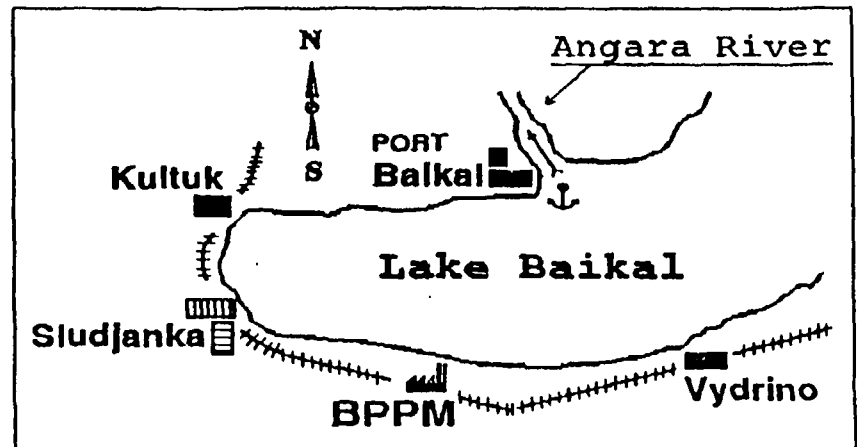
harmful substances discharges into atmosphere from automobile transport and stationary sources situated around Lake Baikal

NO_x (thousand t./year)

City	NO _x (thous.t./year)
Zima	2.2
Cheremkhovo	0.9
Usolye-Sibirskoye	7.5
Angarsk	37.0
Irkutsk	12.0
Shelekhov	1.0
Baikalsk	1.8
Kamensk	0.4
Selenginsk	0.8
Gusinozersk	5.2
Ulan-Ude	5.1
Severobaikalsk	0.5
Nyzhneangarsk	0.1



INGREDIENTS	FACT. DISCHARGES (t./year)	
	WHOLE DISTRICT	BPPM
CO	2598.334	811.501
NO _x	2863.58	2551.417
SO ₂	4066.196	2960.236
Dust	6392.795	3660.779
SOURCES NUMBER	391	104



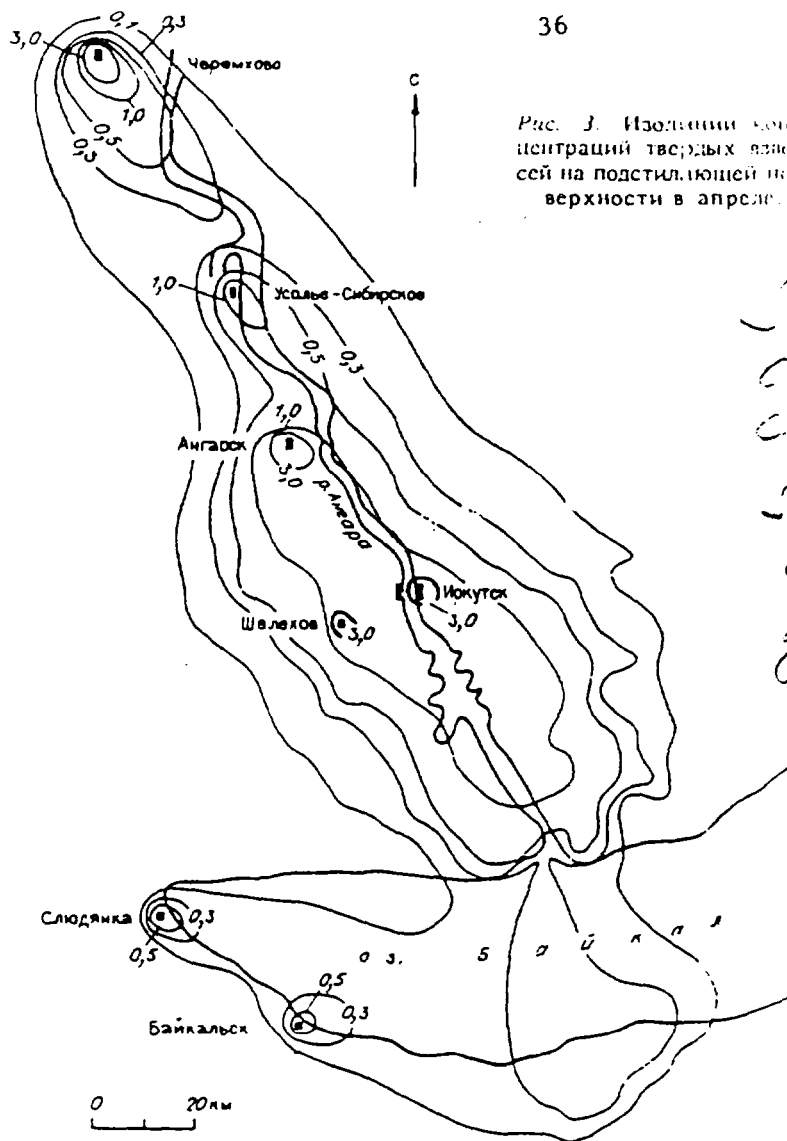


Рис. 3. Изолинии концентрации твердых взвесей на подстилающей поверхности в апреле.

*Sulfur dioxide
concentration =
curve, mg/m³
southern part
of Baikal Lake,
ground level*

ве, Усолье-Сибирском и Черемхове 25 км². Открытая поверхность Байкала загрязняется в основном предприятиями Слюдянки и Байкальска.

Следует отметить, что в качестве входной информации в расчетах использованы только данные о выбросах промышленных приподнятых источников. Пыление отвалов ТЭЦ и горно-рудных предприятий, выбросы жилищно-бытовых объектов и транспорта в данных расчетах не учтены.

Эксперимент 2. Задается характерное для северо-западного типа на Байкале ветровое поле по классификации [3], причем для лучшей аппроксимации ветра рассматриваются дополнительные пункты наблюдений (см. таблицу).

Поток твердых взвешенных частиц, подхваченный направленным северо-западным переносом, по долине Ангары устремляется в сторону Байкала (рис. 3, 4). Вблизи промышленных центров загрязненность уменьшается по сравнению с результатами расчетов эксперимента 1. Площади превышения значений максимальных разовых ПДК в Ангарске и Черемхове 25 км².

ANNEX 7.

Process descriptions and emission sources

TECHNICAL REPORT # 1070

Identification
of
dust and gas emissions into the air
from
technological units at Baikalsk P.P.M.

1. Introduction
2. Brief technical characteristics of production line.
 - 2.1. Technological emission sources of cooking-washing plant.
 - 2.2. Technological emission sources of bleaching plant
 - 2.3. Technological emission sources of bleaching chemicals plant.
Chlorine dioxide preparation.
 - 2.4. Technological emission sources of lime caustisation and recovery plant.
 - 2.5. Tall oil production.
 - 2.6. Technological emission sources of mechanical-repairing plant.
 - 2.7. Technological emission sources of drying plant.
 - 2.8. Technological emission sources of vaporation plant.
 - 2.9. Technological emission sources of Heat & Power plant.
 - 2.10. Technological emission sources of sewage water treatment plant.
 - 2.11. Technological emission sources of sediment treatment plant.
3. Preparation works.
4. Production line inspecting.
5. Conclusion & recommendations.

Annexes.

- I. Protocol on works starting.
- II. Technical protocol on works completion.

1. Introduction.

Works on identification of dust-gas emissions into the air from technological equipment of Baikalsk P.P.M. were made on the basis of Agreement # 26-50 dd on Nov. 10. 1889 since Jan. up to Dec. 1990.

The inspection of emissions was made from the equipment of cooking-washing plant, vaporation plant, bleaching plant, drying plant, lime caustisation & recovery plant, by-products plant, bleaching chemicals plant, sediment treatment plant, mechanical-repairing plant, sewage water treatment plant, Heat & Power plant.

Pulp cooking is realised by two stages. At the first stage (redhydraulisys) acute steam ($t = 200$ Celcium degrees) is loaded into the digester (#4) charged by chips (Fig.1). During the process of hydraulisys in the digester are formed fumes of: turpentne, methyl alcohol, volatile organic substances, and also steam and air, resting after the digester loading. The presence of gasforming products creates surplus pressure in the digester, so reaching 100 Celcium degrees a turpentine blowing is made. The blowing is made continiously up to the end of hydraulisys. Blowing gases are moved to alkali separator (5), the gass coming through filters are moved for cooling into heat exchangers (6).

Water-turpentine emulsion (gases condensated in heat exchangers) are moved to turpentine section, non-condensated gases are emmitted into the air. At the end of cooking (3 - 3,5 hours later) pulp mass is blowed out from the digester. For heat saving, emitted as blowing steam is used a Rosenblad system unit.

