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AUTOMATION OF SMALL ROLLING MILLS1

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Small rolling mills can be defined either by their products or by their rolling capacity. Typical products for small rolling mills are

> $\ddot{\bullet}$ robare . wire rods snail sections medium sections

Less frequent is the application of small rolling mills for

> narrow strips plates heavy sections

Wide strip is, because of the equipment costs and the very nigh capacity of a wide strip mill, not a typical product for small rolling mills.

Combinations between different products on the same mill are frequent, i. e. between reinforcing bars and wire rods or reinforcing bars and small sections.

Typical capacities for small rolling mills range between 30.000 and 100.000 tons/year for older mills and between 80.000 and 300.000 tons/year for newer mills.

Automation of existing mills cam be aimed towards a number of different problems in the mill. It is usually intended to improve the operati or. of a mill without changing the basic features, 1. e. the mill arrangement.

For new mills, considerations for automation are basically concerned with all the questions of lay-out.

The automation in rolling mill operation can have a number of different aims (see Fig. 1).

Pig. ¹ - Objectives of automation in rolling-mill operation

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I will state in advance that I shall not discuss the item 5, namely reducing of non-production time, since it is more of a factor for high-production mills,which have to attempt to squeeze non-production time to ^a minimum level when all other means of raising production have been exhausted and, for instance, speed increases are not possible.

This reduction of non-productive time normally requires considerable equipment and is connected with high capital investment. It is therefore not typical for the small mill practice which we discuss here.

If we first take up the automation of existing mills we will use as an example a simple bar mill as shown in rig. 2.

This mill consists of one three-high roughing stand, being supplied with billets from ^a pusher-type furnace, and an open finishing train with, for instance, ⁶ passes. After the finishing stand the bars are guided to a cooling bed which could be a grid-type manually operated bed.

The billet weight is limited by the length of the run-outs, particularly before the last pass, and by the maximum bar length that the cooling bed can accept. If the smallest rod size is 14 mm Ø the billet weight is limited to 80 kg.

If the mill is to be automated for higher weights the following steps are necessary (Pig. 3) :

- a) Install a flying dividing shear after the last stand and equip the cooling bed run-in table in such a way that it can accept a number of consecutive bars directly after sheering.
- b) Intall repeaters between the stands of the finishing train.

The same effect can, of course, also be obtained by menual repeating which, however, is a hazardous Operation and requires considerable skill.

0} Split the drive of the finishing train to liait loop lengths and give a higher exit speed.

> With these measures the piece weight can be increased from, say, 80 kg to 150 kg, and the corresponding increase production is from 5 tons/hour to 7.5 tons/hour.

The bottle-neck for a further increase in billet weight and production is the one-stand non-automated roughing train.

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A second roughing stand has to be installed, the 10 passes have to be shared between the two stands, and bars have to be guided from one stand to the other by the ise of repeaters.

With this a piece weight of 300 kg becomes possible and the production can be increased to approx. 12 tons/hour.

Since the production now depends very much on the exact and accurate work of the roughing stand for different passes, it is highly desirable at this stage to automate the pass sequence of the first stand. The normal means of automation of the first stand are $(r_i, 4)$:

> tilting table on either the entry or the exit side, depending on the prss design

and

slide walls on the opposite side to tilt the rectangular oval bars up when running out between top and midle rolls and re-enter in the upright position between bottom and intermediate roll.

The purpose of the tilting table is to allow to run a number of bars simultaniously towards the rolls and at the same time eliminate the manual lifting and guiding of the bars on this side.

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The slide walls eliminate the manual work of turning.

 $\sim 10^{11}$ km $^{-1}$

The obvious short-coming of the slide walls is that, if the bars are not perfectly straight,difficulties nay arise due to the bars sticking between the slide walls.

Therefore the bar length to be used on the slide walls is Halted, especially if the bars become thinner. The practical limit is in the order of 12 m.

If for some applications longer slide walls are required, it is recommendable to install a vertical pinch-roll set at the bottom of the walls to ensure that the bars are, if necessary, forced up and guided into the next pass.

^A ¹⁰ pass roughing train, fully automated, consisting of tuo stands will be able to harile up to ²⁰ tens/hour.