Blowing steams coming throug "Gethner" trap unit are moved into jet condensator (9), where cooled water is fed, which forms condensate while mixing with blowing steam. Non-condensated steams and air are removed from tank-accumulator into the air. There is a steam removing line moving gases to gas-washing tower.

2.2 Technological emission sources of bleaching plant. (Fig.3;4)

Main technological process of pulp bleaching is taking place in tower of continious action of "Kamur" system. Pulp washing after each bleaching stage is made in "Rauma-Repola" vacuum-filters. Screened, washed and diluted in vacuum-filter "A" pulp is moved into fiber storage tower Б-1, where fresh water is added. From the tower pulp comes inyo mixer IB, where it is mixed with chlorine, and then it is moved to chlorination tower, after which pulp is washed in vacuum-filter I and moved to the second bleaching stage. Caustic is moved into vacuum-filter screw. After that pulp is moved into tank 1Б through the mixer 2B, washed in vacuum-filter 2 and moved to the third (sodium hypochlorite) bleaching stage. The fourth (hot alkalinity) bleaching is started at vacuum-filter 4a screw. Pulp washed in mixer 4B comes to vacuum-filter 5, where starts the fifth (chlorine dioxide treatment) beaching stage. Sodium hypochlotite is added to the pulp washed in vaccum filter (6). To nuetralize the balance chlorine, extract mineral dashes and stabilize brightness is made the final bleaching stage in vacuum-filter 7 (oxidizing by sulphur dioxide). Vacuum-filters are covered by caps. Steam-gas mixture from the caps is pumped out by fans and discharged into the air.

The works goals: numerical identification of harmful substances, emitted into the air from technological equipment and ventilation systems of the mill.

The staff of inspection team:

N. Antooshev - I category engineer;
 A. Shmelev - II category engineer;
 I. Radaeva - II category engineer;
 N. Korikova - engineer;
 M. Gryaznova - lab. assistant;
 A. Antoosheva - technician.

The given report gives data for 1990.

2. Brief technical characteristics of production line.

The main product manufactured by Baikalsk P.P.M. is cord sulphate pulp, meeting TY-81-04-468-76, on the first technological line, and sulphate viscose pulp, meeting TY 81-04-346-75, on the second technological line. Production capacity of Baikalsk P.P.M. are designed to produce 280 000 tons of pulp annually.

Besides the main product - pulp, the mill fabricates tall oil, raw turpentine, wrapping paper.

2.1. Technological emission sources of cooking-washing plant.(Fig. 1;2)

Pulp cooking is made with the help of sulphate method from soft & hard wood species in 24 stationary digesters of periodic action with volume of 140 c.m. each.

The process of sulphate pulp cooking is followed by forming of considerable amounts of sulphur compositions, such as sulphur hydrogen, methylmercaptane, dimethylsulphide, dimethyldisulphide and also methanol, turpentine and other compositions.

The presence of bad-odour compositions in steam-gas emissions of cooking plant is determined by the presence of sodium sulphide in cooking liquor and methoxyl groups in wood. The formation of sulphur content compositions is influenced by the following technological parameters of the cooking process: sulphidity of the cooking liquor, concentration of active alkali, temperature and time of cooking, wood specie.

2.1.1. Cooking plant.

2.3. Technological emission sources of bleaching chemicals plant.

2.3.1. Chlorine dioxide preparation (Fig.5;6).

The plant is fabricating liquid chlorine dioxide. with the help of Matisson method. Plant capacity - 1600 t/y.

The main reaction of chlorine dioxide obtaining is taking place in reactor #2, where sulphuric acid and 50% solution of sodium chlorate is fed continuously. To the lower part of reactor 2 is fed sulphur dioxide diluted by air, which coming up is reacting with sodium chlorate forming chlorine dioxide. $2\text{NaClO}_3 + \text{SO}_2 = 2\text{ClO}_2 + \text{Na}_2\text{SO}_4$.

The mixture of chlorine and chlorine dioxide coming out from the upper part of the reactor is moved into absorption tower 3, filled by Rushig coils. In absorption towers chlorine dioxide is diluted in the water and moved into storage tanks. Gases not absorbed in the towers are discharged by fans into the air.

2.4. Technological emission sources of lime caustisation and recovery plant. (Fig. 7;8)

At lime caustisation and recovery plant white liquor preparation and sludge recovery is taking place. White liquor preparation is made by continuous method. Plant capacity - 340 c.m./day of white liquor with concentration 110 g/l of active Na_2O . As a result of sodium carbonate caustisation reaction 80-90% of green liquor transits into calcium hydroxide and turns into calcium carbonate (lime sludge). This process is taking place in slake-classifiers 2, where white liquor and lime is moved. The obtained suspension is decolorized in devices of sedimentation type 4. Decolorized liquid (white liquor) is moved into storage tanks 12, and sediment (lime sludge), passing through additional causticators 5, it is washed in washer 6, condensed in vacuum-filters up to 60 % and moved into rotating lime regeneration kilns. To restore losses of lime crushed lime stone is added into kiln. As a result of lime sludge and stone burning at temperature 1100 - 1200 Celcium degrees lime is formed, which is moved for green liquor caustisation.

2.5. Tall oil production. (Fig. 9;10)

Sulphate soap, coming from tank facilities of vaporation plant, after precipitation in tanks 1;2, is pumped into reactor 4, where sulphuric acid at concentration 30 - 40% and water is added. After heating precipitation

part of liquid is pumped out, sulphate soap is added and starts the main cooking, steam feeding is increased.

Formed tall oil is moved into dryers 5, where drying is taking place with the help of steam, and reactionary bad-odour gases, containing sulphur hydrate and methylmercaptain, coming through rotorclone, sprinkled by weak white liquor, are discharged by fan into the air. Harmful gases annual emission into the air is calculated for equipment operation during 345 days. Ventilation from pos. 1;2;3;5 - natural type.

2.6. Technological emission sources of mechanical-repairing plant. (Fig.11;12)

Air polluting sources at mechanical-repairing plant are electric arc hating furnaces, press for plastic masses, lumber and grinding devices. Metal melting is taking place in electric arc furnace, in heating furnace metal articles are heated up to necessary temperature for further hardening or tempering. The furnaces are covered by caps. Dust-gas mixture is emitted into the air by fans. For welding works a special, site is made, gas pumping out is made by fans.

Wooden and metal dust removing from lumber and grinding devices is made by fan. For air treatment are installed cyclones 5;6.

2.7. Technological emission sources of drying plant. (F. 13;14).

Bleached and washed stock is moved onto mesh part of paper machine, where pulp linen is formed, which after pressing comes for drying. During the drying process great amount of water is vaporated, which is necessary to be removed from caps of drying cylinders. Air exchange is made with the help of air-intake fan unit with utilization of heat of the outgoing air. Moisture saturated air is emitted into the air.

2.8. Technological emission sources of vaporation plant.(Fig.15;16)

At vaporation plant black liquor is vaporated at for six-body vacuum-vaporation station I -VI. Capacity of each station at vaporated water is 100 t/h. To the body I heating steam is moved. Vaporation in the following bodies is made on account of recycling steam heat. At body VI vacuum is kept 530 mm mercury post on account of clean steam condensation in barometric condensator 15 and sucking out non-condensed gases by vacuum pump. Condensate from body V and VI is purified from sulphur content compositions at dezodoration unit 11, to the lower part of which condensate (up to 400 c.m./h) and air (up to 2000 c.m./h) is moved. Gas-steam mixture, formed in the unit is emitted into

the air. Gas-steam mixture from the pit of bad odour gases is discharged into the air. Gas-steam mixture from tank facilities also is discharged into the air.

2.9. Heat & Power Plant technological emissions (Fig. 17; 18).

The main emission sources of HPP are soda recovery boilers; bark boilers, power boilers, melted soda tank collectors. At soda recovery section takes place burning of condensed black liquor, coming from vaporation plant.

Mineral part in the form of melted soda comes from the melted soda tank collector 2, where weak white liquor is added for melted sode dilution. After boilers smoke gases are treated in electric filters 4 (dust (sulphate) removing) , and then by smoke sucker 13 they are moved to the second treatment stage - deezodoration-smoke unit 5, at which additional treatment of smoked gase from dust, sulphur conent compositions - sulphur hydrate, sulphureous gas, methylmercaptane takes place.

Traetment in DDU is made with the help of caustic solution, coming from bleaching chemicals plant.

Steam-gas emissions from melted soda tank-collectors passing through heat exchangers are discharged into the air.

In heavy fuel - bark boilers 7 bark is burnt. Smoke gases are treated in scrubber MC-BTU 8. Water is used as sprinkling liquid. After scrubber treated gases are discharged by smoke sicker 13 to the pipe 9 . Power boilers are designed for coal burning for steam obtaining, used for technological needs and elctric power production. Smoke gases after the boilers are treated in electric filters 11(dust removing), and discharged by smoke sucker 13 into smoke pipe 12.

2.10. Technological emission sources of sewage water treatment plant. (Fig.19)

Sewage water treatment plant was deisigned for treating industrial waste waters and sewage waters. After biological and chemical treatment in sedimentation ponds waste waters are discharged into lake Baikal. Design capacity of the plant is 269000 c.m.

Biological and chemical treatment.

Waste waters are moved to the mixer-nuetralizer 1, in case of necessaty - to alarm discharge pond, where waste water neutralizationis made with the help of sulphuric acid up to pH 6,5 - 7,5; after this it comes to average- preaerator, where waste water averaging and gas blowing (

sulphur hydrate methylmercaptane dymethylsulphide) takes place. From the averager through the distribution channel waste waters are distributed in four channel aerotanks 5, where air is added. Coming through all channels, water comes to the channel of silt mixture, and then to sedimentation ponds 8. After sedimentation silt is moved to the reservoir of active silt.

Biologically treated waste water after sedimentation ponds 8 is moved into mixer 9, where aluminium sulphide and polyakriamide is added and through distribution chamber 10 is distributed among sedimentation ponds. Formed sediment from sedimentation chamber is moved into sediment treatment plant.

2.11. Technological emission sources of sediment treatment plant. (Fig.20;21)

At sediment treatment plant is made sediment extraction and dewatering with further partial transporting out or burning. The plant consists of head flotation section, dewatering section, drying and burning section.

The initial raw for flotation is sludge lignin coming from chemical treatment sedimentation ponds. The dewatering process by the method of head flotation is concluded in extra pressure air charging of sludge lignin. The air balls float the particles of sludge lignin to the water surface, at which a foam layer is formed. To increase dewatering efficiency flocculants-polyacriamide is used with the help of which small particles of sediment are enlarged. The final product of head flotation is flotsludge, which is moved into section of mechanical dewatering on centrifuges. The final product of this section is dewatered flotsludge coming for drying and burning to fluidised bed furnaces and filter. The main emission source is fluidised bed furnaces for sediment burning.]

3. Preparation works.

During preparation works technological process and documentation was studied, determined the points of samples taking, connecting pipes for sample taking and gas streams measuring were joined.

Dust content in gas was determined according to isokinetic method of inner filtration with allonges using 2.

Flow speed measuring was made on methodics, based on taking speed areas by pneumatic pipe type НИИОГАЗ (NIIOGAS), measured dynamic gas pressure, proportional to square of this speed. The amount of dynamic pressure was measured by micri manometer type ММН-240/1/.

Sulphur anhydride content was determined by photoloric method with phucsin phormaldehyde reactive agent /3/.

Sulphur hydrate was determined by the method of potentiometric titration /3/.

Methylmercaptane, dimethylsulphide, dimethyldisulphide, was measured by the method of chromatography analysis /7/.

Turpentine was determined by the method of gas chromatography /1/.

Chlorine dioxide was determined by titrometric method, based on interaction of chlorine with potassium iodide.

Chlorine was determined by photocolometric method by iodine-starch reaction /1/.

Nitrogen oxides were determined by the method, based on interaction of nitrite-ion and p-aminobenzosulphuric acid /1/.

Carbon oxide concentration was determined with the help of device ГХ-4.

Alkaline aerosols were determined by the method based on acid-alkaline indicators capability to change color depending on pH medium /5/.

Phenol was determined by photometric method with 4-aminoantipirin /6/.

During the works were used the following devices and instruments:

- pneumometric & dust-intake pipes
- micromanometer, type MMH-240
- U-shape draught-pressure meters
- manual anemometers, wing type & cup type
- fir aspirator AM-3 & electric aspirator
- timer
- portable universal gas analyser, type УГ-2
- photoelectrocolorimeter ФЭК-М
- pH-meter, millivoltmeter
- laboratory balance
- sample taking of gas-dust emissions was made with the help of electric aspirator, water aspirator, air ejectors
- ГХ-4.

4. Production line inspection

The results of determination of harmful substances emission into the air from technological units of Biakalsk P.P.M. are given in Table 1 - 3. For each emission source were made from five up to ten measurements with two-three parallel samples at each measuring. From obtained results were chosen the minimum and maximum values, and then the average value was calculated.

The amount of emissions per year was calculated taking into consideration actual operational time of equipment.

The working time fund for heating and electric arc furnaces, plastic casting presses, welding sites, cyclones and grinding devices in Mechanical - Repairing Plant is 4 hours/day (345 days a year). for reactors of sulphate soap destructuring plant - 3 - 6 hours a day (345 days a year), for soda recovery, power, bark boilers of Heat & Power Plant - 24 hours a day (300 days a year). The rest inspected effluent sources are calculated coming from the length of equipment operation as 3435 days a year, 24 hours a day.

Newly formed emission sources are numbered from No. 400.

Lime recovery kiln: annual emission calculated from actual operation time - 7504 h/y.

Emission determination from technological units of sewage water treatment plant was made by methodics, designed by УФНИИ-гигиена /15/. The wind speed was determined by slow moving of wing anemometer on the whole square of the conventional cross-cut (at the outflow from the pond).

Air consumption, coming under the pond is determined by formula

$$\alpha = 3600 \times V_1 \times S_1,$$

where V_1 - wind speed, m/sec,

S_1 - conventional cross cut, sq.m.

For the height of conventional cross cut was taken the level, at which harmful substances concentration is equal the concentration of background pollution.

While determining the conventional cross cut for mixer-neutralizer, distribution channels and sedimentation ponds, coming out from wind rose, was taking their length, and for other water ponds - their width.