Still higher tonnages require a reduction of the number of passes in the roughing train.

If two passes are transferred to the finishing train by adding two additional continuous stands at the end, two objectives are achieved, namely the roughing-trein capacity is increased and the finishing-train capacity is also

increased due to a higher finishing speed of the bars by the addition of the two continuous stands.

Such a mill will be capable of piece weights of ³⁰⁰ to 350 kgs (based on ¹⁰⁰ mna square entry] and production rates of approx. 25 tons/hour.

k «till further increase can be achieved by limiting the number of passes in the roughing train to ^C and increasing the number of finishing stands to ⁴ continuous-arranged finishing stands. This arrangement will be capable of productions in the order of 35/40 tons/hour.

In summary, it can be said that for existing mills the following tools of automation are applicable and give the best results

- repeaters on finishing train
- dividing shear in front of cooling bed
- cooling bed entry trough for close sequence of bars automation of roughing train with repeater, tilting tables, and slide walls
- addition of continous finishing stands for speed increase

In many cases the possible increases are limited by the entry piece available, particularly if this is an ingot. Small ingot practice is usually limited to ingot weights of approx. 100 to 120 kg. For heavier ingots the crosssection is such that additional passes are needed in the roughing train, which defeats the purpose of a production Increase.

However, when continuously cast or bought billets are available, one should utilize the possibility of increased lengths and therefore increased weights.

In generally it can be stated that the success of the automation of existing mills is dependent on a high degree of operational and maintenance skill. This explains why the reported successes of such automation vary considerably, even thou. the same elements are used.

May I mention that attempts have been made to automate the roughing trains «ven further by eliminating the tilting table and replacing it by a number of independent narrow tables. With this »»asure the time interdependence between the individual passes can be completely eliminated. On the other hand, very complex controls are necessary. This solution has only found a very limited application with special steel makers.

In recent years it has been realized that an automated rolling process is easier to operate if the mill used is a continuous mill. Therefore, for new mills an investigation should be made to which extent continuous operation is feasible. In many cases it has been decided to install continuous arrangements in spite of the fact that the full production capacity *of* continuous mills was not required in the particular case.

If one looks at a fully continuous mill for rounds (Fig. 5), it becomes apparent that, in addition to the high mechanical equipment costs, the electrics play an important part. The costs of individual O.C. drives can easily amount to ³ - ⁴ Mio Dollars on such a mill, the costs not only stemming from the fact that direct current is used but also from necessity to establish a very close control of the speed ratios. It has therefore been normal to limit the number of drives by grouping a number of stands (2 to 10 stands) and connecting them with fixed gear ratios. Of course, this requires a very good prediction on the pass design and speed ratios to be used and is less flexible if product changes are considered.

Also the roll costs are higher since the sets of rolls have to bo kept matched in di anoter.

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For small mill operation this arrangement is still a relative! ' expensive proposi' ton and is normlly used if production rates of, say, 200.COO tons or more are considered.

Por smaller tonnages a combination in the form of a semicontinuous or hybrid mill is quite adequate (Fig, 6). This hybrid mill la characterized by the use of group drives, A.C. drives with loops inbetwean to take up the variations in roll diameter and the potential speed drops of the A.C. drive on load.

This type of mill is capable of billet weights of 500 to 600 kg, and la possible if one is prepared to sacrifice somewhat in flexibility.

It can be used for mills preaucing rebars and rounds and for combination mills with rèbars, rounds,and wire rods.

It normally does not lend itself for section-mill applications.

The hybrid mill can normally be laid out in such a manner that by exchange of motors and splitting of drives the mill can be converted into a fully continuous mill, accepting much higher entry weights C1.000 to 1.500 kg), and operating at production levels in the order 300.00 tons 'year.

In this case, however, capacity ard arrangement of furnace and arrangement of the cooling bed have to take into account this later addition.

The mechanical costs of such a mill are relatively high since one stand has to be used for every pass required.

An interesting possibility to save on the mechanical side as well is to arrange the roughing train as a twice-through mill (Fig. 7). This arrangement uses, for example, four stands fer 8 passen. The bar is returned to the first stand after passing through No. 4 and only after all 8 passes have been completed the bar will be guided to the intermodiate train.