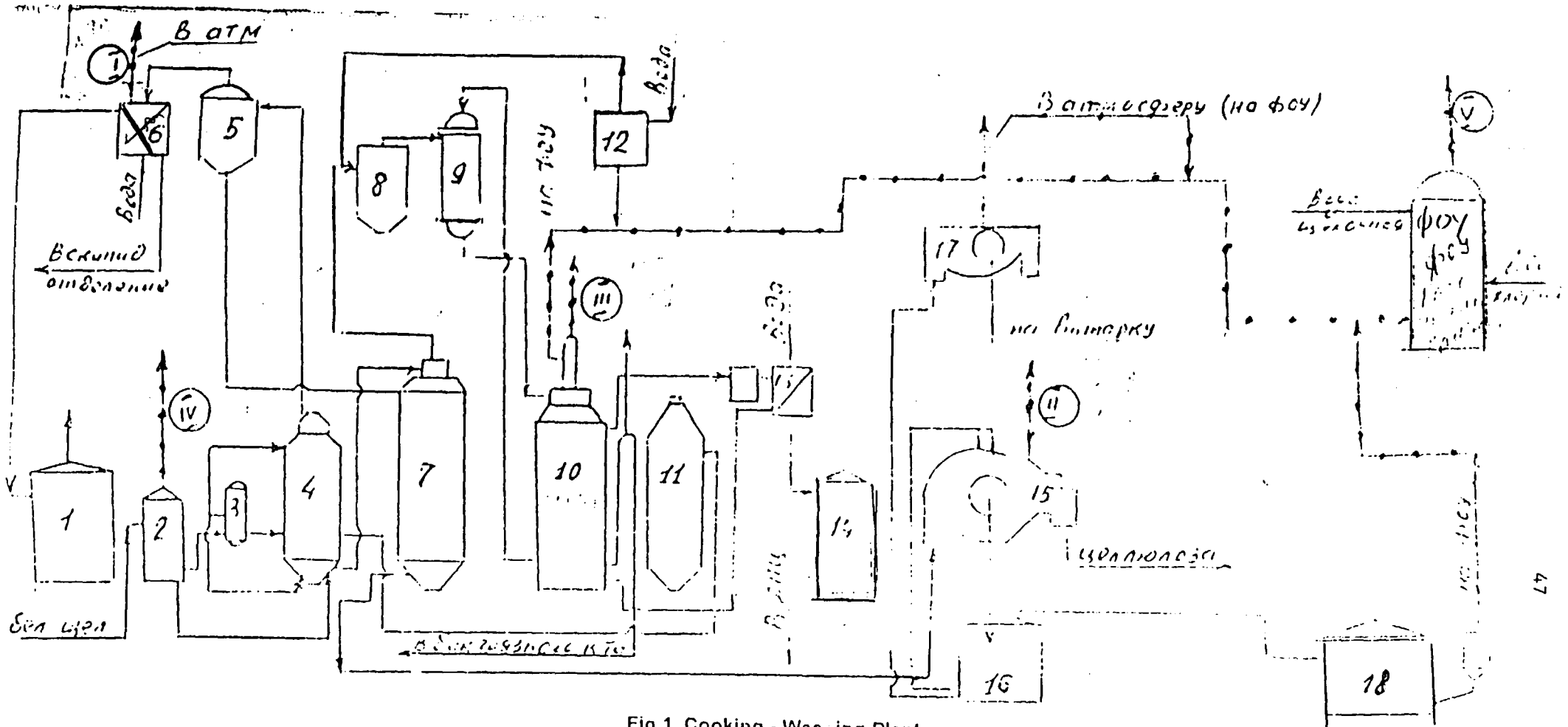


Fig.1. Cooking - Washing Plant

- | | | | | | |
|-----------------------|---------------------------------|--------------------------|-----------------------------|-------------------------------|----------------------------------|
| 1 - Warm water tank | 2 - White liquor measuring unit | 3 - Caloriser | 4 - Digester | 5 - Liquor separator | 6 - Blowing gases heat exchanger |
| 7 - Blowing reservoir | 8 - Getner trap | 9 - Jet condenser | 10 - Accumulation tank | 11 - Hydraulisate tank | 12 - Mixing deck condenser |
| 13 - Heat exchanger | 14. Hot water tank | 15 - Black liquor filter | 16 - Weak black liquor tank | 17 - Weak black liquor filter | 18 - Foam collecting tank |
- ΦΟΥ - gas washing tower
 I - Emission sources No.90; II - No.122, 134; III - # 153, 157; IV - # 401 V - # 135, 136;

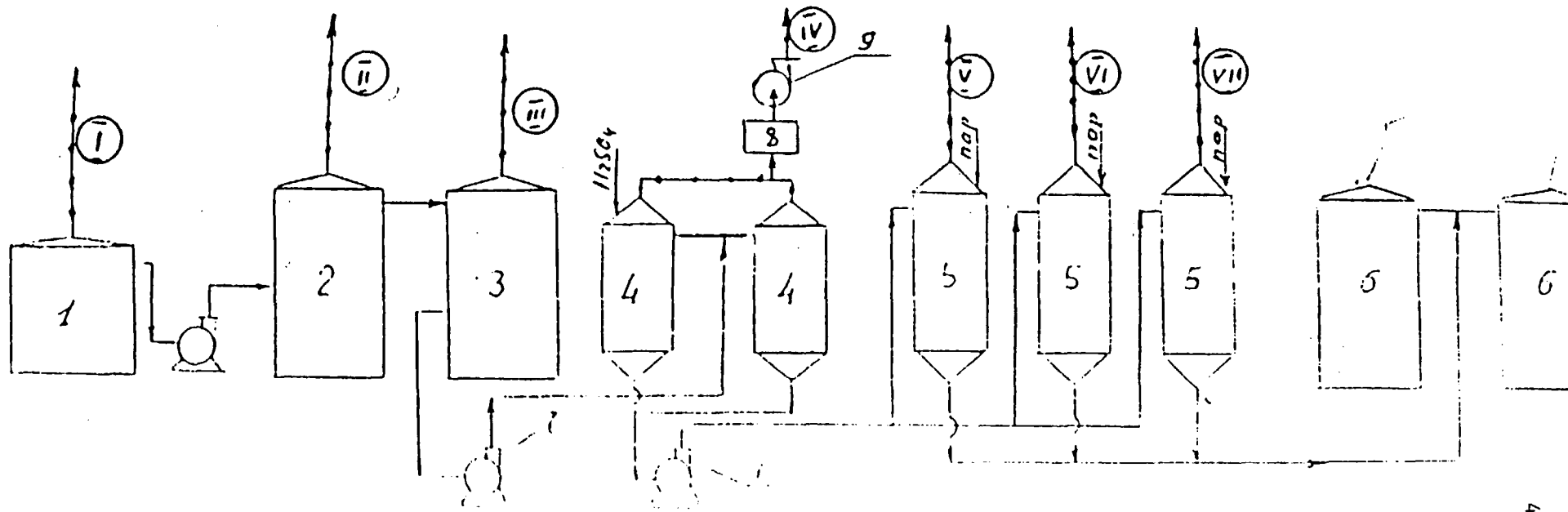


Fig.9. Tall oil production principle technological scheme.

- 1 - receiving tank 2 - Sedimentation tank 3 - Raw soap dosator 4 - reactor 5 - Tall oil washing & drying unit 6 - Tall oil storage tank 7 - Pump
 8 - Rotoclone 9 - Fan I - Emission source into the air #.413, II - #414 III - # 415 IV - # 213 V - # 410 VI - # 411 VII - #412

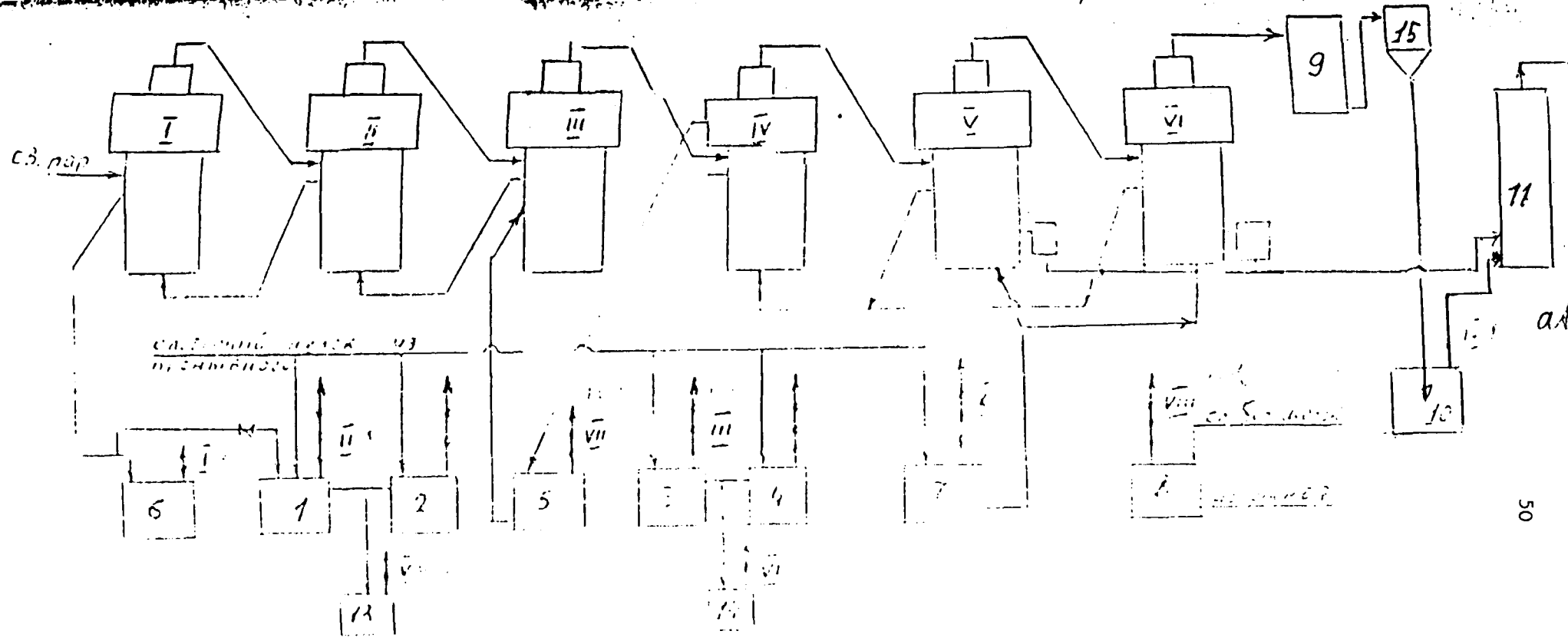


Fig.15. Vaporation Plant principle scheme.

- I, II, III, IV, V, VI -vaporation stations bodies 1, 2, 3, 4 - weak liquor tanks 5 - semi-vaporated liquor tank
 6 - weak liquor tank 7 - feeding tank 8 - weak white liquor tank 9 - surface condenser
 11; 12 - Condensate dezodorization unit 13, 14 - Soap tanks #1; #2. 15 - jet condenser 10 - Ordour gases pit
 I; II - Emission source into the air # 215,216 III - # 217 IV - # 230 V; VI - # 105; 106 VII - # 104 VIII - # 214 IX - # 231 X - # 220

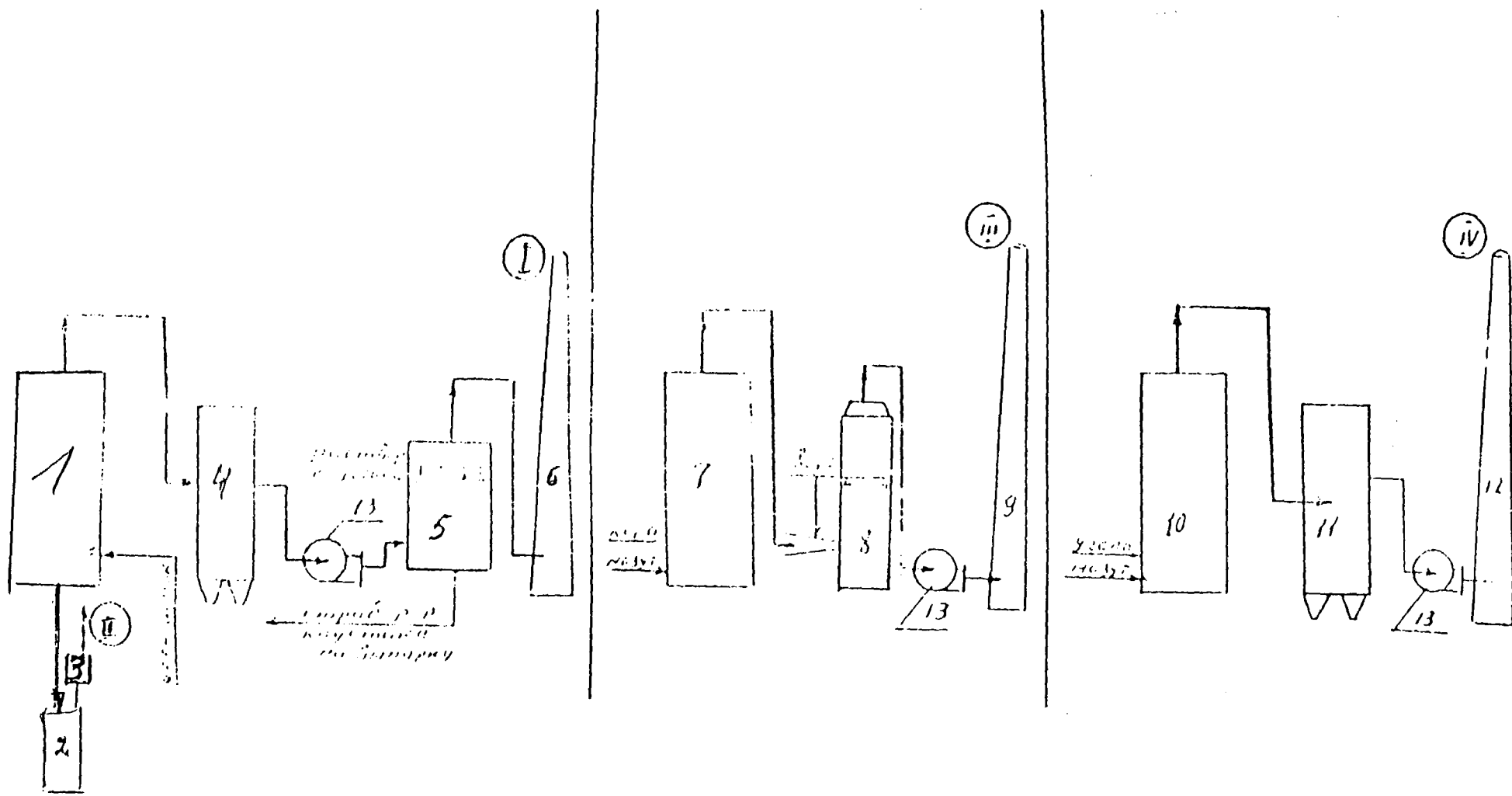


Fig.17. Principle scheme of emission into the air from the technological equipment of Heat & Power Plant .

- 1 - Soda recovery boiler unit
- 2 - Melted soda tank
- 3 - heat exchanger
- 4 - electric filter
- 5 - Dezodoration smoke unit
- 6 - chimney of SRB
- 7 - Heavy fuel bark boiler
- 8 - Scrubber MC-BTI;
- 9 - Chimney of bark boiler
- 10 - Power boiler
- 11 - el. filter
- 12 - Power boiler chimney
- 13 - Smoke sucker.
- I - Emission source into the air # 240
- II - # 92 - 95; 229
- III - # 221
- IV - # 222

III, Gas treating and dust removing units operational indicies.

Emission source name & its number	Gas treating and dust removing units			Treated harmful substances	Providing co-efficient		Harmful substances concentration	
	Total	Defective	Non-effective		normative. %	actual, %	before	after
							treatment, g/c.m.	treatment, g/c.m.
1	2	3	4	5	6	7	8	9
Electrofilters plus deodorization of soda recovery boilers, 1-5(240)	8 + 4	1		dust SO2 MM	100	100	8,32 0,05 0,0004	0,764 0,0003
Power boilers electrofilters (222)	5			H2S dust	100	100	0,1081 11,6001	0,0744 0,336
Ventury scrubbers of bark boilers (221)	2			dust SO2	100	100	0,4229 0,12	0,089 0,0007
Melted soda tank-collector dezodoration CPK-1 (92)	1			dust H2S MM	100	100	3,7133 0,425 0,0064	0,557 0,085 0,0032
Melted soda tank-collector dezodoration CPK-2 (93)	1	+		H2S dust	100	100	0,1188 0,629	0,1188 0,629
Melted soda tank-collector dezodoration CPK-3 (94)	1			H2S dust MM	100	100	0,31 0,91 0,0136	0,087 0,546 0,0068
Melted soda tank-collector dezodoration CPK-5 (229)	1			H2S dust MM	100	100	0,132 0,6988 0,00341	0,0665 0,571 0,00341
Lumber units cyclone (223)	1			dust	100	100	2,6425	0,061
Grinding units cyclone (224)	2			dust	100	100	0,89	0,089
Rotoclone (213)	1			H2S Стр. MM	100	100	3,1711 0,0953	0,469 0,0073