This arrangement needs scme additional space and mechanical handling gear for the return of the bars but is still cheaper then an 6-stand roughing train.

Furthermore, it can be extended at any time in future by adding another ⁴ stands, thus making it ^a completely continuous roughing train.

The billet weight is somewhat restricted in this case and should, with a 100 mm square entry, not exceed 450 to 500 kg. Otherwise the space in front and behind the twice-through roughing train becomes excessive.

In the layout of mills producing sections a fully continuous mill is normally not compatible with the needs of a small rolling mill. The reason is that a continuous section mill can normally not employ group drives and has to have a number of vertical stands in order to have the necessary edging **DASSes.**

Also continuous section mills require complex mechanical and electrical equipment for quick pass and stand changes to maintain the required flexibility with frequent section changes.

For small rolling mills therefore the following solution for section rolling is preferable (Fig. 8) :

roughing train:

continuous, possibly as twice-through train or arranged as a automated three-high mill

intermediate train: open

with repeaters for the lighter sections, such as angles

finishing train

consisting of one to three continuous individually driven stands behind the last stand of the open train

This will limit the length of the free run-outs or the loops and pernit rolling of a precise product. Also the finishing speed can be higher then normal with open trains.

The main tasks for automation of small-tonnage section mills lie in the finishing end *(?ig.* 9).

Instead of the conventional double-handling by cutting to finished length first, storing, untangling, straightening, and stacking,it is definitely preferable to do ail this in one production flow.

This, however, requires an increased cooling-bed size, cooling the bars down to a temperature acceptable for straightening (for instance 100 °C), and straightening with

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a high-speed straightener directly off the cooling bed in full cooling-bed bar length.

Only after this, the bars are collected to groups and out and stacked.

It is realized that this requires heavy additional investments in the finishing end because of

- the larger size of the cooling beds
- the high-speed straightening
- the considerable mechanical equipment and space needed for collecting groups of bars and allowing cutting and stacking

Mowever, this is more than balanced by the fact that far less manpower is needed, that the cut length can be easier varied for customer demands, and that no intermediate stockage is required, which otherwise would tie large amounts of operating capital.

Returning to bar mills (Fig. 10), it may be interesting to know the recent developments in the automation of cooling beds. The most simple cooling bed is normally a trough followed by a grid-type cooling bed, operated manually.

Nost new.r mills have a cool.ng bed which can accept a sequence of bars, transfer them to a rake system, from where the bars are collected by shuffle-bars into groups and then cut on the cold shear. It is characteristic for this type of cooling bed that the bars entering the cooling bed are pre-cut into multiples of sales lengths, 1. $e. 60$ m long to give 5 x 12 m on the cold shear.

A newer development is to cut directly to sales lengths at the shear bahind the last stand, cooling the bars on a short fast-cycle cooling bed. After cooling, the bars can the directly collected into groups and, without further, baadling, bundled and shipped.

This type of cooling bed depends, of course, heavily on the shear in front of the cooling bed. From our own practice I oaa report that with such a shear, which is ^a start-stop shear, we are achieving an accuracy of plus/minus 2 om when cutting at ¹¹ a/eec.

The savings on manpower amount to at least 6 man per shift or oa ¿.shift operation IS workers.

Also the apace requirement ia so much less that this la itaelf justifies the higher expenses for the rotary shear.

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La sumary I you d'ilse to bring out the main points again:

The easonation of chieting mills is a complex task relying heavily on the operational and maintenance skill. This is true in spite of the fact that the individual elements of such automation, such as repeators, slide wills, tilting trble, continuous finishing stands, etc. are well known. In any case, such an automation requires a datailed study not only on the elements to be automated but also of the other parameters involved, such as furnace capacity, cooling bed performance, atc. Any such automation should only be done as a step-by-step approach.

For new mills, particularly mills rolling rebars and rounds, the automation should take into account the experience that continuous mills are nume eas, to operate the vopen trains. Any such automation should therefore use as many elements of continuous mills as possione. even compromises have been obtained by using group drives driven by A.C. motors and by twice-through roughing mills.

For section mills, any automation should preferably start at the finishing and where most saving can be accomplished.

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A notable development in the automation of mills is the introduction of sales-length cooling beds which have led to a considerable decrease in nill manpower.