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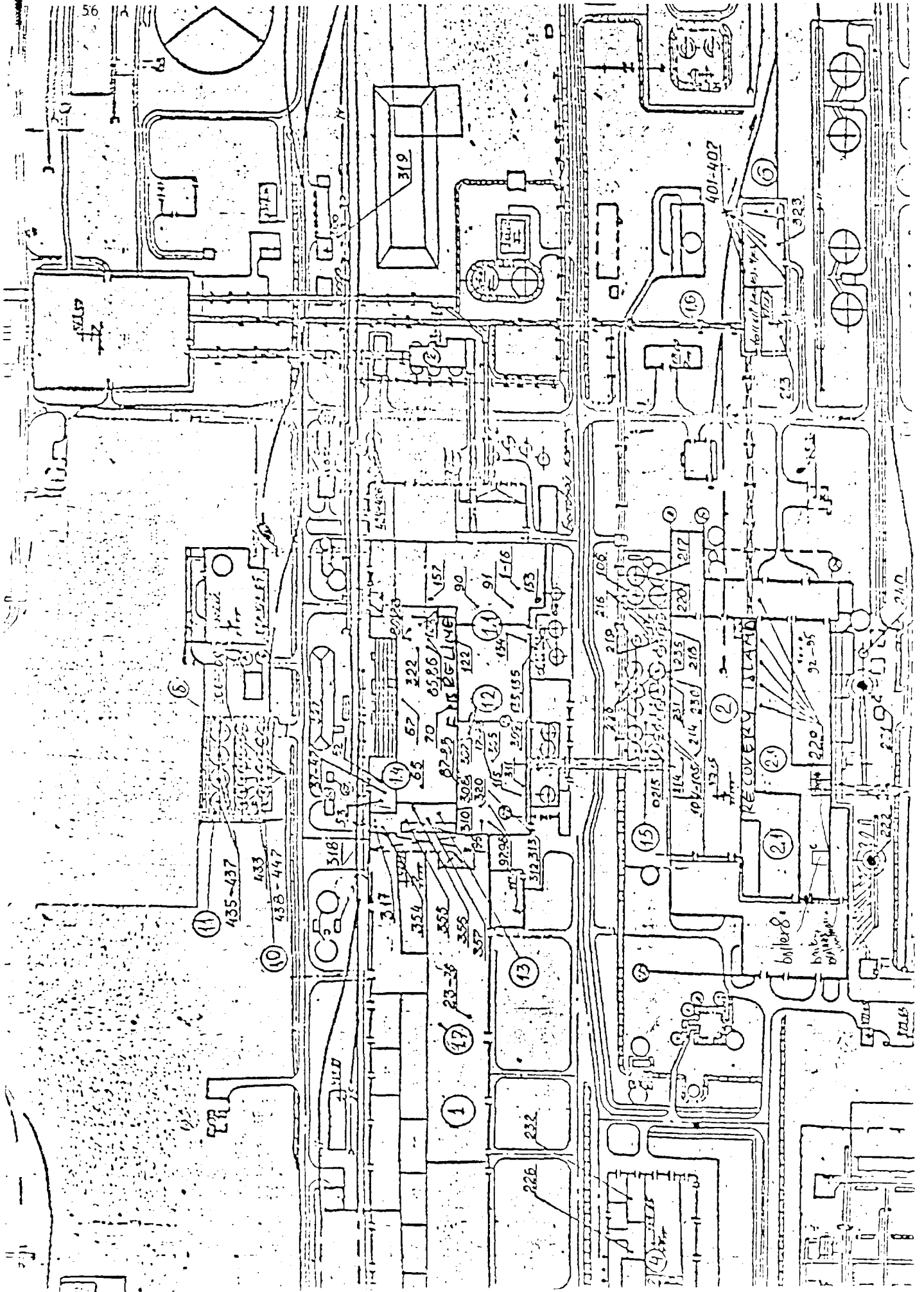
1	2	3	4	DMDS	6	7	0,0159	0,0013
1	2	3	4	5	6	7	8	9
Scrubber at chlorine dioxide tower (87)	2			DMS	100	100	0,0027	0,0078
				ClO2			1,1058	0,3292
Scrubber at chlorine dioxide tower (88)	2			ClO2	100	100	1,3678	0,0324
Scrubber at lime kilns (62)	2			dust	100	100	18,2015	0,9206
				H2S			0,288	0,2147
				SO2			0,111	0,0788
Hose filter at sulphate storage (323)	3			dust	100	100	5,42	0,271
Gas-washing tower (135)	1			H2S	100	100	0,4349	0,08
				MM			0,0732	0,064
				DMS			0,6739	0,017
				DMDS			none	none
				turpentine			2,1317	0,55
Gas-washing tower (136)	1			phenol	100	100	0,0067	0,0045
				phenol			0,0189	0,0063
				H2S			1,665	0,0332
				MM			0,1592	0,0425
				DMS			0,0226	0,0104
				DMDS			none	none
				turpentine			0,522	0,323
Scrubber at fluidized bed furnaces (300)	2			SO2	100	100	3,58	0,1795
				dust			18,5	0,367
Cyclone at lime conveyor(407)	1			dust	100	100	5,252	1,4945
Cyclone at lime conveyor(103)	1			dust	100	100	3,905	2,488

**IV. Total emission amount of effluent substances into the air,
its treatment and utilization, t/y**

Effluent name	Amount of effluents, coming from all pollution sources	including: emitted without treatment	From those moved for treatment					Totally emitted into the air	Caught & deharmed in % ratio to total amount	
			Moved to treatment system	Emitted into the air	Caught & deharmed				Plan	Actual
					Plan	Actual	Utilized			
A	1	2	3	4	5	6	7	B	C	D
TOTAL	151550,163 (cln.2 + cln.3)	5660,147	145890,011 (cln4 + cln6)	8126,607		137763,404	11396,1117	13786,754 (cln.2 + cln.4)		(cln.6 x 100 / cln.1) 90,9
including:										
solids (non-ordanic dust)	142555,409	112,352	142443,057	7322,598		135120,459	11127,471	7434,95		94,8
gaseous & liquid from them:	8994,754	5547,705	3446,954	804,009		2642,945	268,6407	6351,804		29,4
SO2	4657,279	2161,871	2495,408	258,934		2236,474	0,687	2420,805		48
H2S	908,154	82,202	825,952	518,379		307,573	249,24	600,581		33,9
Methylmercaptane	138,454	131,003	7,451	4,314		3,137	0,898	135,317		2,3
Dimethylsulphide	60,501	37,039	23,462	0,598		22,864	0,0447	37,637		37,8
Dimethyldisulphide	39,726	39,404	0,316	0,005		0,311	0,311	39,409		0,8
Turpentine	101,232	26,956	74,276	19,231		55,045		46,187		54,4
Nitrogen oxides	1974,02	1974,02						1974,02		
Carbon oxide	1076,165	1076,165						1076,165		
Alkaline aerzoles	14,034	14,034						14,034		
ClO2	21,341	1,491	19,85	2,39		17,46	17,46	3,881		81,8
Clorine	3,085	3,085						3,085		
Phenol	0,763	0,524	0,239	0,158		0,081		0,682		10,6

ANNEX 8.

The lay-out of the Mill and air emission sources



ANNEX 9.

Sulphur emissions in 1994

SULFUR EMISSIONS IN 1994, PRODUCTION 120 253 ADt

SOURCE	TREATMENT	VENT	FLOW nr	SO2 kgS/ADt	TRS kgS/ADt
STRONG ODOR GASES					
Cooking plant: *Accumulator tanks *Foam collect. tank *Brown stock filters		Stack 30m	153,157		1,432
	Relief gas	Alkaline Scrubber			
	Vent gas	Pipe	135,136		0,103
	Vent gas	Pipe			
		Pipe	122,134		0,001
*Turpentine recov.	Relief gas	Pipe	90		0,018
*Prehydrolysate tank	Vent gas	Pipe			0,004
Evaporation plant	Relief gases, hot well				
	Foul condensate	4 catalytic scrubbers, air:condensate 10:1			
		Pipe	231		0,000
WEAK ODOR GASES					
Cooking plant	Vent gas from white liquor dosing tank	Pipe	401		0,000
Tall oil preparation	Reactor gases	Rotoclone scrubber			
		Pipe	213		0,011
Evaporation plant:					
*Weak B.L tanks	Vent lines connected from 6 tanks	Pipe	217		0,024
*Strong B.L tanks	Vent lines connected from 4 tanks	2 pipes	215,216		
*Med. B.L.tanks	Vent lines connected from 5 tanks	Pipe	104		
*Weak W.L. tanks	Vent lines connected from 2 tanks	2 pipes	424,409		
*Strong W.L. tanks	Vent lines connected from 2 tanks	Pipe	214		
OTHER SULFUR CONTAINING PROCESS WASTE GASES					
Recovery boiler dissovvers	Vent gases	4 Heat exchangers			
		4 Stacks	92...95		0,088
2 Lime kilns	Flue gases	2 Alkali scrubbers 1 Emulgator reactor			
		Stack 60m	62	0,06	0,352
Bleaching plant	Vent gases from tower	Pipe		0,02	
Other miscellaneous sources: *Cooking plant *Sludge processing *W.water tr. plant *Storages				0,06	0,363

SULFUR EMISSIONS IN 1994, PRODUCTION 120 253 Adt

SOURCE		TREATMENT	VENT	FLOW nr	SO2	TRS
					kgS/ADt	kgS/ADt
FLUE GASES FROM BOILERS						
Recovery boiler 1	Flue gas	Electr. precipitator	Stack 120m	240	0,16	0,117
Recovery boiler 2	Flue gas	Electr. precipitator				
Recovery boiler 3	Flue gas	Electr. precipitator	Stack 120m	221	0,55	0,110
Recovery boiler 4	Flue gas	Electr. precipitator				
Bark boiler 5	Flue gas	Cyclones+scrubber			0,00	
Bark boiler 6	Flue gas	Cyclones+scrubber				
Coal power boiler 7	Flue gas	El.precip.				
Coal power boiler 8	Flue gas	Desulfurization Lifac				
Coal power boiler 9	Flue gas	El.precip.	Stack 120 m	222	11,44	
Coal power boiler 10	Flue gas	El.precip.				
Coal power boiler 11	Flue gas	El.precip.				
Efluent sludge boiler	Flue gas	Cyclones and scrubber	Stack 120m	300	0,03	
Efluent sludge boiler	Flue gas	Cyclones and scrubber				

TOTAL SULFUR EMISSIONS:

SULFUR EMISSIONS FROM HEAT GENERATION TO BAIKALSK CITY:

TOTAL SULFUR EMISSIONS OF MILL OPERATIONS:

Recommended level in Finland:

New permits in Finland:

SO2+TRS	SO2	TRS
kgS/ADt	kgS/ADt	kgS/ADt
14,93	12,31	2,624
	-1,60	
13,33	10,71	2,624
2,00		
1,5..2,0		

TRS emissions from strong odor gases

TRS emissions from weak odor gases

TRS emissions from recovery boiler dissolver tanks

TRS emissions from the lime kiln

TRS emissions from miscellaneous sources

TRSEmissions from recovery boilers

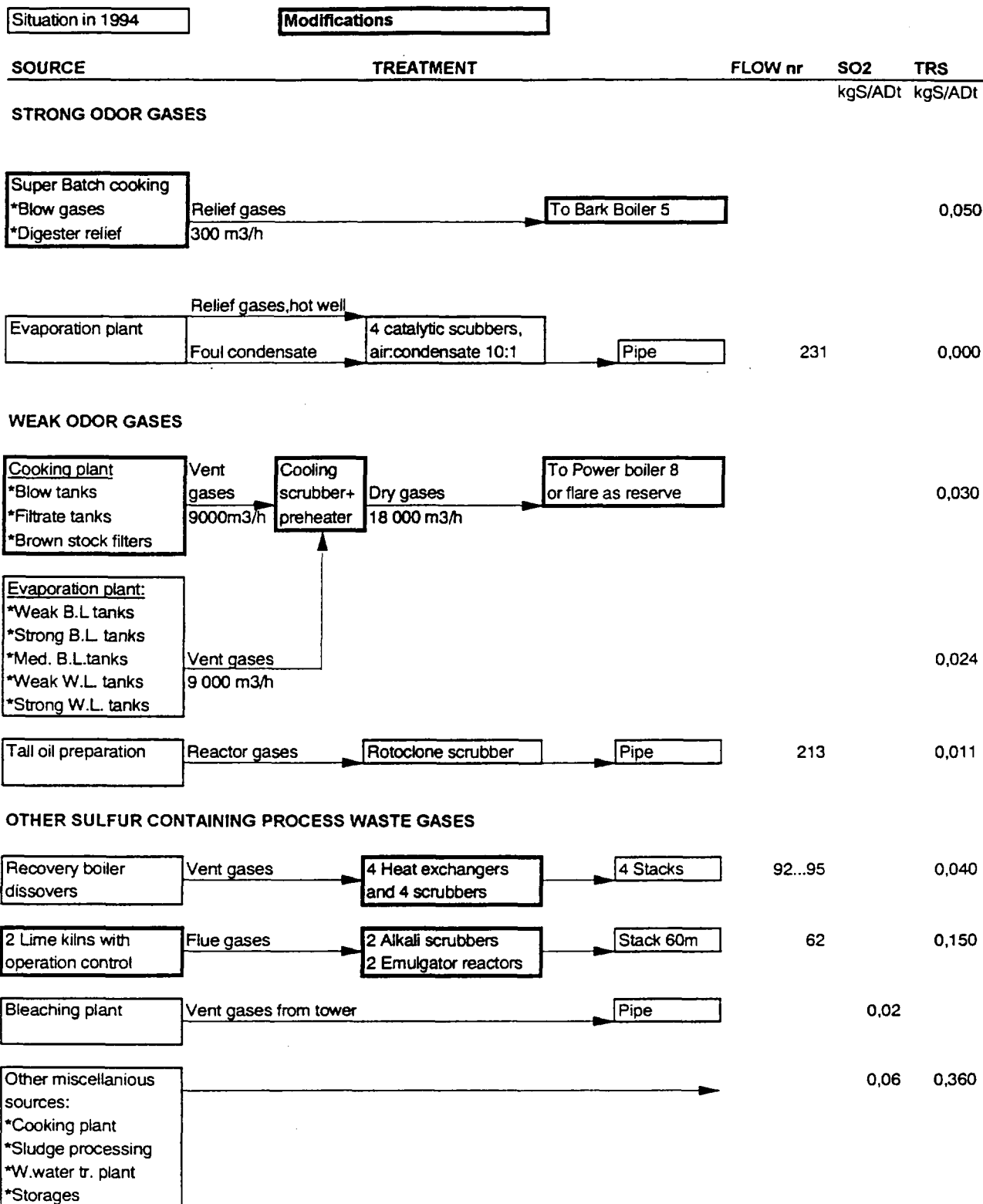
Total TRS emissions

Finland		BPPM
TRS	TRS	TRS
kgS/ADt	kgS/ADt	kgS/ADt
1,4..2,8		1,559
0,4..1,1		0,035
0..0,05		0,088
0,08..0,2		0,352
		0,363
0,05..0,1		0,227
1,9..4,2		2,624

ANNEX 10.

Sulphur emissions after modifications

SULFUR EMISSIONS AFTER MODIFICATIONS, PRODUCTION 200 000 ADt



SULFUR EMISSIONS AFTER MODIFICATIONS, PRODUCTION 200 000 ADt

SOURCE	TREATMENT	VENT	FLOW nr	SO2 kgS/ADt	TRS kgS/ADt
FLUE GASES FROM BOILERS					
Recovery boiler 1	Flue gas → Electr. precipitator	Stack 120m	240	0,17325	0,125
Recovery boiler 2	Flue gas → Electr. precipitator				
Recovery boiler 3	Flue gas → Electr. precipitator	Stack 120m	221	0,105	0,021
Recovery boiler 4	Flue gas → Electr. precipitator				
Bark boiler 5	Flue gas → Cyclones+scrubber			0,01	
Bark boiler 6	Flue gas → Cyclones+scrubber				
Coal power boiler 7	Flue gas → El.precip.				
Coal power boiler 8	Flue gas → Desulfurization Lifac → El.precip.				
Coal power boiler 9	Flue gas → El.precip.	Stack 120 m	222	5,21	
Coal power boiler 10	Flue gas → El.precip.				
Coal power boiler 11	Flue gas → El.precip.				
Efluent sludge boiler	Flue gas → Cyclones and scrubber	Stack 120m	300	0,03	
Efluent sludge boiler	Flue gas → Cyclones and scrubber				

TOTAL SULFUR EMISSIONS:

SULFUR EMISSIONS FROM HEAT GENERATION TO BAIKALSK CITY:

TOTAL SULFUR EMISSIONS OF MILL OPERATIONS:

Recommended level in Finland:

New permits in Finland:

SO2+TRS kgS/ADt	SO2 kgS/ADt	TRS kgS/ADt
6,31	5,606	0,707
	-0,73	
5,58	4,88	0,707
2,00		
1,5..2,0		
Finland BPPM		
TRS	TRS	
kgS/ADt	kgS/ADt	
1,4..2,8	0,000	
0,4..1,1	0,011	
0..0,05	0,040	
0,08..0,2	0,150	
	0,360	
0,05..0,1	0,146	
1,9..4,2	0,707	

TRS emissions from strong odor gases

TRS emissions from weak odor gases

TRS emissions from recovery boiler dissolver tanks

TRS emissions from the lime kiln

TRS emissions from miscellaneous sources

TRSEmissions from recovery boilers

Total TRS emissions

ANNEX 11.

Power and heat production in 1994

FUTURE PULP PROD.	120 253	ADI/a	Rec boil.1		Rec boil.2		Rec boil.3		Rec boil.4		Bark boil.5		Bark boil.6		Power boil.7		Power boil.8		Power boil.9		Power boil.10		Power boil.11		Sludge furnace		
	Units	TOTAL	Tampella	Tampella	Tampella	Tampella	Tampella	Tampella	KM/Tamp.	KM75-40	BKS-160/100	BKS-160/100	BKS-160/100	BKS-160/100	BKS-160/100	BKS-160/100	BKS-160/100	BKS-160/100	BKS-160/100	BKS-160/100	BKS-160/100	BKS-160/100	BKS-160/100	BKS-160/100	KC/Marubeni		
Boiler type																											
Operating hours	h/a	51 179	3 494	4 962	7 010	2 696	5 421	179			6 397	1 554	3 615	4 768	3 915	7 168											
Capacity																											
Rated power	MW/h																										
Steam pressure	bar		39	39	39	39	40	40	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	
Steam temperature	C		440	440	440	440	440	440	520	520	520	520	520	520	520	520	520	520	520	520	520	520	520	520	520	520	
Rated steam production	t/h		63	63	63	63	50	75	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	
Rec boiler capacity	IDS/d	1 520	380,0	380,0	380,0	380,0																					
Fuel consumption																											
Bl. liquor dry solids cons.	l/a																										
Coal consumption	l/a	464 504								139 775,0	39 593,0	78 185,0	111 790,0	95 161,0													
Heavy fuel oil consumption	l/a	15 593						25,0		11 884,0	1 105,0	368,0	737,0	1 179,0	295,0												
Bark consumption	m3/a							164 062,0																			
Flue gas treatment			E.P.	E.P.	E.P.	E.P.	Scrubber	Scrubber	E.P.	E.P.+Lifac	E.P.	E.P.	E.P.	E.P.	Cyclone+Scrub												
Efficiency	% SO2						90,0	90,0		60,0																80,0	
	%Dust		98,5	97,5	99,6	75,5	93,8	91,0	87,8	90,0	97,9	85,0	95,2	96,0													
Fuel properties																											
Heavy fuel oil	%S						0,9	0,9																			
Lower Heat Value	MJ/kg						40,2	40,2																			
Specific SO2 emission	mg/MJ	448																									
Coal	%S								0,5	0,5	0,5	0,5	0,5														
	%ash								16,0	16,0	16,0	16,0	16,0														
	%DS								77,0	77,0	77,0	77,0	77,0														
Lower Heat Value	MJ/kg								15,6	15,6	15,6	15,6	15,6														
Specific SO2 emission	mg/MJ	639																									
Black liquor	%DS		67	67	67	67																					
Emissions																											
SO2	l/a	2 931,2	16,2	22,8	93,1	39,9		0,5	902,0	283,0	541,0	627,0	399,0	6,7													
	mg/Nm3		38,8	38,2	110,7	123,5	55,0	93,0	653,0	843,0	693,0	609,0	472,0														
	mg/MJ								350	450	369	325	252														
NOx	l/a	2 261,0						89,4	3,0	715,0	252,0	361,0	497,0	337,0	6,6												
	mg/Nm3							110,0	112,0	517,0	750,0	462,0	482,0	398,0													
	mg/MJ								276,0	400,0	246,0	257,0	212,0														
Dust	l/a	3 149,3	19,3	45,7	10,4	357,8	44,5	2,5	1 065,0	267,0	121,0	919,0	272,0	25,1													
	mg/Nm3		46,0	77,0	12,0	1 107,0			771,0	795,0	155,0	892,0	322,0														
	mg/MJ								414,0	424,0	83,0	479,0															
Heat and power production																											
Electrical power production	GWh/a	337,2	12,9	18,4	26,0	10,0	8,3		82,6	20,1	46,7	61,6	50,6														
	TJ	1 213,9	46,6	66,2	93,5	36,0	29,9		297,5	72,3	168,1	221,8	182,1														
	kWh/ADt	2 804,1																									
Total heat production	TJ	10 336,6	618,3	863,9	1 252,3	448,4	391,7		2 064,3	563,8	1 187,3	1 591,7	1 355,0														
Heat to city	TJ	1 206,5							1 206,5																		
Heat to mill after turbines	TJ	7 612,4																									

ANNEX 12

Power and heat balance

1994 PRODUCTION ADt/a	120 400					
FUTURE PRODUCTION ADt/a	200 000					
HEAT BALANCE		BPPM	Cond.	Finland 70's	Target BPPM	
	GJ	GJ/ADt	ret.%	GJ/ADt	GJ/ADt	GJ
Woodhandling	45 960	0,38		0,35	0,35	70 000
Cooking+washing+screen	1 079 930	8,97		4,60	5,00	1 000 000
Bleaching+bleach chemicals	456 626	3,79		1,50	1,50	300 000
Drying	772 011	6,41	80,00	3,80	3,80	760 000
Evaporation	2 320 196	19,27	80,00	4,00	8,00	1 600 000
Recovery+power boilers	481 706	4,00		1,25	2,00	400 000
Causticisation+lime kilns	20 057	0,17		0,15	0,15	30 000
Total, process	5 176 486	42,99		15,65	20,80	4 160 000
Effluent treatment+sludge	105 249	0,87			0,35	70 000
Paper machine 2 t/t paper	41 141	0,34			0,32	64 000
Town	1 267 202	10,52			6,34	1 267 202
Heating +ventilation+hot water	891 904	7,41			4,46	891 904
Other departments	42 156	0,35			0,34	68 000
Losses	88 262	0,73			0,70	140 000
TOTAL	7 612 400	63,23			33,31	6 661 106
POWER BALANCE						
		BPPM		Finland 70's	Target BPPM	
		kWh/ADt	GWh/a	kWh/ADt	kWh/ADt	GWh/a
Woodhandling		84	10,11	50,00	50,00	10,00
Cooking		98	11,80	40,00	50,00	10,00
Washing+screening		100	12,04	150,00	100,00	20,00
Bleaching+bleach chem.prep.		123	14,81	200,00	120,00	24,00
Drying		237	28,53	150,00	170,00	34,00
Evaporation		71	8,55	20,00	50,00	10,00
Causticisation+lime kilns		70	8,43	20,00	60,00	12,00
Total pulp process		783	94,27	630,00	600,00	120,00
Water supply		102	12,28		60,00	12,00
Effluent treatment+sludge		490	59,00		220,00	44,00
Compressed air station		164	19,75		90,00	18,00
Paper machine 630 kWh/t paper		46	5,54		44,00	8,80
Lighting+ventilation+maintenance		172	20,71		100,00	20,00
Other departments		64	7,71		40,00	8,00
Losses		18	2,17		12,00	2,40
TOTAL		1 839	221,42		1 166,00	233,20

ANNEX 13

Target power and heat production

FUTURE PULP PROD	200 000 ADI/a	Rec.boil.1	Rec.boil.2	Rec.boil.3	Rec.boil.4	Bark boil.5	Bark boil.6	Power boil.7	Power boil.8	Power boil.9	Power boil.10	Power boil.11	Sludge furnace
Units	TOTAL	Tampella	Tampella	Tampella	Tampella	KM/Tamp.	KM75-40	BKS-160/100	BKS-160/100	BKS-160/100	BKS-160/100	BKS-160/100	KC/Marubeni
Boiler type													
Operating hours	h/a	50 958	7 500	7 500	3 160		7 300	2 000	3 330	7 000	6 000		7 168
Capacity			18 160										
Rated power	MWth												
Steam pressure	bar		39	39	39	39	40	40	100	100	100	100	100
Steam temperature	C		440	440	440	440	440	440	520	520	520	520	520
Rated steam production	t/h		63	63	63	63	50	75	160	160	160	160	160
Rec.boiler capacity	IDS/d	1 520	380,0	380,0	380,0	380,0							
Fuel consumption													
Bl. liquor dry solids cons.	t/a												
Coal consumption	t/a	380 875						72 760,8	178 346,8	129 767,6			
Heavy fuel oil consumption	t/a	12 103					33,7	6 186,3	4 977,5	610,8			295,0
Bark consumption	m3/a					220 928,4							
Flue gas treatment		E.P.	E.P.	E.P.	E.P.	Scrubber	Scrubber	E.P.	E.P.+Lifac	E.P.	E.P.	E.P.	Cyclone+Scrub
Efficiency	% SO2					90,0	90,0		60,0				80,0
	%Dust		98,5	97,5	99,6	75,5	93,8	91,0	87,8	90,0	97,9	85,0	95,2
													96,0
Fuel properties													
Heavy fuel oil	%S						0,9	0,9					
Lower Heat Value	MJ/kg						40,2	40,2					
Specific SO2 emission	mg/MJ	448											
Coal	%S								0,5	0,5	0,5	0,5	0,5
	%ash								16,0	16,0	16,0	16,0	16,0
	%DS								77,0	77,0	77,0	77,0	77,0
Lower Heat Value	MJ/kg								15,6	15,6	15,6	15,6	15,6
Specific SO2 emission	mg/MJ	639											
Black liquor	%DS		67	67	67	67							
Emissions													
SO2	t/a	2 204,3	34,8	34,5	42,0			5,6	469,5	713,4	897,9		6,7
	mg/Nm3		38,8	38,2	110,7	123,5	55,0	93,0	653,0	843,0	693,0	609,0	472,0
	mg/MJ								350	450	369	325	252
NOx	t/a	2 267,0					120,4	33,5	372,2	1 135,1	599,2		6,6
	mg/Nm3						110,0	112,0	517,0	750,0	462,0	482,0	398,0
	mg/MJ								276,0	400,0	246,0	257,0	212,0
Dust	t/a	2 186,1	41,4	69,1	4,7		59,9	27,9	554,4	1 202,7	200,8		25,1
	mg/Nm3		46,0	77,0	12,0	1 107,0			771,0	795,0	155,0	892,0	322,0
	mg/MJ								414,0	424,0	83,0	479,0	
Heat and power production													
Electrical power production	GWh/a	286,4	67,3				8,3		43,0	87,1	80,6		
	TJ	1 031,1	242,4				30,0		154,9	313,6	290,3		
	kWh/ADI	1 432,1											
Total heat production	TJ	9 159,2	618,3	863,9	1 252,3	448,4	391,7		1 074,6	2 539,4	1 970,7		
Heat to city	TJ	1 206,5							1 206,5				
Heat to mill after turbines	TJ	6 663,7											